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NAVAL POSTGRADUATE SCHOOL

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THESIS

COMPUTER PROGRAMS FOR HELICOPTER DATA DISPLAY
AND CONCEPTUAL DESIGN

by

Gary M. Bishop

December 1983

Thesis Advisor:

Donald M. Layton

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that uses the FORTRAN language the ability to do a complete conceptual design of a helicopter at one sitting in accordance with the procedures in the Helicopter Design Manual published as course notes for the AE 4306 Helicopter Design course at the Naval Postgraduate School.

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Computer Programs for Helicopter Data Display
and Conceptual Design

by

Gary M. Bishop
Captain, United States Army
B.S., United States Military Academy, 1975

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL
December 1983

Author: _____

Approved by: _____

Thesis Advisor

Chairman, Department of Aeronautics

Dean of Science and Engineering

ABSTRACT

→ This thesis allows a person with access to a computer that uses the FORTRAN language and that is equipped with the DISSPLA software system the ability to select and graphically portray for analysis the critical design parameters of actual helicopters. It also allows a person with access to any computer that uses the FORTRAN language the ability to do a complete conceptual design of a helicopter at one sitting in accordance with the procedures in the Helicopter Design Manual published as course notes for the ~~AE 4306~~ Helicopter Design course at the Naval Postgraduate School.

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I. INTRODUCTION

A. BACKGRUND

The helicopter industry, as in most industries, incorporates many of the attributes of its previous designs into its new products. New aircraft are generally built upon the successes of previous designs with minor changes due to technological advances. These technological advances usually relate to new materials and new methods of control but hardly ever result in drastic changes to the aerodynamic surfaces. These proven designs of the integral parts which have specific aerodynamic characteristics are well documented and extremely useful in the design process. It is essential for the designer to have this corporate knowledge of design trends for the design process as well as for the validation of his design. This knowledge of design trends is necessary for both the designer in industry and the student in a learning environment.

Outside of specific helicopter companies, little has been done to analyze the interrelationships that exist between design parameters. These interrelationships provide a bases for the simplification of assumptions and validation of design results. This knowledge needs to be available to

the design student just as it is to the design engineer so that the information can be used for an analysis or verification during the design process. Therefore, it is important that this information be readily available and that the student have quick, easy and well defined access to this information.

The retrieval and analysis of historical data is but one part of the design process. The critical part is the actual process whereby a conceptual design is accomplished through many iterations. This process is long and involved but provides the design student with a basic understanding of the design process. For a more indepth study of the design process it is necessary for the student to vary as many of the design parameters as possible in order to see the interrelationships that exist. This process also allows the student to become intimately familiar with the problems and needs of the designer.

To date, no known programs for the IBM 3033 have been prepared that will take the design student through the entire process from historical analyses to conceptual design completion.

B. GOALS

The objective of this study was to develop an interactive capability for the design student using the IBM 3033 computer. The program, if used at the Naval Postgraduate School, should be capable of providing graphical representations of the critical data necessary for a proper analysis in the data analysis phase. During the conceptual design phase the program should allow for design student/computer interaction so that the design student can readily see the effects of varying critical parameters. To maximize the assets available at the Naval Postgraduate School, the Tektronix 618 dual screen system and the DISSPLA [Ref. 1] software system should be incorporated in the structuring of the computer programs.

The programs should be designed primarily for the use of Aeronautical Engineering students at the Naval Postgraduate School enrolled in the Helicopter Performance, Helicopter Design, and Advanced Helicopter Design courses.

II. APPROACH TO THE PROBLEM

A. INTRODUCTION

The basic approach was to write two computer programs utilizing the DISSPLA software system for use on the IBM 3033 using FORTRAN IV. The programs are completely interactive, prompting the user for all necessary information and then graphically depicting the information in the form of tables on the IBM 3278 screen or as a graph on either the Tektronix 618 screen or by use of the VERSATEC plotter. If the Tektronix machine is used, the displayed graph can be copied directly using electrostatic copiers attached to each machine.

B. ANALYSIS OF HELICOPTER DESIGN DATA

The first program consists of a historical data display system that takes thirty critical design parameters and allows the user to select the parameters for analysis. The user can then specify the page format as well as the number of graphs per page of the finished graph. Subroutines within the program are as follows:

1. Block data
2. Data point identification
3. Graphical display formatting

C. CONCEPTUAL HELICOPTER DESIGN

The second program is written to correspond procedurally WITH THE Helicopter Design Manual [Ref. 2] used in the AE 4306 Helicopter Design course at the Naval Postgraduate School. The formulae necessary for the computation of each section is provided in lieu of subroutine use. This allows for quick and easy updating of the program as it becomes necessary. Also, if the student desires, it can be seen how the data that is received is computed. This program is completely interactive and requires only that the student have the information listed on the design specification sheet and the accompanying charts and references necessary for the required decisions during the design process. All tables and graphs are generated and displayed either on the IBM 3278 screen or the Tektronix 618 screen. Output for the tabular data is provided on a separate file and the single graph needed for design decisions can be obtained using the electrostatic printers.

Detailed knowledge of the IBM 3033 computer is not necessary. A familiarity of helicopter aerodynamics and performance is, however, necessary for proper utilization of the program in order to obtain meaningful design information.

III. SOLUTIONS TO THE PROBLEMS

A. DATA DISPLAY PROGRAM

Table I lists the thirty critical design parameters used most often in any analysis of an aircrafts performance as found in the Helicopter Performance Manual [Ref. 3].

TABLE I

Design Parameters

Main rotor radius
Tail rotor radius
Number of main rotor blades
Number of tail rotor blades
Height of the main rotor system
Speed of the main rotor
Speed of the tail rotor
Chord of the main rotor
Chord of the tail rotor
Span of the main rotor
Span of the tail rotor
Twist of the main rotor blade
Twist of the tail rotor blade
Profile drag of the main rotor blade
Profile drag of the tail rotor blade
Disc loading of the main rotor system
Width of the fuselage
Length of the fuselage
Frontal equivalent flat plate area
Vertical equivalent flat plate area
Maximum forward velocity
Maximum range
Rate of climb
Hover ceiling (IGE)
Hover ceiling (CGE)
Length of the tail
Operating weight
Load weight
Fuel weight
Maximum gross weight

The above parameters have been deemed those most critical to the design process. The airfoil data has been extrapolated from NACA data and the specific helicopter

performance parameters have been extrapolated from the various manuals for the specific helicopters. Tables III through X, Appendix C, list the specific data utilized for the study.

Table II lists the helicopters used for the analysis portion of the graphing.

TABLE II
Representative Helicopters

| <u>Military Designator</u> | <u>Weight Classification</u> | <u>Branch of Service</u> |
|----------------------------|------------------------------|--------------------------|
| AH-64 | Medium | USA |
| OH-6A | Light | USA |
| SH-3H | Medium | USN |
| S-76 | Medium | USN |
| UH-60A | Medium | USA/USN |
| CH-54B | Heavy | USA |
| CH-53D | Heavy | USN |
| CH-53E | Heavy | USN |

All the helicopters selected for study were single main rotor helicopters that are still in the active inventories of the agencies listed. The selections were made with deference to aircraft of the U.S. Army and U.S. Navy and then to a representative sampling of the three major weight classifications.

The data from Tables III through X can now be graphed in the following combinations using the Data Display program:

1. Simple X-Y plot

- a. Horizontal page format (11 X 8.5 inches)
- b. Vertical page format (8.5 X 11 inches)
2. Two parameters versus a third
 - a. Horizontal page format (11 X 8.5 inches)
 - (1) Two axes on the abscissa scale
 - (2) Two axes on the ordinate scale
 - b. Vertical page format (8.5 X 11 inches)
 - (1) Two axes on the abscissa scale
 - (2) Two axes on the ordinate scale
3. Two X-Y plots on the same page with a horizontal page format
4. Three parameters versus one common parameter with a vertical page format
5. Four separate X-Y plots on the same page with a horizontal page format

Figures 3.1. through 3.9., Appendix C, illustrate the capability of the program. The program was devised so as to allow the greatest flexibility for the analyst as to the graphical presentation.

B. CONCEPTUAL DESIGN PROGRAM

The design process is in accordance with the procedural steps as outlined in the Helicopter Design Manual. The

program is devised so as to allow the design student the ability to do a complete conceptual design at one sitting if he is properly prepared. The program lists all critical tables and information necessary for doing an analysis of the design and also provides the necessary information to prepare a written report. If the Tektronix dual screen combination is used, the student has a graphical representation of the total power curve at altitude presented to him which must be used to extrapolate critical design performance parameters. Figure 3.10. is a sample of the graphical representation provided. Sample output is provided in Appendix B to illustrate the capabilities of the program and the possible usefulness to the design student.

IV. RESULTS AND CONCLUSIONS

A. DATA DISPLAY PROGRAM

This program provided good results in use for the analyses of the design parameters considered, particularly in the correlation between commonly used 'rules of thumb' and graphical analyses of the same parameters.

The capability of the program could be enhanced in several ways. First, additional single main rotor helicopters could be added to enable a more complete analysis to be accomplished. Second, the use of different scales, such as the logarithmic scale, for the graphical analysis could prove to be more suitable for some of the parameters. Third, additional parameters that other companies have compiled in their technical manuals could be added for analysis.

B. CONCEPTUAL DESIGN PROGRAM

This program provided information consistent with existing aircraft. The interactive characteristic of the program allows the student to actively participate in the design process and, most importantly, the program allows the student to vary parameters and see the effects of changing a

single parameter on the entire design process. If the student was prepared and had all the appropriate references, this process need only take an hour to complete one iteration of the entire process. This allows for multiple iterations, optimization, and parameter variation.

One problem with the program is that it is only as good as the assumptions that have been made for the model to simplify the formulae used as given in Reference 3. A crude approximation to existing aircraft can be made with the understanding that the aircraft designed during this process is merely a conceptual design and the beginning step in the process for the final product. This model has been developed so that changes made to the course can be incorporated easily and that any corrections can be made quickly. This program also can be run on any FORTRAN capable computer using the coding listed in Appendix B.

APPENDIX A

A. USERS GUIDE TO THE DATA DISPLAY PROGRAM

The program has been written with the user in mind. It is completely interactive once the program has been loaded into the DISSPLA mode so that the user need only read the instructions presented on the screen carefully.

Use the following procedure to invoke the Data Display program once the Fortran program resides on the users disk.

1. Logon as normal at either a regular IBM 3278 terminal or at a Tektronix 618 dual screen terminal
2. Obtain the use of temporary storage space by entering the following:

DEFINE STORAGE 1M (enter)

3. When the PSW '00020000 00000000' appears on the screen type in:

I CMS (enter)

4. If the program has not been previously compiled on your disk type in:

PORTGI HELODATA (enter)

5. When the program has been compiled you are ready to enter into DISSPLA by typing in:

DISSPLA HELODATA (enter)

6. Follow the instructions given on the screen. If you desire a hard copy of the graphs do the following:

IBM terminal--Exit the program and
enter DISSPOP and then
follow the instructions

TEK terminal--Press the hard copy button
on the large monitor

B. PROGRAM NOMENCLATURE

| <u>MNEMONIC</u> | <u>DEFINITION</u> |
|-----------------|---|
| ANS | General variable for reading keyboard answers |
| B | Number of main rotor blades |
| BTR | Number of tail rotor blades |
| C | Chord of a main rotor blade in feet |
| CDO | Profile drag of a main rotor blade section |
| CDOTR | Profile drag of a tail rotor blade section |
| CTR | Chord of a tail rotor blade in feet |
| DL | Disc loading of the main rotor system |
| FH | Frontal effective flat plate area in square feet |
| FV | Vertical effective flat plate area in square feet |
| FWT | Fuel weight in pounds |
| HOVIGE | Hover ceiling (in ground effect) in feet |
| HOVOGE | Hover ceiling (out of ground effect) in feet |
| HT | Height of the main rotor system above the ground in feet |
| I | Do loop variable |
| IPAK | Array for packing legend information |
| KINDS | Array for packing legend information |
| LGH | Length of the fuselage in feet |
| LT | Length of the tail in feet |

| | |
|--------|---|
| LWT | Load weight in pounds |
| MGW | Maximum gross weight in pounds |
| OPTION | Term used in Switch subroutine for page formatting |
| OWT | Operating weight in pounds |
| PANS | References page format selection |
| R | Main rotor radius in feet |
| RC | Maximum rate of climb in feet per minute |
| RNG | Maximum range in nautical miles |
| RPM | Speed of the main rotor system in RPM |
| RPMT | Speed of the tail rotor system in RPM |
| RS | Span of a main rotor blade in feet |
| RSTR | Span of a tail rotor blade in feet |
| RTR | Tail rotor radius in feet |
| TEMP1 | Dummy parameter returned from subroutine |
| TEMP2 | Dummy parameter returned from subroutine |
| TEMP3 | Dummy parameter returned from subroutine |
| TITALT | Program trip used in multiple axes plotting |
| TWOAX | References which axis has two axes plotted |
| TWST | Twist of a main rotor blade in degrees |
| TWSTR | Twist of a tail rotor blade in degrees |
| VM | Maximum velocity in knots |
| WDT | Width of the fuselage in feet |
| X | Array returned from Switch subroutine containing abscissas for plotting |

| | |
|-------|---|
| XANS | Answer referenced to X axis selection |
| XANS1 | Answer referenced to multiple X axes selection |
| XANS2 | Answer referenced to multiple X axes selection |
| XMAX | Maximum value of abscissa desired for plotting |
| XORIG | Minimum value of abscissa desired for plotting |
| XPOS | Array of values referencing subplot locations of abscissas |
| XSTP | Increment size between minimum and maximum of the abscissa axis |
| XTWO | Array returned from Switch subroutine containing abscissas for plotting |
| X2ANS | Array for X axis answers for two graph option |
| X4ANS | Array for X axis answers for four graph option |
| Y | Array returned from Switch subroutine containing ordinates for plotting |
| YANS | Answer referenced to Y axis selection |
| YANS1 | Answer referenced to multiple Y axes selection |
| YANS2 | Answer referenced to multiple Y axes selection |
| YMAX | Maximum value of abscissa desired for plotting |
| YORIG | Minimum value of ordinate desired for plotting |
| YPOS | Array of values referencing subplot locations of ordinates |
| YSTP | Increment size between minimum and maximum of the abscissa axis |
| YTWO | Array returned from Switch subroutine containing ordinates for plotting |
| Y2ANS | Array for Y axis answers for two graph option |
| Y3ANS | Array for Y axis answers for three graph option |

Y4ANS Array for Y axis answers for four graph option
Z Array in subroutine switch for parameters

```

REAL R(8), RTR(8), B(8), BTR(8), HT(8), RPM(8), RPMTR(8), C(8), CTR(8)
REAL RS(8), RSTR(8), TWST(8), TWSTR(8), CDO(8), CDOCTR(8), DL(8)
REAL HCVG(8), LGH(8), FV(8), VM(8), RNG(8), RC(8), HOVI GE(8)
REAL HORIGE(8), QWT(8), LWP(8), FWT(8), MGW(8)
REAL YORIGE(8), YMAX, XORIG, XMAX, XANS, YANS, XANS1, XANS2, XANS, Y
1ANS2, YANS2, TITALT, TWOAX, ANS, PANS, XTWO
2(8), YTHC(8), TEMP1, TEMP2, TEMP3, XPOS(9), YPOS(9), Y3ANS(3), X4ANS(4), Y4
3ANS(4), X2ANS(2), X(8), Y(8)
INTEG XPOS(1), I, K, IINDS(200), IPAK(200)
DATA XPOS/1.5, 6.5, 1.1, 1.1, 6.5, 1.1, 6.5/
DATA YPOS/1.1, 1.1, 3.75, 6.1, 1.1, 1.1, 4.4/
COMMON /C1/ R, RTR, B, BTR, HT, RPM, RPMTR, C, CTR, RS, RSTR, TWST, TWSTR, CDO
1, CDOCTR, CL, W, CT, LGH, FV, VM, RNG, RC, HOVI GE, HOVGE, LT, OWT, LWT, FWT, MGW
C*** THIS SECTION DETERMINES WHICH TYPE OF TEKTRONIX EQUIPMENT THAT YOU
C*** ARE USING AND MAKES THE APPROPRIATE CALLS TO BRING THE SYSTEM ON
C*** LINE

```

```

CALL FRTCHS (,'CLSCRN 6')
WRITE (6,37C)
WRITE (6,38C)
READ (5,*) ANS
IF (ANS.NE.1.) GO TO 360
CALL FRTCHS (,'CLSCRN 6')
WRITE (6,39C)
READ (5,*) ANS
CALL FRTCHS (,'CLSCRN 6')
IF (ANS.NE.1.) GO TO 10
CALL TEK618
GO TO 30
IF (ANS.NE.2.) GO TO 20
CALL TEKALL (462,30,31,1,0)
GO TO 30
IF (ANS.NE.3.) GO TO 340
CALL CCMPRS
CONTINUE SSL
CALL SWHTCLR (,1)
CALL HEIGHT
CALL HEIGHT
C*****
C THIS PORTION PACKS THE INFORMATION INTO AN ARRAY SO THAT A STORY
C CAN BE PRIVATE CNTD EACH GRAPH WITH THE MEANING OF THE NUMBERS THAT
C LABELS GIVE FOR EACH PLOT
C*****
CALL LINES (,1, AH-64 5. UH-60A$,KINDS,1)

```



```

40      CALL RESET ('HEIGHT')
      GO TO 20 NE 2.) GO TO 340
      WRITE (6,*) ANS
      READ (5,*) ANS
      IF (ANS.NE.1.) GO TO 340
      CALL FRAMES (1,CLRSCRN 6)
      CALL PAGE (5,11)
      CALL HPROT ('AUTO')
      CALL AREA2D (6,8)
      CALL HEIGHT (3)
      CALL MESSAGE ('HELICOPTER DESIGN',-100,0.,8.5)
      CALL RESET ('HEIGHT')
      CALL MESSAGE ('AE 4306/4900$,100,1.2,8.25)
      CALL MESSAGE ('KINDS,4,4.25,8.25)
      CONTINUE (6,41)
      WRITE (6,*) ANS,VANS
      READ (5,*) ANS,VANS
      CALL FRAMES (6,CLRSCRN 6)
      CALL FRAME (1,NCENDS)
      CALL XAXEND (1,NCENDS)
      CALL SWITCH (XANS,1.,X,XORIG,XSTP,XMAX)
      CALL SWITCH (VANS,2.,Y,YORIG,YSTP,YMAX)
      CALL GRAF (XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)
      CALL GRESET (XTTICKS)
      CALL RESERVE (Y,Y,8,-1)
      CALL CURVEL (X,Y)
      CALL LABEL (X,Y)
      TT=0.0
      GO TO 180

```

50

```

**SINCE 3 PARAMETERS WERE CHOSEN, THE USER IS GIVEN A CHOICE OF PAGE
**FORMAT (LOCAL BEING DISPLA A LEVEL REQUIREMENTS, THEREFORE, THE ADDITIONAL
**SCALES USED TO BE DESIGNATED FOR ADDITIONAL AXES CAN BE MADE
**VALUES TO BE DISPLA A LEVEL REQUIREMENTS, THEREFORE, THE ADDITIONAL
**HAS BEEN A SUBROUTINE FOR ADDITIONAL AXES CAN BE MADE
**CALL TO CONTINUE
**CONTINUE HEIGHT (1)
**CALL MYLEGN (1)
**CALL SETCLR (RED)
**CALL LINES (PRIMARY)
**CALL SETCLR (GREEN)

```

60

```

70      CALL LINES ('SECONDARY AXES$', IPAK, 2)
      CALL LSETCLR ('BLACK')
      CALL RESET ('HEIGHT')
      IF (ANS.NE.3.) GO TO 340
      WRITE (6, 430)
      READ (5, 440) FANS
      CALL FRTCMS ('CLRSCRN 6')
      WRITE (6, 450)
      READ (5, 460) TWOAX
      CALL FRTCMS ('CLRSCRN 6')
      IF (PANS.NE.1.) GO TO 70
      IF (TWOAX.NE.1.) GO TO 110
      GO TO 90
      IF (PANS.NE.2.) GO TO 340
      IF (TWOAX.NE.1.) GO TO 80
      GO TO 130
      IF (TWOAX.NE.2.) GO TO 340
      GO TO 150
      CONTINUE
      WRITE (6, 470) ANS
      IF (ANS.NE.1.) GO TO 340
      CALL FRTCMS ('CLRSCRN 6')
      WRITE (6, 480)
      WRITE (6, 490) XANS1, XANS2, YANS
      READ (5, 500) XANS1, XANS2, YANS
      CALL FRTCMS ('CLRSCRN 6')
      CALL PAGE (11, 8.5)
      CALL PHYSOR (1, 5.2)
      CALL AREAZD (9, 5)
      CALL HEIGHT (3)
      CALL MESSAGE ('HELICOPTER DESIGN$', -100, 0, 5.5)
      CALL RESET ('HEIGHT')
      CALL MESSAGE ('AE 4306/4900$', 100, 1.2, 5.25)
      CALL MESSAGE ('KINDS 4, 7.25, 5.25')
      CALL MESSAGE ('XANS1, 1. X, XORIG, XSTP, XMAX')
      CALL MESSAGE ('YANS, 2. Y, YORIG, YSTP, YMAX')
      DO 100 I=1, 1
      YTH(I)=Y(I)
      CONTINUE
      YTOTAL=1.0
      GO TO 170
      CONTINUE
      WRITE (6, 510) ANS
      READ (5, 520) ANS
      IF (ANS.NE.1.) GO TO 340
      CALL FRTCMS ('CLRSCRN 6')
      WRITE (6, 530)

```

```

120 WRITE (6,47C) XANS,YANS1,YANS2
    READ (5,4) XANS,YANS1,YANS2
    CALL FRICMS (1,1,8.5)
    CALL PAGEFOR (1,2,5,1.0)
    CALL AREA2D (7,5,6.)
    CALL HEIGHT (3)
    CALL HESEAG (HEIGHT)
    CALL HESEAG (HEIGHT)
    CALL HESEAG (AE 4306/4900$,100,1.2,6.25)
    CALL LSTORY (KINDS,4,5,75,6.25)
    CALL SWITCH (XANS1,1,X,XORIG,XSTP,XMAX)
    CALL SWITCH (YANS1,2,Y,YORIG,YSTP,YMAX)
    DO 120 I=1,6
    XTWO(I)=X(I)
    CONTINUE
    TITALT=2.0
    GO TO 170
130 CONTINUE
    WRITE (6,48C)
    READ (5,4) XANS
    IF (XANS.NE.1.) GO TO 340
    CALL FRICMS (1,1,8.5)
    WRITE (6,410)
    WRITE (6,46C) XANS1,XANS2,YANS
    READ (5,4) XANS1,XANS2,YANS
    CALL FRICMS (1,1,8.5)
    CALL PAGEFOR (1,2,5,1.0)
    CALL HEIGHT (3)
    CALL HESEAG (HEIGHT)
    CALL HESEAG (AE 4306/4900$,100,1.2,7.75)
    CALL LSTORY (KINDS,4,4,75,7.75)
    CALL SWITCH (XANS1,1,X,XORIG,XSTP,XMAX)
    CALL SWITCH (YANS1,2,Y,YORIG,YSTP,YMAX)
    DO 140 I=1,6
    YTWO(I)=Y(I)
    CONTINUE
    TITALT=3.0
    GO TO 170
140 CONTINUE
    WRITE (6,49C)
    READ (5,4) XANS
    IF (XANS.NE.1.) GO TO 340
    CALL FRICMS (1,1,8.5)

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160 WRITE (6,41C)
    READ (5,47C)
    CALL FRAMES (ANS,YANS1,YANS2,
    CALL FRAMES (CLRSCRN 6,
    CALL HPHYSOR (8.5,11,
    CALL HPHYSOR (2.25,1.
    CALL AREAZD (5.75,8.
    CALL AREAZD (3,
    CALL HESAG (HEIGHT,
    CALL HESAG (AE 4306/4900$,100,1.2,8.25)
    CALL HESAG (KINDS 4,4.8,25)
    CALL LSTCRY (XANS,1.0,X,XORIG,XSTP,XMAX)
    CALL SWITCH (YANS1,2.0,Y,YORIG,YSTP,YMAX)
    DO 160 I=1,E
    XTWO(I)=X(I)*E
    CONTINUE
    TITAT=4.0
    GO TO 170
170 CONTINUE
C** NORMAL DISPLA CALLS TO ESTABLISH THE STYLE OF WRITING, PUTTING A
C BORDER AROUND THE SUBPLOT AREA, MAKING A GENERIC HEADING, SUPPRESSING
C PRINTED VALUES AT THE ENDS OF THE GRAPHS, CALLING THE CURVE
C AXES, PLOTS THEIR INCREMENT AND THEN CALLING A ROUTINE THAT LABELS THE
C THAT PLOTS ONLY A MARKER AND THEN CALLING A ROUTINE THAT LABELS THE
C MARKERS BY THE TYPE OF AIRCRAFT
C** SETCLR ('RED')
CALL FRAME
CALL XAXEND ('NCENDS')
CALL YAXEND ('NOENDS')
CALL GRAF (XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)
CALL RESET ('XTICKS')
CALL RESET ('YTIKS')
CALL CURVE (X,Y,8,-1)
CALL LABEL (X,Y)
CALL RESET ('HEIGHT')
C** SECONDARY AXIS IS DRAWN WITH APPROPRIATE TITLE AND VALUES AND THEN A
C PLOT OF THE NEW POINTS IS MADE AND THEIR POINTS LABELLED
C** CONTINUE
180 IF (TITAT.NE.0.0) GO TO 190
    GO TO 350
190 IF (TITAT.NE.1.0) GO TO 200
    CALL SWITCH (XANS2,3.0,XTWO,TEMP1,TEMP2,TEMP3)

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200 GO TO 230
    IF (ITALT.NE.2.0) GO TO 210
    CALL SWITCH (VANS2,4.,YTWO,TEMP1,TEMP2,TEMP3)
    GO TO 230
210 IF (ITALT.NE.3.0) GO TO 220
    CALL SWITCH (XANS2,5.,XTWO,TEMP1,TEMP2,TEMP3)
    GO TO 230
220 CONTINUE
    CALL SWITCH (VANS2,6.,YTWO,TEMP1,TEMP2,TEMP3)
    GO TO 230
230 CONTINUE
    CALL SETCLR ('GREEN')
    CALL MARKER (16,
    CALL CURVE (XTWO,YTWO,8,-1)
    CALL LABEL (XTWO,YTWO)
    CALL RESET ('HEIGHT')
    IF (ITALT.NE.1.) GO TO 240
    CALL LEGEND (IPAK,2.0,2.4,5)
    GO TO 270
240 IF (ITALT.NE.2.) GO TO 250
    CALL LEGEND (IPAK,2.0,2.5,5)
    GO TO 270
250 IF (ITALT.NE.3.) GO TO 260
    CALL LEGEND (IPAK,2.0,2.7,1)
    GO TO 270
260 IF (ITALT.NE.4.) GO TO 340
    CALL LEGEND (IPAK,2.0,2.7,5)
    GO TO 270
270 CONTINUE
    CALL RESET ('MARKER')
    GO TO 350
C*****
C THIS SECTION ALLOWS THE USER TO SELECT 2 SEPARATE GRAPHS ON THE
C SAME PAGE CN A HORIZONTAL PAGE FORMAT.
C*****
280 IF (ANS.NE.2.) GO TO 340
    WRITE (6,48)
    READ (5,*) ANS
    CALL FRICMS ('CLRCRN 6')
    IF (ANS.NE.2.0) GO TO 300
    WRITE (6,60)
    READ (5,*) ANS
    IF (ANS.NE.1.) GO TO 340
    CALL FRICMS ('CLRCRN 6')
    WRITE (6,41)
    WRITE (6,49)
    READ (5,*) X2ANS(1),Y2ANS(1),X2ANS(2),Y2ANS(2)

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C


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CALL FRTCMS ('CLRSCRN 6')
CALL PAGEA2D (11,8.5)
CALL HEIGHT (9,6)
CALL HESAG ('HELICOPTER DESIGN',-100,0.25,6.5)
CALL HESSET ('HEIGHT')
CALL MESSAG ('AE 4306/4900$,100,1.45,6.25)
CALL MESSAG ('KINDS,4,7.5,6.25)
CALL LENDCR (0)
DO 290 SETI=1,2
CALL SETCLR ('RED')
CALL PHYSOR (XPOS(1),YPOS(1))
CALL FRAMEA2D (3.85,6.)
CALL HEIGHT (14)
CALL SWITCH (X2ANS(1),1,X,XORIG,XSTP,XMAX)
CALL SWITCH (Y2ANS(1),2,Y,YORIG,YSTP,YMAX)
CALL XAXEND ('NCENDS')
CALL YAXEND ('NCENDS')
CALL GRAF ('XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)
CALL GRESET ('XTICKS')
CALL RRESET ('VTICKS')
CALL CURVE (X,Y,8,-1)
CALL LABEL (X,Y)
CALL LENDCR (0)
CONTINUE
CALL SETCLR ('BLACK')
GO TO 350
290 *****
C** THIS SECTION ALLOWS THE USER TO PUT 3 GRAPHS WITH A COMMON X AXIS *****
C** ON ONE VERTICAL PAGE PLACED ONE ON TOP OF THE OTHER. *****
C** *****
300 IF (ANS.NE.3.0) GO TO 320
WRITE (6,61)
READ (5,*) ANS
IF (ANS.NE.1.1) GO TO 340
CALL FRTCMS ('CLRSCRN 6')
WRITE (6,41)
WRITE (5,50)
READ (5,*) XANS,Y3ANS(1),Y3ANS(2),Y3ANS(3)
CALL FRTCMS ('CLRSCRN 6')
CALL HPRQT ('AUTO')
CALL HPRQT (5,11.)
CALL PAGEA2D (6,7.7)
CALL HEIGHT (3)
CALL HESAG ('HELICOPTER DESIGN',-100,0.8.)
CALL HESSET ('HEIGHT')
CALL MESSAG ('AE 4306/4900$,100,1.2,7.75)

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CALL STCRY (KINDS,4,5.25,7.75)
CALL LENDGR (0)
CALL SETCLR (GREEN)
CALL PHYSOR (XPOS(3),YPOS(3))
CALL AREAZD (7.2,5)
CALL FRAME (XANS,1.0,X,XORIG,XSTP,XMAX)
CALL SWITHT (10)
CALL SWITHT (Y3ANS(1),2.0,Y,YORIG,YSTP,YMAX)
CALL XAXEND (NENDS)
CALL YAXEND (NENDS)
CALL GRAF (XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)
CALL CURVE (X,Y,8,-1)
CALL RESET (HEIGHT)
CALL LABEL (X,Y)
CALL LENDGR (0)
DO 310 I=1,2
CALL PHYSOR (XPOS(I+3),YPOS(I+3))
CALL AREAZD (7.2,5)
CALL FRAME (XANS,7.0,X,XORIG,XSTP,XMAX)
CALL SWITHT (10)
CALL SWITHT (Y3ANS(I+1),2.0,Y,YORIG,YSTP,YMAX)
CALL XAXEND (NENDS)
CALL YAXEND (NENDS)
CALL XNCNUM (XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)
CALL GRAF (XTICKS)
CALL RESET (Y TICKS)
CALL CURVE (X,Y,8,-1)
CALL LABEL (X,Y)
CALL RENDGR (0)
CALL CONTINUE
CALL SETCLR (BLACK)
GO TO 350
310 *****
C** THIS SECTION ALLOWS THE USER TO PUT 4 GRAPHS ON A HORIZONTAL PAGE,
C** BASICALLY DIVIDE THE PAGE IN QUARTERS, WITH WHATEVER AXES WANTED.
C** *****
320 *****
IF (ANS.NE.4.0) GO TO 340
WRITE (6,62C)
READ (5,*) ANS
IF (ANS.NE.1) GO TO 340
CALL FRICMS (CLRSCRN 6)
WRITE (6,51C)

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READ (5,*) X4ANS(1),Y4ANS(1),X4ANS(2),Y4ANS(2),X4ANS(3),Y4ANS(3),X
14ANS(4),Y4ANS(4)
CALL FRICMS ('CLRSCRN 6')
CALL PAGE2D (11,8,5)
CALL AREAZD (9,5)
CALL HEIGHT (3)
CALL HESSET ('HELICOPTER DESIGN',-100,-.25,5.5)
CALL HESSET ('HEIGHT')
CALL HESSAG ('AE 4306/4900',100,.95,5.25)
CALL LSTORY (KINDS,4,7.5,5.25)
CALL ENDGR (0)
DO 330 I=1,4
CALL HYSOR (XPOS(I+5),YPOS(I+5))
CALL SETCLR ('RED')
CALL AREAZD (4,2,5)
CALL FRAME (10)
CALL HEIGHT (X4ANS(1),1,X,XORIG,XSTP,XMAX)
CALL SWITCH (Y4ANS(1),2,Y,YORIG,YSTP,YMAX)
CALL XAXEND ('NCENDS')
CALL YAXEND ('NOENDS')
CALL GRAF (XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)
CALL RESET ('XTICKS')
CALL RESET ('Y TICKS')
CALL CURVE (X,Y,8,-1)
CALL LABEL (X,Y)
CALL RESET ('HEIGHT')
CALL ENDGR (0)
CONTINUE
CALL SETCLR ('BLACK')
GO TO 350
330 *****
C THIS SECTION ALLOWS THE USER TO REMAIN WITHIN THE PROGRAM IF HE
C MAKES A MISTAKE IN ENTERING DATA.
C *****
340 CONTINUE
WRITE (6,52C)
READ (5,*) ANS
CALL FRICMS ('CLRSCRN 6')
IF (ANS.NE.1.) GO TO 360
GO TO 30
350 CONTINUE
CALL ENDPL (0)
C *****
C THIS SECTION IS USED TO ALLOW THE USER TO MAKE ADDITIONAL GRAPHS
C WITHOUT LEAVING THE PROGRAM AND HAVING TO REINITIATE DISPLA
C *****
WRITE (6,53C)

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READ (5,*) ANS
CALL FRICMS ('CLRS CRN 6')
IF (ANS.NE.1.) GO TO 360
CALL RESET ('ALL')
GO TO 30
CONTINUE
CALL DCNEPL
STOP
360
C*****
370
C*****
380
C*****
390
C*****
400
C*****
410
C*****
420
C*****
430
C*****

```

***** THIS IS AN INTERACTIVE PROGRAM FOR YOU TO BE ABLE TO, 2
 10H GRAPHICALLY DISPLAY, /, 36H THE VARIOUS DESIGN PARAMETERS THAT, 3
 20H YOU HAVE BEEN EXPOSED TO IN HELICOPTER, /, 15H DESIGN. PLEASE, 53H
 3 ENTER A NUMBER AS A RESPONSE TO THE QUESTIONS ASKED. /, /, /, 9X, 53H*
 4 ***** PLEASE FOLLOW THE INSTRUCTIONS *****
 1, 39H
 1, 39H
 1, 10H
 2, 20X, 27H
 3, 20X, 25H3
 1, 11H
 2, 10X, 32H
 3, 10X, 19H2
 15X, 22H2
 23, 5X, 32H4
 4, 5X, 27H9
 5, 5X, 26H10
 6, 5X, 27H12
 7, 5X, 27H13
 8, 5X, 27H14
 9, 5X, 27H15
 10, 5X, 27H16
 11, 5X, 27H17
 12, 5X, 27H18
 13, 5X, 27H19
 14, 5X, 27H20
 15, 5X, 27H21
 16, 5X, 27H22
 17, 5X, 27H23
 18, 5X, 27H24
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 458, 5X, 27H464
 459, 5X, 27H465
 460, 5X, 27H466
 461, 5X, 27H467
 462, 5X, 27H468
 463, 5X, 27H469
 464, 5X, 27H470
 465, 5X, 27H471
 466, 5X, 27H472
 467, 5X, 27H473
 468, 5X, 27H474
 469, 5X, 27H475
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 471, 5X, 27H477
 472, 5X, 27H478
 473, 5X, 27H479
 474, 5X, 27H480
 475, 5X, 27H481
 476, 5X, 27H482
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 479, 5X, 27H485
 480, 5X, 27H486
 481, 5X, 27H487
 482, 5X, 27H488
 483, 5X, 27H489
 484, 5X, 27H490
 485, 5X, 27H491
 486, 5X, 27H492
 487, 5X, 27H493
 488, 5X, 27H494
 489, 5X, 27H495
 490, 5X, 27H496
 491, 5X, 27H497
 492, 5X, 27H498
 493, 5X, 27H499
 494, 5X, 27H500
 495, 5X, 27H501
 496, 5X, 27H502
 497, 5X, 27H503
 498, 5X, 27H504
 499, 5X, 27H505
 500, 5X, 27H506
 501, 5X, 27H507
 502, 5X, 27H508
 503, 5X, 27H509
 504, 5X, 27H510
 505, 5X, 27H511
 506, 5X, 27H512
 507, 5X, 27H513
 508, 5X, 27H514
 509, 5X, 27H515
 510, 5X, 27H516
 511, 5X, 27H517
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 513, 5X, 27H519
 514, 5X, 27H520
 515, 5X, 27H521
 516, 5X, 27H522
 517, 5X, 27H523
 518, 5X, 27H524
 519, 5X, 27H525
 520, 5X, 27H526
 521, 5X, 27H527
 522, 5X, 27H528
 523, 5X, 27H529
 524, 5X, 27H530
 525, 5X, 27H531
 526, 5X, 27H532
 527, 5X, 27H533
 528, 5X, 27H534
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 531, 5X, 27H537
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 535, 5X, 27H541
 536, 5X, 27H542
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 538, 5X, 27H544
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 561, 5X, 27H567
 562, 5X, 27H568
 563, 5X, 27H569
 564, 5X, 27H570
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 566, 5X, 27H572
 567, 5X, 27H573
 568, 5X, 27H574
 569, 5X, 27H575
 570, 5X, 27H576
 571, 5X, 27H577
 572, 5X, 27H578
 573, 5X, 27H579
 574, 5X, 27H580
 575, 5X, 27H581
 576, 5X, 27H582
 577, 5X, 27H583
 578, 5X, 27H584
 579, 5X, 27H585
 580, 5X, 27H586
 581, 5X, 27H587
 582, 5X, 27H588
 583, 5X, 27H589
 584, 5X, 27H590
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 588, 5X, 27H594
 589, 5X, 27H595
 590, 5X, 27H596
 591, 5X, 27H597
 592, 5X, 27H598
 593, 5X, 27H599
 594, 5X, 27H600
 595, 5X, 27H601
 596, 5X, 27H602
 597, 5X, 27H603
 598, 5X, 27H604
 599, 5X, 27H605
 600, 5X, 27H606
 601, 5X, 27H607
 602, 5X, 27H608
 603, 5X, 27H609
 604, 5X, 27H610
 605, 5X, 27H611
 606, 5X, 27H612
 607, 5X, 27H613
 608, 5X, 27H614
 609, 5X, 27H615
 610, 5X, 27H616
 611, 5X,


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560 6X,1HX,1
    FORMAT (//6X,42H THIS IS THE TYPE FORMAT THAT YOU SELECTED,16H--I
1S IT CORRECT?/,6X,59H
2  //,30X,6HI- YES,7,30X,5H2- NO,7,7,19X,30H-
3  I,28X,1HI,7,19X,1HI,28X,1HI,19X,1HI,28X,1HI,7,17X,3HV
4  19X,30H-
5  SECONDARY X,/,30X,9HPRIMARY X,/,29X,11H
6  FORMAT (//6X,42H THIS IS THE TYPE FORMAT THAT YOU SELECTED,16H--IS
570 1S IT CORRECT?/,6X,59H
2  //,30X,6HI- YES,7,30X,5H2- NO,7,7,15X,44HS
3  R,1,36X,1HI,7,15X,7HD,1,15X,7HE P,1,36X,1HI,/,15X,7HC
55X,7HD A,1,36X,1HI,/,15X,7HA R,1,36X,1HI,/,15X,7HR M,1,36X,1HI,/,1
6HI,/,15X,7HY I,36X,1HI,/,15X,7H Y,1,36X,1HI,/,15X,44HV
7  FORMAT (//6X,42H THIS IS THE TYPE FORMAT THAT YOU SELECTED,16H--IS
580 1S IT CORRECT?/,6X,59H
2  //,30X,6HI- YES,7,30X,5H2- NO,7,7,26X,15H
3  I,7,26X,1HI,1,13X,1HI,/,26X,1HI,13X,1HI,7,24X,3HV
4  1,13X,1HI,/,26X,1HI,13X,1HI,/,26X,1HI,13X,1HI,7,24X,3HV
5,26X,1HI,1,13X,1HI,/,26X,1HI,13X,1HI,/,26X,1HI,13X,1HI,/,
6  9HPRIMARY X,/,27X,11HSECONDARY X,/,26X,15H
590 1S IT CORRECT?/,6X,59H
2  //,30X,6HI- YES,7,30X,5H2- NO,7,7,22X,21HS
3  HD,1,13X,1HI,/,22X,7HE P,1,13X,1HI,/,22X,7HC R,1,13X,1HI,/,22X,7
4  22X,7HA R,1,13X,1HI,/,22X,7HN M,1,13X,1HI,/,22X,7HD A,1,13X,1HI,/,
5,1HI,/,22X,7H Y,1,13X,1HI,/,22X,7HR Y,1,13X,1HI,/,22X,7HY
6  1HX,1
600 1S IT CORRECT?/,6X,59H
2  //,30X,6HI- YES,7,30X,5H2- NO,7,7,19X,34H
3  8H
4  19X,1HI,2X,1HI,6X,1HI,/,19X,1HI,32X,1HI,/,15X,1HI,6X,8H
5  19X,1HI,2X,1HI,6X,1HI,/,19X,1HI,6X,1HI,6X,1HI,6X,1HI,4X,1HI,6X
6  6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,3X,1HI,4HV,1,1,6X,1HI,3X,4HV,2,1,6X,1HI,
7  4X,1HI,/,19X,1HI,6X,1HI,6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,6X,1
8  HI,6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,6X,8H
9  4X,1HI,/,19X,1HI,6X,8H X1,6X,8H X2,4X,1HI,/,19X,34H
610 1S IT CORRECT?/,6X,59H
2  //,30X,6HI- YES,7,30X,5H2- NO,7,7,26X,19H
3  8H
4  19X,1HI,2X,1HI,6X,1HI,/,19X,1HI,32X,1HI,/,15X,1HI,6X,8H
5  19X,1HI,2X,1HI,6X,1HI,/,19X,1HI,6X,1HI,6X,1HI,6X,1HI,4X,1HI,6X
6  6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,3X,1HI,4HV,1,1,6X,1HI,3X,4HV,2,1,6X,1HI,
7  4X,1HI,/,19X,1HI,6X,1HI,6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,6X,1
8  HI,6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,6X,8H
9  4X,1HI,/,19X,1HI,6X,8H X1,6X,8H X2,4X,1HI,/,19X,34H
1S IT CORRECT?/,6X,59H
2  //,30X,6HI- YES,7,30X,5H2- NO,7,7,26X,19H
3  8H
4  19X,1HI,2X,1HI,6X,1HI,/,19X,1HI,32X,1HI,/,15X,1HI,6X,8H
5  19X,1HI,2X,1HI,6X,1HI,/,19X,1HI,6X,1HI,6X,1HI,6X,1HI,4X,1HI,6X
6  6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,3X,1HI,4HV,1,1,6X,1HI,3X,4HV,2,1,6X,1HI,
7  4X,1HI,/,19X,1HI,6X,1HI,6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,6X,1
8  HI,6X,1HI,6X,1HI,4X,1HI,/,19X,1HI,6X,8H
9  4X,1HI,/,19X,1HI,6X,8H X1,6X,8H X2,4X,1HI,/,19X,34H

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6X, 1H 1.9X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 1H, 26X, 6
7H, 1H 1.9X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 1H, 26X, 6
8, 9X, 1H, 7X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 1H, 26X, 6
9, 1H, 7X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 1H, 26X, 6
1 IT CORRECT? 6X, 59H
2
3
4X, 8H 1.9X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 1H, 26X, 6
5, 1H, 7X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 1H, 26X, 6
6 1.9X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 1H, 26X, 6
7, 5X, 1H, 7X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 6
8H, 1H, 7X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 6
9H X2 5X, 1H, 7X, 1H, 2X, 1H, 26X, 1H, 4X, 1H 2X, 1H, 26X, 1H, 26X, 6
END

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*****
C DATA USED THROUGHOUT THE PROGRAM FOR THE COMMON VARIABLES SO THAT
C ADDITIONAL FILECEFS DO NOT HAVE TO BE USED. DATA OBTAINED HEREIN
C IS ONLY THAT OF THE 30 PARAMETERS USED IN COMPARISON
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BLOCK DATA
REAL R(8), B(8), BTR(8), HT(8), RPM(8), RPMTR(8), C(8), CTR(8)
REAL RS(8), TWS(8), TWS(8), FV(8), VM(8), CDO(8), CDO(8), DL(8)
REAL HOVOGE(8), LT(8), OMT(8), LWT(8), FWT(8), MGV(8)
COMMON /C1/ R, B, BTR, HT, RPM, RPMTR, C, CTR, RS, RSTR, TWS, TWS(8), CDO
1, CDO(8), CL, WCT, LGH, FV, VM, RNG, RC, HOVOGE, HOVOGE(8), LT, OMT, FWT, MGV
C THE DATA IS LISTED IN THE FOLLOWING SEQUENTIAL MANNER FOR EASY
C MANIPULATION WITHIN THE DISPLA PROGRAM AND FOR CONSISTENT MARKER
C IDENTIFICATION:
/ AH64, OH6A, SH3H, S76, UH60A, CH54B, CH53D, CH54E/

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DATA R/24., 16., 31., 22., 26., 8., 36., 36., 1., 38., 5/
DATA B/4., 6., 4., 3., 5., 3., 4., 5., 8., 8., 10./
DATA BTR/4., 2., 7., 5., 7., 4., 10., 1., 2., 258./
DATA HT/12., 6., 4., 70., 203., 1243., 151., 91., 28., 172., 44./
DATA RPM/28., 5., 7., 1., 52., 1., 54., 81., 23., 3., 4., 25., 6., 45., 8., 53./
DATA C/1., 75., 5., 7., 1., 52., 1., 54., 81., 23., 3., 4., 25., 6., 45., 8., 53./
DATA CTR/1., 75., 5., 7., 1., 52., 1., 54., 81., 23., 3., 4., 25., 6., 45., 8., 53./
DATA RS/18., 81., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1./
DATA RSTR/18., 81., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1./
DATA TWS/18., 81., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1./
DATA TWS(8)/18., 81., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1./
DATA CDO/18., 81., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1./
DATA CDO(8)/18., 81., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1., 9., 1./
DATA DL/8., 1., 4., 6., 8., 6., 96., 6., 58., 8., 95., 10., 3., 15., 0./

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REAL RS(8), RSTR(8), TWST(8), TWSTTR(8), CDO(8), CDOTR(8), DL(8)
REAL WDT(8), LGH(8), FH(8), FV(8), VM(8), RNG(8), RC(8), HOVIGE(8)
REAL HOVOGE(8), LT(8), OWT(8), LWT(8), FWT(8), MGW(8), X(8)
REAL XORIG, XSTP, XMAX, Z, OPTION
INTEGER I
COMMON /C1/ R, RTR, B, BTR, HT, RPM, RPMTR, C, CTR, RS, RSTR, TWST, TWSTTR, CDO
1, CDOTR, CL, WCT, LGH, FH, FV, VM, RNG, RC, HOVIGE, HOVOGE, LT, OWT, LWT, FWT, MGW
CALL XAXEND (NOENDS)
CALL YAXEND (NOENDS)
CALL YAXANG (0)
IF (Z, NE, 1) GO TO 90
DO 10 I=1, 8
X(I)=R(I)
CONTINUE
XORIG=15.
XSTP=5.
XMAX=4.5
IF (OPTION, NE, 1) GO TO 20
CALL XNAME (MAIN ROTOR RADIUS (FT)$, 100)
GO TO 2710
IF (OPTION, NE, 2) GO TO 30
CALL YTICKS (5)
CALL YNAME (MAIN ROTOR RADIUS (FT)$, 100)
GO TO 2710
IF (OPTION, NE, 3) GO TO 40
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS (XORIG, XSTP, XMAX, 9., MAIN ROTOR RADIUS (FT)$,
100, 0., -.75,
XTICKS)
1 CALL RESET
GO TO 2710
IF (OPTION, NE, 4) GO TO 50
CALL YTICKS (5)
CALL YREVTK
CALL YGRAXS (XORIG, XSTP, XMAX, 6., MAIN ROTOR RADIUS (FT)$,
100, -1., 0.,
YTICKS)
1 CALL RESET
GO TO 2710
IF (OPTION, NE, 5) GO TO 60
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS (XORIG, XSTP, XMAX, 6.5, MAIN ROTOR RADIUS (FT)$,
100, 0., -.75,
XTICKS)
1 CALL RESET
GO TO 2710
IF (OPTION, NE, 6) GO TO 70
CALL YTICKS (5)

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1 CALL YREVTK (XORIG,XSTP,XMAX,8.,'MAIN ROTOR RADIUS (FT)',$
CALL YGRAXS (100,-1,15,0.)
CALL RESET (YTIKCS)
GO TO 2710
IF (OPTION,NE,7.) GO TO 80
CALL XTIKCS (5)
CALL XNAME ('',1)
GO TO 2710
CONTINUE
GO TO 2700
IF (Z,NE,2.) GO TO 180
DO 100 I=1,E
X(I)=RTR(I)
CONTINUE
XORIG=0.
XSTP=2.
XMAX=12.
IF (OPTION,NE,1.) GO TO 110
CALL XTIKCS (5)
CALL XNAME ('TAIL ROTOR RADIUS (FT)',$,100)
GO TO 2710
IF (OPTION,NE,2.) GO TO 120
CALL YTIKCS (2)
CALL YNAME ('TAIL ROTOR RADIUS (FT)',$,100)
GO TO 2710
IF (OPTION,NE,3.) GO TO 130
CALL XTIKCS (2)
CALL XREVTK
CALL XGRAXS (XORIG,XSTP,XMAX,9.,'TAIL ROTOR RADIUS (FT)',$,
100,0.,-.75)
1 GO TO 2710
IF (OPTION,NE,4.) GO TO 140
CALL YTIKCS (2)
CALL YREVTK
CALL YGRAXS (XORIG,XSTP,XMAX,6.,'TAIL RCTOR RADIUS (FT)',$,
100,-1,0.)
1 GO TO 2710
IF (OPTION,NE,5.) GO TO 150
CALL XTIKCS (2)
CALL XREVTK
CALL XGRAXS (XORIG,XSTP,XMAX,6.5,'TAIL ROTOR RADIUS (FT)',$,
100,0.,-.75)
1 GO TO 2710
IF (OPTION,NE,6.) GO TO 160
CALL YTIKCS (2)
CALL YREVTK
CALL YGRAXS (XORIG,XSTP,XMAX,8.,'TAIL ROTOR RADIUS (FT)',$,

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100,-1.15,0.)
1 GO TO 2710
IF (OPTION,NE.7.) GO TC 170
CALL XTICKS(2)
CALL XNAME(1,1)
GO TO 2710
CONTINUE
GO TO 2700
IF (Z,NE.3.) GO TO 270
DO 190 I=1,E
X(I)=8(I)
CONTINUE
XORIG=0.
XSTP=1.
XMAX=9.
IF (OPTION,NE.1.) GO TO 200
CALL XINTAX
CALL XINTAX
GO TO 2710
IF (OPTION,NE.2.) GO TC 210
CALL YNAME
CALL YINTAX
GO TO 2710
IF (OPTION,NE.3.) GO TO 220
CALL XREVTK
CALL XGRAXS (XORIG,XSTP,XMAX,9,'BLADES$',100,0,--,75)
1 CALL XINTAX
GO TO 2710
IF (OPTION,NE.4.) GO TC 230
CALL YREVTK
CALL YGRAXS (XORIG,XSTP,XMAX,6,'BLADES$',100,-1,0,0.)
1 CALL YINTAX
GO TO 2710
IF (OPTION,NE.5.) GO TC 240
CALL XREVTK
CALL XGRAXS (XORIG,XSTP,XMAX,6.5,'BLADES$',100,0,--,75)
1 CALL XINTAX
GO TO 2710
IF (OPTION,NE.6.) GO TO 250
CALL YREVTK
CALL YGRAXS (XORIG,XSTP,XMAX,8,'BLADES$',100,-1.15,0.)
1 CALL YINTAX
GO TO 2710
IF (OPTION,NE.7.) GO TO 260

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260      CALL XNAME (' ',1)
      GO TO 2710
      CONTINUE
270      GO TO 2700
      IF (Z.NE.4.) GO TO 360
      DO 280 I=1,5
      X(I)=BTR(I)
      CONTINUE
      XORIG=0.
      XSTP=1.
      XMAX=6.
      IF (OPTION.NE.1.) GO TO 290
      CALL XNAME ('NUMBER TAIL ROTOR BLADES$',100)
      CALL XINTAX
      GO TO 2710
290      IF (OPTION.NE.2.) GO TO 300
      CALL YNAME ('NUMBER TAIL ROTOR BLADES$',100)
      CALL YINTAX
      GO TO 2710
300      IF (OPTION.NE.3.) GO TO 310
      CALL XREVTK
      CALL XGRAXS
      (XORIG,XSTP,XMAX,9,'NUMBER TAIL ROTOR BLADES$',100,0.,-.75)
1
      CALL XINTAX
      GO TO 2710
310      IF (OPTION.NE.4.) GO TO 320
      CALL YREVTK
      CALL YGRAXS
      (XORIG,XSTP,XMAX,6,'NUMBER TAIL ROTOR BLADES$',100,-1.,0.)
1
      CALL YINTAX
      GO TO 2710
320      IF (OPTION.NE.5.) GO TO 330
      CALL XREVTK
      CALL XGRAXS
      (XORIG,XSTP,XMAX,6.5,'NUMBER TAIL ROTOR BLADES$',100,0.,-.75)
1
      CALL XINTAX
      GO TO 2710
330      IF (OPTION.NE.6.) GO TO 340
      CALL YREVTK
      CALL YGRAXS
      (XORIG,XSTP,XMAX,8,'NUMBER TAIL ROTOR BLADES$',100,-1.15,0.)
1
      CALL YINTAX
      GO TO 2710
340      IF (OPTION.NE.7.) GO TO 350
      CALL XNAME (' ',1)
      GO TO 2710
350      CONTINUE
      GO TO 2730

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360 IF (Z.NE.5.) GO TO 450
DO 370 I=1,8
X(I)=HT(I)
CONTINUE
XORIG=0.
XSTP=5.
XMAX=20.
IF (OPTION.NE.1.) GO TO 380
CALL XTICKS (5)
CALL XNAME ('HEIGHT OF ROTOR SYSTEM (FT)',100)
GO TO 2710
380 IF (OPTION.NE.2.) GO TO 390
CALL YTICKS (5)
CALL YNAME ('HEIGHT OF ROTOR SYSTEM (FT)',100)
GO TO 2710
390 IF (OPTION.NE.3.) GO TO 400
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS
1 GO TO 2710
400 IF (OPTION.NE.4.) GO TO 410
CALL YTICKS (5)
CALL YREVTK
CALL YGRAXS
1 GO TO 2710
410 IF (OPTION.NE.5.) GO TO 420
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS
1 GO TO 2710
420 IF (OPTION.NE.6.) GO TO 430
CALL YTICKS (5)
CALL YREVTK
CALL YGRAXS
1 GO TO 2710
430 IF (OPTION.NE.7.) GO TO 440
CALL XTICKS (5)
CALL XNAME ('',1)
GO TO 2710
440 CONTINUE
GO TO 2700
450 IF (Z.NE.6.) GO TO 540
DO 460 I=1,8
X(I)=RPM(I)

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460 CONTINUE
XORIG=0.
XSTP=50.
XMAX=600.
CALL XINTAX
IF (OPTICN, NE, 1.) GO TO 470
CALL XTICKS (5)
CALL XNAME ('MAIN ROTOR SPEED (RPM)$', 100)
CALL XINTAX
GO TO 2710
IF (OPTICN, NE, 2.) GO TO 480
CALL YTICKS (5)
CALL YNAME ('MAIN ROTOR SPEED (RPM)$', 100)
CALL YINTAX
GO TO 2710
IF (OPTICN, NE, 3.) GO TO 490
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS
1 CALL XINTAX
GO TO 2710
IF (OPTICN, NE, 4.) GO TO 500
CALL YTICKS (5)
CALL YREVTK
CALL YGRAXS
1 CALL YINTAX
GO TO 2710
IF (OPTICN, NE, 5.) GO TO 510
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS
1 CALL XINTAX
GO TO 2710
IF (OPTICN, NE, 6.) GO TO 520
CALL YTICKS (5)
CALL YREVTK
CALL YGRAXS
1 CALL YINTAX
GO TO 2710
IF (OPTICN, NE, 7.) GO TO 530
CALL XTICKS (5)
CALL XNAME ('', 1)
GO TO 2710

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530 CONTINUE
540 GO TO 2700
550 IF (Z.NE.7.) GO TO 630
DO 550 I=1,8
X(I)=RPMTR(I)
CONTINUE
XSTP=500.
XMAX=3500.
IF (OPTION.NE.1.) GO TO 560
CALL XTICKS (5)
CALL XNAME ('TAIL ROTOR SPEED (RPM)$',100)
CALL XINTAX
GO TO 2710
560 IF (OPTION.NE.2.) GO TO 570
CALL YTICKS (5)
CALL YNAME ('TAIL ROTOR SPEED (RPM)$',100)
CALL YINTAX
GO TO 2710
570 IF (OPTION.NE.3.) GO TO 580
CALL XTICKS (5)
CALL XREVTX
CALL XGRAXS
1 CALL XINTAX
GO TO 2710
580 IF (OPTION.NE.4.) GO TO 590
CALL YTICKS (5)
CALL YREVTX
CALL YGRAXS
1 CALL YINTAX
GO TO 2710
590 IF (OPTION.NE.5.) GO TO 600
CALL XTICKS (5)
CALL XREVTX
CALL XGRAXS
1 CALL XINTAX
GO TO 2710
600 IF (OPTION.NE.6.) GO TO 610
CALL YTICKS (5)
CALL YREVTX
CALL YGRAXS
1 CALL YINTAX
GO TO 2710
610 IF (OPTION.NE.7.) GO TO 620
CALL XTICKS (5)
CALL XNAME ('TAIL ROTOR SPEED (RPM)$',100,0,-.75)
CALL XINTAX
GO TO 2710

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620      CALL XTICKS (5)
        CALL XNAME (I,1)
        GO TO 2710
        CONTINUE
630      IF (Z.NE.8.) GO TO 720
        DO 640 I=1,E
        X(I)=C(I)
        CONTINUE
        XORIG=0.0
        XSTP=0.5
        XMAX=3.0
        IF (OPTION.NE.1.) GO TO 650
        CALL XTICKS (5)
        CALL XNAME (MAIN ROTOR BLADE CHORD(FT),100)
        GO TO 2710
650      IF (OPTION.NE.2.) GO TO 660
        CALL YTIKKS (5)
        CALL YNAME (MAIN ROTOR BLADE CHORD(FT),100)
        GO TO 2710
660      IF (OPTION.NE.3.) GO TO 67C
        CALL XTICKS (5)
        CALL XREVTK
        CALL XGRAXS
        1 GO TO 2710
        IF (OPTION.NE.4.) GO TO 680
        CALL YTIKKS (5)
        CALL YREVTK
        CALL YGRAXS
        1 GO TO 2710
        IF (OPTION.NE.5.) GO TO 690
        CALL XTICKS (5)
        CALL XREVTK
        CALL XGRAXS
        1 GO TO 2710
        IF (OPTION.NE.6.) GO TO 700
        CALL YTIKKS (5)
        CALL YREVTK
        CALL YGRAXS
        1 GO TO 2710
        IF (OPTION.NE.7.) GO TO 710
        CALL XTICKS (5)
        CALL XNAME (I,1)
        GO TO 2710

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```

710 CONTINUE
720 GO TO 2700
    IF (Z.NE.9.) GO TO 810
    DO 730 I=1,5
    X(I)=CTR(I)
730 CONTINUE
    XORIG=0.3
    XSTP=0.1
    XMAX=1.5
    IF (OPTION.NE.1.) GO TO 740
    CALL XTICKS (5)
    CALL XNAME ('TAIL ROTOR BLADE CHORD(FT)',100)
    GO TO 2710
740 IF (OPTION.NE.2.) GO TO 750
    CALL YTICKS (5)
    CALL YNAME ('TAIL ROTOR BLADE CHORD(FT)',100)
    GO TO 2710
750 IF (OPTION.NE.3.) GO TO 760
    CALL XTICKS (5)
    CALL XREVTK
    CALL XGRAXS
    1 GO TO 2710
    IF (OPTION.NE.4.) GO TO 770
    CALL YTICKS (5)
    CALL YREVTK
    CALL YGRAXS
    1 GO TO 2710
    IF (OPTION.NE.5.) GO TO 780
    CALL XTICKS (5)
    CALL XREVTK
    CALL XGRAXS
    1 GO TO 2710
    IF (OPTION.NE.6.) GO TO 790
    CALL YTICKS (5)
    CALL YREVTK
    CALL YGRAXS
    1 GO TO 2710
    IF (OPTION.NE.7.) GO TO 800
    CALL XTICKS (5)
    CALL XNAME ('',1)
    GO TO 2710
800 CONTINUE
    GO TO 2700
810 IF (Z.NE.10.) GO TO 900

```

| | |
|-----|---|
| 820 | DO 820 I=1,E X(I)=RS(I) CONTINUE XORIG=10. XSIP=5. XMAX=40. IF (OPTION,NE,1.) GO TO 830 CALL XTICKS (5) CALL XNAME ('MAIN ROTOR BLADE SPAN(FT)',100) GO TO 2710 IF (OPTION,NE,2.) GO TO 840 CALL YTICKS (5) CALL YNAME ('MAIN ROTOR BLADE SPAN(FT)',100) GO TO 2710 IF (OPTION,NE,3.) GO TO 850 CALL XTICKS (5) CALL XREVTK CALL XGRAXS (XORIG,XSIP,XMAX,9.,SPAN(FT)',100,0.,-.75) 1 GO TO 2710 IF (OPTION,NE,4.) GO TO 860 CALL YTICKS (5) CALL YREVTK CALL YGRAXS (XORIG,XSIP,XMAX,6.,SPAN(FT)',100,-1.,0.) 1 GO TO 2710 IF (OPTION,NE,5.) GO TO 870 CALL XTICKS (5) CALL XREVTK CALL XGRAXS (XORIG,XSIP,XMAX,6.5,SPAN(FT)',100,0.,-.75) 1 GO TO 2710 IF (OPTION,NE,6.) GO TO 880 CALL YTICKS (5) CALL YREVTK CALL YGRAXS (XORIG,XSIP,XMAX,8.,SPAN(FT)',100,-1.,5,0.) 1 GO TO 2710 IF (OPTION,NE,7.) GO TO 890 CALL XTICKS (5) CALL XNAME ('',1) GO TO 2710 CONTINUE GO TO 2700 IF (2,NE,11.) GO TO 990 DO 910 I=1,E X(I)=RSTR(I) CONTINUE |
| 830 | |
| 840 | |
| 850 | |
| 860 | |
| 870 | |
| 880 | |
| 890 | |
| 900 | |
| 910 | |

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XORIG=0.
XSTP=1.
XMAX=1.
IF (OPTION, NE, 1.) GO TO 920
CALL XTICKS (5)
CALL XNAME (,TAIL ROTOR BLADE SPAN(FT)$,100)
GO TO 2710
920 IF (OPTION, NE, 2.) GO TC 930
CALL YTICKS (5)
CALL YNAME (,TAIL ROTOR BLADE SPAN(FT)$,100)
GO TO 2710
930 IF (OPTION, NE, 3.) GO TO 940
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS
1 GO TO 2710
IF (OPTION, NE, 4.) GO TO 950
CALL YTICKS (5)
CALL YREVTK
CALL YGRAXS
1 GO TO 2710
950 IF (OPTION, NE, 5.) GO TC 960
CALL XTICKS (5)
CALL XREVTK
CALL XGRAXS
1 GO TO 2710
960 IF (OPTION, NE, 6.) GO TC 970
CALL YTICKS (5)
CALL YREVTK
CALL YGRAXS
1 GO TO 2710
970 IF (OPTION, NE, 7.) GO TO 980
CALL XTICKS (5)
CALL XNAME (, ,1)
GO TO 2710
980 CONTINUE
GO TO 2700
990 IF (Z, NE, 12.) GO TO 1080
DO 1000 I=1,8
X(I)=TWST(I)
CONTINUE
XORIG=-5.
XSTP=-5.
XMAX=-20.
1000

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1010 IF (OPTION,NE,1.) GO TO 1010
      CALL XTICKS (5)
      CALL XNAME ('MAIN ROTOR BLADE TWIST(DEG)$',100)
      GO TO 2710
      IF (OPTION,NE,2.) GO TC 1020
      CALL YTICKS (5)
      CALL YNAME ('MAIN ROTOR BLADE TWIST(DEG)$',100)
      GO TO 2710
      IF (OPTION,NE,3.) GO TO 1030
      CALL XTICKS (5)
      CALL XREVTK
      CALL XGRAXS
      1 GO TO 2710
      (XORIG,XSTP,XMAX,9,TWIST(DEG)$,100,0.,-.75)
      IF (OPTION,NE,4.) GO TC 1040
      CALL YTICKS (5)
      CALL YREVTK
      CALL YGRAXS
      1 GO TO 2710
      (XORIG,XSTP,XMAX,6,TWIST(DEG)$,100,-1.,0.)
      IF (OPTION,NE,5.) GO TG 1050
      CALL XTICKS (5)
      CALL XREVTK
      CALL XGRAXS
      1 GO TO 2710
      (XORIG,XSTP,XMAX,6.5,TWIST(DEG)$,100,0.,-.75)
      IF (OPTION,NE,6.) GO TO 1060
      CALL YTICKS (5)
      CALL YREVTK
      CALL YGRAXS
      1 GO TO 2710
      (XORIG,XSTP,XMAX,8,TWIST(DEG)$,100,-1.15,0.)
      IF (OPTION,NE,7.) GO TO 1070
      CALL XTICKS (5)
      CALL XNAME ('',1)
      GO TO 2710
      CONTINUE
      1070 GO TO 2700
      IF (2,NE,13.) GO TO 1170
      DO 1090 I=1,8
      XI(I)=TWSTTR(I)
      CONTINUE
      XORIG=5.
      XSTP=-5.
      XMAX=-2.
      IF (OPTION,NE,1.) GO TO 1100
      CALL XTICKS (5)
      CALL XNAME ('TAIL ROTOR BLADE TWIST(DEG)$',100)

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1100      GO TO 2710
          IF (OPTION,NE,2.) GO TO 1110
          CALL YTICKS (5)
          CALL YNAME ('TAIL ROTOR BLADE TWIST(DEG)$',100)
          GO TO 2710
1110      IF (OPTION,NE,3.) GO TO 1120
          CALL XTICKS (5)
          CALL XREVTK
          CALL XGRAXS (XORIG,XSTP,XMAX,9.,TWIST(DEG)$,100,0.,-.75)
          1 GO TO 2710
1120      IF (OPTION,NE,4.) GO TO 1130
          CALL YTICKS (5)
          CALL YREVTK
          CALL YGRAXS (XORIG,XSTP,XMAX,6.,TWIST(DEG)$,100,-1.,0.)
          1 GO TO 2710
1130      IF (OPTION,NE,5.) GO TO 1140
          CALL XTICKS (5)
          CALL XREVTK
          CALL XGRAXS (XORIG,XSTP,XMAX,6.5,TWIST(DEG)$,100,0.,-.75)
          1 GO TO 2710
1140      IF (OPTION,NE,6.) GO TO 1150
          CALL YTICKS (5)
          CALL YREVTK
          CALL YGRAXS (XORIG,XSTP,XMAX,8.,TWIST(DEG)$,100,-1.15,0.)
          1 GO TO 2710
1150      IF (OPTION,NE,7.) GO TO 1160
          CALL XTICKS (5)
          CALL XNAME ('',1)
          GO TO 2710
1160      CONTINUE
1170      GO TO 2700
          IF (Z,NE,14.) GO TO 1260
          DO 1180 I=1,8
          X(I)=CCCC(I)
          CONTINUE
          XORIG=.007
          XSTP=.001
          XMAX=.011
          IF (OPTION,NE,1.) GO TO 1190
          CALL XTICKS (5)
          CALL XNAME ('PROFILE DRAG MAIN ROTORS$',100)
          GO TO 2710
1190      IF (OPTION,NE,2.) GO TO 1200
          CALL YTICKS (5)

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1200      CALL YNAME ('PROFILE DRAG MAIN ROTCR$',100)
        GO TO 2710
        IF (OPTION,NE,3.) GO TC 1210
        CALL XTICKS$ (5)
        CALL XREVTK
        CALL XGRAXS (XORIG,XSTP,XMAX,9.,
                     'PROFILE DRAG MAIN ROTCR$',100,0.,-.75)
1      GO TO 2710
1210      IF (OPTION,NE,4.) GO TO 1220
        CALL XTICKS$ (5)
        CALL YREVTK
        CALL YGRAXS (XORIG,XSTP,XMAX,6.,
                     'PROFILE DRAG MAIN ROTCR$',100,-1.,0.)
1      GO TO 2710
1220      IF (OPTION,NE,5.) GO TO 1230
        CALL XTICKS$ (5)
        CALL XREVTK
        CALL XGRAXS (XORIG,XSTP,XMAX,6.5,
                     'PROFILE DRAG MAIN ROTCR$',100,0.,-.75)
1      GO TO 2710
1230      IF (OPTION,NE,6.) GO TO 1240
        CALL XTICKS$ (5)
        CALL YREVTK
        CALL YGRAXS (XORIG,XSTP,XMAX,8.,
                     'PROFILE DRAG MAIN ROTCR$',100,-1.15,0.)
1      GO TO 2710
1240      IF (OPTION,NE,7.) GO TC 1250
        CALL XTICKS$ (5)
        CALL XNAME ('',1)
        GO TO 2710
        CONTINUE
1250      GO TO 2700
1260      IF (Z,NE,15.) GO TO 1350
        DO 1270 I=1,8
        X(I)=CCCTR(I)
        CONTINUE
        XORIG=.007
        XSTP=.002
        XMAX=.017
        IF (OPTION,NE,1.) GO TO 1280
        CALL XTICKS$ (2)
        CALL XNAME ('PROFILE DRAG TAIL ROTCR$',100)
        GO TO 2710
1280      IF (OPTION,NE,2.) GO TO 1290
        CALL XTICKS$ (2)
        CALL YNAME ('PROFILE DRAG TAIL ROTCR$',100)
        GO TO 2710
1290      IF (OPTION,NE,3.) GO TO 1300

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CALL XTICKS (2)
CALL XREVTK
CALL XGRAXS
1 GO TO 2710
1300 IF (OPTION,NE,4.) GO TC 1310
CALL XTICKS (2)
CALL YREVTK
CALL YGRAXS
1 GO TO 2710
1310 IF (OPTION,NE,5.) GO TO 1320
CALL XTICKS (2)
CALL XREVTK
CALL XGRAXS
1 GO TO 2710
1320 IF (OPTION,NE,6.) GO TO 1330
CALL XTICKS (2)
CALL YREVTK
CALL YGRAXS
1 GO TO 2710
1330 IF (OPTION,NE,7.) GO TO 1340
CALL XTICKS (2)
CALL XNAME ('',1)
GO TO 2710
1340 CONTINUE
GO TO 2700
1350 IF (Z,NE,16.) GO TO 1440
DO 1360 I=1,8
X(I)=DL(I)
1360 CONTINUE
XORIG=4.
XSTP=1.
XMAX=16.
IF (OPTION,NE,1.) GO TO 1370
CALL XTICKS (2)
CALL XNAME ('DISC LOADING$',100)
GO TO 2710
1370 IF (OPTION,NE,2.) GO TO 1380
CALL XTICKS (2)
CALL YNAME ('DISC LOADING$',100)
GO TO 2710
1380 IF (OPTION,NE,3.) GO TO 1390
CALL XTICKS (2)
CALL XREVTK
CALL XGRAXS (XORIG,XSTP,XMAX,9.,

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1390      1 GO TO 2710      'DISC LOADING$,100,0.,--.75)
        IF (OPTICN,NE,4.) GO TO 1400
        CALL YTTICKS (2)
        CALL YREVTK
        CALL YGRAXS (XORIG,XSTP,XMAX,6.,100,-1.,0.)
        'DISC LOADING$,100,-1.,0.)
1400      1 GO TO 2710
        IF (OPTICN,NE,5.) GO TO 1410
        CALL XTTICKS (2)
        CALL XREVTK
        CALL XGRAXS (XORIG,XSTP,XMAX,6.5,
        'DISC LOADING$,100,0.,--.75)
1410      1 GO TO 2710
        IF (OPTICN,NE,6.) GO TO 1420
        CALL YTTICKS (2)
        CALL YREVTK
        CALL YGRAXS (XORIG,XSTP,XMAX,8.,100,-1.15,0.)
1420      1 GO TO 2710
        IF (OPTICN,NE,7.) GO TO 1430
        CALL XTTICKS (2)
        CALL XNAME ('',1)
        GO TO 2710
1430      CONTINUE
        GO TO 2700
1440      IF (Z,NE,17.) GO TO 1530
        DO 1450 I=1,8
        X(I)=WDI(I)
        CONTINUE
1450      XORIG=2.
        XSTP=1.
        XMAX=10.
        IF (OPTICN,NE,1.) GO TO 1460
        CALL XTTICKS (2)
        CALL XNAME ('FUSELAGE WIDTH (FT)$',100)
        GO TO 2710
1460      IF (OPTICN,NE,2.) GO TO 1470
        CALL YTTICKS (2)
        CALL YNAME ('FUSELAGE WIDTH (FT)$',100)
        GO TO 2710
1470      IF (OPTICN,NE,3.) GO TO 1480
        CALL XTTICKS (2)
        CALL XREVTK
        CALL XGRAXS (XORIG,XSTP,XMAX,9.,100,0.,--.75)
1480      1 GO TO 2710
        IF (OPTICN,NE,4.) GO TO 1490

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CALL YTICKS (2)
CALL YREVTK
CALL YGRXS (XORIG,XSTP,XMAX,6.5,100,-1.0,0.)
1
GO TO 2710
IF (OPTION,NE,5.) GO TO 1500
CALL XTICKS (2)
CALL XREVTK
CALL XGRXS (XORIG,XSTP,XMAX,6.5,100,0.,-.75)
1
GO TO 2710
IF (OPTION,NE,6.) GO TO 1510
CALL XTICKS (2)
CALL XREVTK
CALL XGRXS (XORIG,XSTP,XMAX,8.5,100,-1.15,0.)
1
GO TO 2710
IF (OPTION,NE,7.) GO TO 1520
CALL XTICKS (2)
CALL XNAME ('',1)
GO TO 2710
CONTINUE
GO TO 2700
IF (Z,NE,18.) GO TO 1620
DO 1540 I=1,8
X(I)=LGH(I)
CONTINUE
XORIG=20.
XSTP=20.
XMAX=120.
IF (OPTION,NE,1.) GO TO 1550
CALL XTICKS (2)
CALL XNAME ('FUSELAGE LENGTH (FT)',100)
GO TO 2710
IF (OPTION,NE,2.) GO TO 1560
CALL XTICKS (2)
CALL YNAME ('FUSELAGE LENGTH (FT)',100)
GO TO 2710
IF (OPTION,NE,3.) GO TO 1570
CALL XTICKS (2)
CALL XREVTK
CALL XGRXS (XORIG,XSTP,XMAX,9,100,0.,-.75)
1
GO TO 2710
IF (OPTION,NE,4.) GO TO 1580
CALL XTICKS (2)
CALL YREVTK
CALL YGRXS (XORIG,XSTP,XMAX,6.,

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1580      1 GO TO 2710
          IF (OPTION, NE, 5.) GO TO 1590
          CALL XTICKS (2)
          CALL XREVTK
          CALL XGRAXS
          ' FUSELAGE LENGTH (FT) $, 100, -1., 0.)

1590      1 GO TO 2710
          IF (OPTION, NE, 6.) GO TO 1600
          CALL YTICKS (2)
          CALL YREVTK
          CALL YGRAXS
          (XORIG, XSTP, XMAX, 6, 5,
           ' FUSELAGE LENGTH (FT) $, 100, 0., -.75)

1600      1 GO TO 2710
          IF (OPTION, NE, 7.) GO TO 1610
          CALL XTICKS (2)
          CALL XNAME ('.', 1)
          GO TO 2710
          CONTINUE

1610      GO TO 2710
          CONTINUE

1620      IF (Z, NE, 19.) GO TO 1710
          DO 1630 I=1, 8
          X(I)=FH(I)
          CONTINUE

1630      XORIG=0.
          XSTP=10.
          XMAX=70.
          IF (OPTION, NE, 1.) GO TO 1640
          CALL XTICKS (2)
          CALL XNAME ('FRONT FLAT PLATE AREA(SF) $, 100)
          GO TO 2710

1640      IF (OPTION, NE, 2.) GO TO 1650
          CALL YTICKS (2)
          CALL YNAME ('FRONT FLAT PLATE AREA(SF) $, 100)
          GO TO 2710

1650      IF (OPTION, NE, 3.) GO TO 1660
          CALL XTICKS (2)
          CALL XREVTK
          CALL XGRAXS
          (XORIG, XSTP, XMAX, 9,
           'FRONT FLAT PLATE AREA(SF) $, 100, 0., -.75)

1660      1 GO TO 2710
          IF (OPTION, NE, 4.) GO TO 1670
          CALL YTICKS (2)
          CALL YREVTK
          CALL YGRAXS
          (XORIG, XSTP, XMAX, 6,
           'FRONT FLAT PLATE AREA(SF) $, 100, -1., 0.)

1670      1 GO TO 2710
          IF (OPTION, NE, 5.) GO TO 1680

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1680      CALL XTICKS (2)
          CALL XREVTK
          CALL XGRAXS (XORIG,XSTP,XMAX,6.5,
            'FRONT',FLAT,PLATE,AREA(SF)$',100,0.0,-.75)
          GO TO 2710
          IF (OPTION,NE,6.0) GO TO 1690
          CALL YTICKS (2)
          CALL YREVTK
          CALL YGRAXS (XORIG,XSTP,XMAX,8.0,
            'FRONT',FLAT,PLATE,AREA(SF)$',100,-1.15,0.0)
1690      GO TO 2710
          IF (OPTION,NE,7.0) GO TO 1700
          CALL XTICKS (2)
          CALL XNAME ('',1)
          GO TO 2710
          CONTINUE
1700      GO TO 2700
1710      IF (Z,NE,20.0) GO TO 1800
          DO 1720 I=1,8
            X(I)=FV(I)
          CONTINUE
          XORIG=0.
          XSTP=30.
          XMAX=150.
          IF (OPTION,NE,1.0) GO TO 1730
          CALL XTICKS (3)
          CALL XNAME ('VERT',FLAT,PLATE,AREA(SF)$',100)
          GO TO 2710
          IF (OPTION,NE,2.0) GO TO 1740
          CALL YTICKS (3)
          CALL YNAME ('VERT',FLAT,PLATE,AREA(SF)$',100)
          GO TO 2710
          IF (OPTION,NE,3.0) GO TO 1750
          CALL XTICKS (3)
          CALL XREVTK
          CALL XGRAXS (XORIG,XSTP,XMAX,9.0,
            'VERT',FLAT,PLATE,AREA(SF)$',100,0.0,-.75)
1750      GO TO 2710
          IF (OPTION,NE,4.0) GO TO 1760
          CALL YTICKS (3)
          CALL YREVTK
          CALL YGRAXS (XORIG,XSTP,XMAX,6.0,
            'VERT',FLAT,PLATE,AREA(SF)$',100,-1.0,0.0)
1760      GO TO 2710
          IF (OPTION,NE,5.0) GO TO 1770
          CALL XTICKS (3)
          CALL XREVTK
          CALL XGRAXS (XORIG,XSTP,XMAX,6.5,

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1770      1 GO TO 2710
          IF (OPTION, NE, 6.) GO TO 1780
          CALL YTICKS (3)
          CALL YREVTX
          CALL YGRAXS
          'VERT. FLAT PLATE AREA(SF)$', 100, 0., -.75)
          'XORIG, XSTP, XMAX, 8.,
          'VERT. FLAT PLATE AREA(SF)$', 100, -1.15, 0.)
1780      1 GO TO 2710
          IF (OPTION, NE, 7.) GO TO 1790
          CALL XTICKS (3)
          CALL XNAME ('.', 1)
          GO TO 2710
1790      CONTINUE
          GO TO 2700
1800      IF (Z, NE, 21.) GO TO 1890
          DO 1810 I=1, 8
          X(I)=VM(I)
          CONTINUE
          XORIG=100.
          XSTP=100.
          XMAX=180.
          IF (OPTION, NE, 1.) GO TO 1820
          CALL XTICKS (2)
          CALL XNAME ('MAXIMUM VELOCITY (KNT)$', 100)
          CALL XINTAX
          GO TO 2710
1820      IF (OPTION, NE, 2.) GO TO 1830
          CALL YTICKS (2)
          CALL YNAME ('MAXIMUM VELOCITY (KNT)$', 100)
          CALL YINTAX
          GO TO 2710
1830      IF (OPTION, NE, 3.) GO TO 1840
          CALL XTICKS (2)
          CALL XREVTX
          CALL XGRAXS
          'XORIG, XSTP, XMAX, 9.,
          'MAXIMUM VELOCITY (KNT)$', 100, 0., -.75)
          'XORIG, XSTP, XMAX, 6.,
          'MAXIMUM VELOCITY (KNT)$', 100, -1., 0.)
1840      1 CALL XINTAX
          GO TO 2710
          IF (OPTION, NE, 4.) GO TO 1850
          CALL YTICKS (2)
          CALL YREVTX
          CALL YGRAXS
          'XORIG, XSTP, XMAX, 6.,
          'MAXIMUM VELOCITY (KNT)$', 100, -1., 0.)
1850      1 CALL YINTAX
          GO TO 2710
          IF (OPTION, NE, 5.) GO TO 1860
          CALL XTICKS (2)
          CALL XREVTX

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1 CALL XGRAXS (XORIG,XSTP,XMAX,6.5,
  'MAXIMUM VELOCITY (KNT)$',100,0.,-.75)
1860 CALL XINTAX
      GO TO 2710
      IF (OPTION,NE,6.) GO TO 1870
      CALL XTICKS (2)
      CALL YREVTX
      CALL YGRAXS
      (XORIG,XSTP,XMAX,8.,
        'MAXIMUM VELOCITY (KNT)$',100,-1.15,0.)
1 CALL YINTAX
      GO TO 2710
      IF (OPTION,NE,7.) GO TO 1880
      CALL XTICKS (2)
      CALL XNAME ('',1)
      GO TO 2710
      CONTINUE
      GO TO 450
      IF (Z,NE,22.) GO TO 1980
      DO 1900 I=1,8
      X(I)=RNG(I)
      CONTINUE
      XORIG=150.
      XSTP=550.
      XMAX=550.
      IF (OPTION,NE,1.) GO TO 1910
      CALL XTICKS (2)
      CALL XNAME ('MAXIMUM RANGES (NM)$',100)
      CALL XINTAX
      GO TO 2710
      IF (OPTION,NE,2.) GO TO 1920
      CALL VTICKS (2)
      CALL YNAME ('MAXIMUM RANGES (NM)$',100)
      CALL YINTAX
      GO TO 2710
      IF (OPTION,NE,3.) GO TO 1930
      CALL XTICKS (2)
      CALL XREVTX
      CALL XGRAXS (XORIG,XSTP,XMAX,9,
        'MAXIMUM RANGE (NM)')
1 CALL XINTAX
      GO TO 2710
      IF (OPTION,NE,4.) GO TO 1940
      CALL XTICKS (2)
      CALL YREVTX
      CALL YGRAXS (XORIG,XSTP,XMAX,6.,
        'MAXIMUM RANGE (NM)')
1 CALL YINTAX
      GO TO 2710

```

```

1940 IF (OPTION,NE,5.) GO TO 1950
      CALL XTICKS (2)
      CALL XREVTX (XORIG,XSTP,XMAX,6.5)
      CALL XGRAXS (XORIG,XSTP,XMAX,6.5)
1
      CALL XINTAX
      GO TO 2710
1950 IF (OPTION,NE,6.) GO TO 1960
      CALL YTICKS (2)
      CALL YREVTX (XORIG,XSTP,XMAX,8.)
      CALL YGRAXS (XORIG,XSTP,XMAX,8.)
1
      CALL YINTAX
      GO TO 2710
1960 IF (OPTION,NE,7.) GO TO 1970
      CALL XTICKS (2)
      CALL XNAME (,1)
      GO TO 2710
1970 CONTINUE
      GO TO 2700
1980 IF (Z,NE,23.) GO TO 2070
      DO 1990 I=1,8
      X(I)=RC(I)
1990 CONTINUE
      XORIG=C.
      XSTP=500.
      XMAX=3000.
      IF (OPTION,NE,1.) GO TO 2000
      CALL XTICKS (2)
      CALL XNAME (RATE OF CLIMB (FT/MIN)$,100)
      CALL XINTAX
      GO TO 2710
2000 IF (OPTION,NE,2.) GO TO 2010
      CALL YTICKS (2)
      CALL YNAME (RATE OF CLIMB (FT/MIN)$,100)
      CALL YINTAX
      GO TO 2710
2010 IF (OPTION,NE,3.) GO TO 2020
      CALL XTICKS (2)
      CALL XREVTX (XORIG,XSTP,XMAX,9)
      CALL XGRAXS (XORIG,XSTP,XMAX,9)
1
      CALL XINTAX
      GO TO 2710
2020 IF (OPTION,NE,4.) GO TO 2030
      CALL YTICKS (2)
      CALL YREVTX (XORIG,XSTP,XMAX,6.)
      CALL YGRAXS (XORIG,XSTP,XMAX,6.)

```

```

1 CALL YINTAX
  GO TO 2710
  IF (OPTICN,NE,5.) GO TO 2040
  CALL XTICKS (2)
  CALL XREVTK
  CALL XGRAXS
  (XORIG,XSTP,XMAX,6.5,
  'RATE OF CLIMB {FT/MIN}$',100,0.,-.75)
1 CALL XINTAX
  GO TO 2710
  IF (OPTICN,NE,6.) GO TO 2050
  CALL YTICKS (2)
  CALL YREVTK
  CALL YGRAXS
  (XORIG,XSTP,XMAX,8.7,
  'RATE OF CLIMB {FT/MIN}$',100,-1.15,0.)
1 CALL YINTAX
  GO TO 2710
  IF (OPTICN,NE,7.) GO TO 2060
  CALL XTICKS (2)
  CALL XNAME ('!',1)
  GO TO 2710
  CONTINUE
  GO TO 2700
  IF (Z,NE,24.) GC TO 2160
  DO 2080 I=1,8
  X(I)=HCVIGE(I)
  CONTINUE
  XORIG=3000.
  XSTP=3000.
  XMAX=15000.
  IF (OPTICN,NE,1.) GO TO 2090
  CALL XTICKS (3)
  CALL XNAME ('HOVER CEILING (FT) IGE$',100)
  CALL XINTAX
  GO TO 2710
  IF (OPTICN,NE,2.) GO TO 2100
  CALL YTICKS (3)
  CALL YNAME ('HOVER CEILING (FT) IGE$',100)
  CALL YINTAX
  GO TO 2710
  IF (OPTICN,NE,3.) GO TO 2110
  CALL XTICKS (3)
  CALL XREVTK
  CALL XGRAXS
  (XORIG,XSTP,XMAX,9.7,
  'HOVER CEILING {FT} IGE$',100,0.,-.75)
1 CALL XINTAX
  GO TO 2710
  IF (OPTICN,NE,4.) GO TO 2120

```



```

2200      CALL XINTAX
        GO TO 2710
        IF (OPTION, NE, 4.) GO TO 2210
        CALL YTTICKS (3)
        CALL YREVTK
        CALL YGRAXS (XORIG, XSTP, XMAX, 6., OGE$, 100, -1., 0.)
1      CALL YINTAX
        GO TO 2710
        IF (OPTION, NE, 5.) GO TO 2220
        CALL XTICKS (3)
        CALL XREVTK
        CALL XGRAXS (XORIG, XSTP, XMAX, 6., OGE$, 100, 0., -.75)
1      CALL XINTAX
        GO TO 2710
        IF (OPTION, NE, 6.) GO TO 2230
        CALL YTTICKS (3)
        CALL YREVTK
        CALL YGRAXS (XORIG, XSTP, XMAX, 8., OGE$, 100, -1.15, 0.)
1      CALL YINTAX
        GO TO 2710
        IF (OPTION, NE, 7.) GO TO 2240
        CALL XTICKS (3)
        CALL XNAME (, , 1)
        GO TO 2710
        CONTINUE
        GO TO 2700
        IF (Z, NE, 26.) GO TO 2340
        DO 2260 I=1, 8
        X(I)=LT(I)
        CONTINUE
        XORIG=10.
        XSTP=10.
        XMAX=60.
        IF (OPTION, NE, 1.) GO TO 2270
        CALL YTTICKS (5)
        CALL XNAME (, LENGTH OF TAIL (FT)$, 100)
        GO TO 2710
        IF (OPTION, NE, 2.) GO TO 2280
        CALL YTTICKS (5)
        CALL YNAME (, LENGTH OF TAIL (FT)$, 100)
        GO TO 2710
        IF (OPTION, NE, 3.) GO TO 2290
        CALL XTICKS (5)
        CALL XREVTK
        CALL XGRAXS (XORIG, XSTP, XMAX, 9.,

```

```

1      GO TO 2710      'LENGTH OF TAIL (FT)$',100,0.,-.75)
2290   IF (OPTION,NE,4.) GO TO 2300
      CALL YTICKS (5)
      CALL YREVTX
      CALL YGRAXS (XORIG,XSTP,XMAX,6.,
1      'LENGTH OF TAIL (FT)$',100,-1.,0.)
2300   GO TO 2710
      IF (OPTION,NE,5.) GO TO 2310
      CALL XTICKS (5)
      CALL XREVTX
      CALL XGRAXS (XORIG,XSTP,XMAX,6.,5,
1      'LENGTH OF TAIL (FT)$',100,0.,-.75)
2310   GO TO 2710
      IF (OPTION,NE,6.) GO TO 2320
      CALL YTICKS (5)
      CALL YREVTX
      CALL YGRAXS (XORIG,XSTP,XMAX,8.,7,
1      'LENGTH OF TAIL (FT)$',100,-1.15,0.)
2320   GO TO 2710
      IF (OPTION,NE,7.) GO TO 2330
      CALL XTICKS (5)
      CALL XNAME (,1)
      GO TO 2710
2330   CONTINUE
      GO TO 2700
2340   IF (Z,NE,27.) GO TO 2430
      DO 2350 I=1,8
      X(I)=0.0
      CONTINUE
      XORIG=0.0
      XSTP=5000.
      XMAX=4000.
      IF (OPTION,NE,1.) GO TO 2360
      CALL YTICKS (2)
      CALL XNAME ('OPERATING WEIGHT (LB)$',100)
      CALL XINTAX
      GO TO 2710
2360   IF (OPTION,NE,2.) GO TO 2370
      CALL YTICKS (2)
      CALL YNAME ('OPERATING WEIGHT (LB)$',100)
      CALL YINTAX
      GO TO 2710
2370   IF (OPTION,NE,3.) GO TO 2380
      CALL XTICKS (2)
      CALL XREVTX
      CALL XGRAXS (XORIG,XSTP,XMAX,9.,
1      'OPERATING WEIGHT (LB)$',100,0.,-.75)

```

```

2380      CALL XINTAX
        GO TO 2710
        IF (OPTION, NE, 4.) GO TO 2390
        CALL YTTICKS (2)
        CALL YREVTK
        CALL YGRAXS
        1 CALL YINTAX
        GO TO 2710
        IF (OPTION, NE, 5.) GO TO 2400
        CALL XTTICKS (2)
        CALL XREVTK
        CALL XGRAXS
        1 CALL XINTAX
        GO TO 2710
        IF (OPTION, NE, 6.) GO TO 2410
        CALL YTTICKS (2)
        CALL YREVTK
        CALL YGRAXS
        1 CALL YINTAX
        GO TO 2710
        IF (OPTION, NE, 7.) GO TO 2420
        CALL XTTICKS (2)
        CALL XNAME ('', 1)
        GO TO 2710
        CONTINUE
        GO TO 2700
        IF (Z, NE, 28.) GO TO 2520
        DO 2440 I=1,8
        X(I)=LWT(I)
        CONTINUE
        XORIG=0.
        XSTP=5000.
        XMAX=30000.
        IF (OPTION, NE, 1.) GO TO 2450
        CALL XTTICKS (2)
        CALL XNAME ('LOAD WEIGHT (LB)$', 100)
        CALL XINTAX
        GO TO 2710
        IF (OPTION, NE, 2.) GO TO 2460
        CALL YTTICKS (2)
        CALL YNAME ('LOAD WEIGHT (LB)$', 100)
        CALL YINTAX
        GO TO 2710
        IF (OPTION, NE, 3.) GO TO 2470
        CALL XTTICKS (2)

```

```

CALL XREVTX
CALL XGRAXS (XORIG,XSTP,XMAX,9,1,100,0,0,-.75)
1 CALL XINTAX
GO TO 2710
IF (OPTION,NE,4,0) GO TO 2480
CALL YTTICKS (2)
CALL YREVTX
CALL YGRAXS (XORIG,XSTP,XMAX,6,1,100,-1,0,0)
1 CALL YINTAX
GO TO 2710
IF (OPTION,NE,5,0) GO TO 2490
CALL XTTICKS (2)
CALL XREVTX
CALL XGRAXS (XORIG,XSTP,XMAX,6,5,100,0,0,-.75)
1 CALL XINTAX
GO TO 2710
IF (OPTION,NE,6,0) GO TO 2500
CALL YTTICKS (2)
CALL YREVTX
CALL YGRAXS (XORIG,XSTP,XMAX,8,1,100,-1,15,0)
1 CALL YINTAX
GO TO 2710
IF (OPTION,NE,7,0) GO TO 2510
CALL XTTICKS (2)
CALL XNAME ('',1)
GO TO 2710
CONTINUE
GO TO 2700
IF (Z,NE,29,0) GO TO 2610
DO 2530 I=1,8
X(I)=FWT(I)
CONTINUE
XORIG=C
XSTP=3000
XMAX=21000
IF (OPTION,NE,1,0) GO TO 2540
CALL XTTICKS (3)
CALL XNAME ('FUEL WEIGHT (LB)$',100)
CALL XINTAX
GO TO 2710
IF (OPTION,NE,2,0) GO TO 2550
CALL YTTICKS (3)
CALL YNAME ('FUEL WEIGHT (LB)$',100)
CALL YINTAX

```

2470

2480

2490

2500

2510

2520

2530

2540

```

2550      GO TO 2710
        IF (OPTION, NE, 3.) GO TO 2560
        CALL XTICKS (3)
        CALL XREVTK
        CALL XGRAXS (XORIG, XSTP, XMAX, 9., 100, 0., -.75)
1
        CALL XINTAX
        GO TO 2710
2560      IF (OPTION, NE, 4.) GO TO 2570
        CALL YTICKS (3)
        CALL YREVTK
        CALL YGRAXS (XORIG, XSTP, XMAX, 6., 100, -1., 0.)
1
        CALL YINTAX
        GO TO 2710
2570      IF (OPTION, NE, 5.) GO TO 2580
        CALL XTICKS (3)
        CALL XREVTK
        CALL XGRAXS (XORIG, XSTP, XMAX, 6.5, 100, 0., -.75)
1
        CALL XINTAX
        GO TO 2710
2580      IF (OPTION, NE, 6.) GO TO 2590
        CALL YTICKS (3)
        CALL YREVTK
        CALL YGRAXS (XORIG, XSTP, XMAX, 8., 100, -1.15, 0.)
1
        CALL YINTAX
        GO TO 2710
2590      IF (OPTION, NE, 7.) GO TO 2600
        CALL XTICKS (3)
        CALL XNAME (., ., 1)
        GO TO 2710
2600      CONTINUE
        GO TO 2700
2610      IF (Z, NE, 30.) GO TO 2700
        DO 2620 I=1, 8
        X(I)=MGW(I)
2620      CONTINUE
        XORIG=0.
        XSTP=30000.
        XMAX=90000.
        IF (OPTION, NE, 1.) GO TO 2630
        CALL XTICKS (3)
        CALL XNAME ('MAXIMUM GROSS WEIGHT (LB)', 100)
        CALL XINTAX
        GO TO 2710
2630      IF (OPTION, NE, 2.) GO TO 2640

```

```

2640      CALL YTTICKS (3)
          CALL YNAME ('MAXIMUM GROSS WEIGHT (LB) $', 100)
          CALL YINTAX
          GO TO 2710
          IF (OPTION, NE, 3.) GO TO 2650
          CALL XTTICKS (3)
          CALL XREVTK
          CALL XGRAXS
          1 CALL XINTAX
          GO TO 2710
          IF (OPTION, NE, 4.) GO TO 2660
          CALL YTTICKS (3)
          CALL YREVTK
          CALL YGRAXS
          1 CALL YINTAX
          GO TO 2710
          IF (OPTION, NE, 5.) GO TO 2670
          CALL XTTICKS (3)
          CALL XREVTK
          CALL XGRAXS
          1 CALL XINTAX
          GO TO 2710
          IF (OPTION, NE, 6.) GO TO 2680
          CALL YTTICKS (3)
          CALL YREVTK
          CALL YGRAXS
          1 CALL YINTAX
          GO TO 2710
          IF (OPTION, NE, 7.) GO TO 2690
          CALL XTTICKS (3)
          CALL XNAME ('', 1)
          GO TO 2710
          CONTINUE
          GO TO 2700
          CONTINUE
          WRITE (6, 2720)
          CONTINUE
          CALL RESET ('XREVTK')
          CALL RESET ('YREVTK')
          RETURN
          FORMAT (54H YOU HAVE MADE A MISTAKE AND ENTERED AN INVALID NUMBER)
          END

```

APPENDIX B

A. USERS GUIDE TO THE CONCEPTUAL DESIGN PROGRAM

The design program has been developed with the user in mind. The program is completely interactive in that it prompts the user for any inputs needed. The following steps should be taken to invoke the program and to get an output file useable for analysis.

1. Logon as normal on either the IBM 3278 or the Tektronix 618 dual screen system
2. Obtain temporary storage space by typing in:

DEFINE STORAGE 1M (enter)
3. When PSW '00020000 00000 000' appears on the screen type in:

I CMS (enter)
4. If the program has not been compiled on your disk yet type in the following:

FORTGI DESIGN (enter)
5. After the program has been compiled you are ready to run the program by typing in:

DISSPLA (enter)
6. You will be asked to enter library functions or to press enter. Press the enter key.
7. You will then be asked if you want additional temporary space for shading, etc.. Again, press the enter key.
8. Next you will be asked to enter any defined files that you want. Here you should enter the following:

FILEDEF 08 DISK DESIGN (file name)

9. After entering the above line the screen will flash and your FILEDEF should be listed on the bottom line of the existing FILEDEFS. If your filedef is listed press the enter key to start the program execution.
10. Follow the instructions given on the screen. You will need the Helicopter Design Manual and the appropriate handouts/references to complete the process.
11. If you are on the IBM 3278 terminal you will not get a graph, therefore, you must plot the total power data by hand and extrapolate the needed data
12. If you are using the TEK 618 dual screen system a graph will be drawn of the total power curve and its components at altitude which can immediately be used to extrapolate the necessary data to complete the entire design process.
13. Note that the output file of all the information that you have computed is in the file that you have defined. To get your data type in:

PRINT DESIGN (filename) (CC

B. PROGRAM NOMENCLATURE

MNEMONIC

DEFINITION

| | |
|-------|--|
| A | Sonic speed at standard sea level |
| AALT | Sonic speed at specification density altitude |
| AASLY | Average aircraft serviceable life in years |
| AFHPF | Average flight hours per flight |
| AFHPY | Average flight hours per year per airframe |
| ALPHA | Ordinate intercept of fuel flow-horsepower curve |
| ALT | Maximum rate of climb calculation altitude |
| ALTSC | Service ceiling altitude |
| AMAX | Steady flow stall angle of the airfoil |

| | |
|--------|--|
| ANS | General variable for keyboard answer |
| AR | Aspect ratio of the main rotor system |
| AREAMR | Area of the main rotor disc |
| AREATR | Area of the tail rotor disc |
| ARTR | Aspect ratio of the tail rotor |
| ARVS | Vertical stabilizer aspect ratio |
| AVAIL | Availability of an engine |
| AVAILM | Availability (multiple engine) |
| A11 | Term in definition of THETA2 |
| A12 | Term in definition of THETA2 |
| A13 | Term in definition of THETA2 |
| A14 | Term in definition of THETA2 |
| A80 | Vertical stabilizer angle of attack at 80 knots |
| A90 | Angle of attack of the advancing blade (radians) |
| A160 | Vertical stabilizer angle of attack at 160 knots |
| A90D | Angle of attack of the advancing blade (degrees) |
| A270 | Angle of attack of retreating blade (radians) |
| A270D | Angle of attack of retreating blade (degrees) |
| B | Main rotor tip loss factor |
| BETA | Slope of the fuel flow horsepower curve |
| BH | Main rotor tip loss factor at a hover |
| BL | Blade loading of the main rotor system |
| BLADES | Number of main rotor blades |

| | |
|--------|---|
| BLADTR | Number of tail rotor blades |
| BS | Term used in inboard stall analysis |
| BTA | Tail rotor tip loss factor at altitude |
| BTR | Tail rotor tip loss factor |
| BVS | Span of the vertical stabilizer |
| CDO | Coefficient of drag of a main rotor blade |
| CDOTR | Coefficient of drag of a tail rotor blade |
| CHORD | Chord of a main rotor blade |
| CHORDT | Chord of a tail rotor blade |
| CL | Coefficient of lift of a main rotor blade section |
| CLA | Lift curve slope of a main rotor blade section |
| CLMAX | Maximum coefficient of lift for a blade section |
| CL80 | Section coefficient of lift at 80 knots |
| CL160 | Section coefficient of lift at 160 knots |
| COLL | Collective position (radians) |
| COLLD | Collective position (degrees) |
| COMPAR | Weight variance parameter |
| CONST | Constant value in ICAO formulae |
| COUNT | Counter variable |
| CPC | Correction to power coefficient |
| CPS | Correction to power coefficient due to stall |
| CREW | Number of specified crew |
| CS | Term used in stall analysis |

| | |
|--------|---|
| CT | Main rotor coefficient of thrust |
| CTH | Main rotor coefficient of thrust at a hover |
| CTTA | Tail rotor coefficient of thrust at altitude |
| CTTR | Tail rotor coefficient of thrust at sea level |
| CYCD | Cyclic position (degrees) |
| CYCLIC | Cyclic position (radians) |
| C1 | Cost of main rotor |
| C2A | Cost of tail rotor |
| C2B | Cost of tail rotor structure |
| C3 | Cost of body |
| C4 | Cost of landing gear |
| C5 | Cost of nacelle |
| C6A | Cost of engine |
| C6B | Cost of drive system |
| C6C | Cost of fuel tanks |
| C7 | Cost of flight controls |
| C8 | Cost of auxillary power |
| C9 | Cost of instruments |
| C10 | Cost of hydraulics |
| C11 | Cost of electrical system |
| C12 | Cost of avionics |
| C13 | Cost of furnishings |
| C14 | Cost of air and ice |

| | |
|--------|---|
| C15 | Cost of load and handling |
| D | Diameter of the rotor system |
| DA270 | Blade angle of advancing blade (degrees) |
| DELTA | Fuel flow ratio |
| DERR | Error function |
| DL | Disc loading of the main rotor system |
| DLAMB | Term used in blade stall analysis |
| DP | Parasite drag |
| DREF | Acceptable error function |
| DW | Powerplant dry weight of an engine |
| DWG | Design gross weight |
| DWM | Powerplant dry weight (multiple engine) |
| D1 | Stall analysis parameter |
| D2 | Stall analysis parameter |
| EFPAFF | Effective flat plate area (horizontal) |
| EFPAVF | Effective flat plate area (vertical) |
| EIW | Engine installed weight |
| EIWM | Engine installed weight (multiple engine) |
| ENGSEL | Engine selected |
| ESHPR | Estimated shaft horsepower required to hover |
| EW | Estimated engine weight from weight estimations |
| EWNEW | New engine weight using powerplant data |
| EXCESS | Excess weight |

| | |
|--------|---|
| E1 | Stall analysis parameter |
| E2 | Stall analysis parameter |
| E3 | Stall analysis parameter |
| FL | Factor for landing gear weight approximation |
| FSLT | Length of the fuselage |
| FSLTS | Specification maximum length of the fuselage |
| FUEL | Amount of fuel in pounds |
| PW | Fuel weight in pounds |
| PWNEW | Change in original fuel weight for printout |
| GALIN | Internal fuel weight in gallons |
| GALOUT | External fuel weight in gallons |
| GAM | Stall analysis parameter |
| GWSPEC | Specification maximum gross weight |
| HL | Life of the aircraft |
| HOVIGE | Specification hover ceiling (in ground effect) |
| HP | Hover power of the main rotor system (out of ground effect) |
| ht | Rotor system height above the ground |
| I | Do loop parameter |
| IC | Initial cost of an engine |
| ICM | Initial costs (multiple engine) |
| IER | Library function error code |
| IF | Installation fraction |
| IHP | Array for plotting |

| | |
|--------|--|
| IR | Inflation rate in 1977 dollars |
| K | Dc lcop parameter |
| KNOTS | Increment for forward speed |
| KNT | Increment for fcrward speed |
| KNTS | Knots increment for table |
| KS | Stall analysis parameter |
| LAMBDA | Stall analysis parameter |
| LAMB1 | Stall analysis parameter |
| LAMFR | Used for reliability calculation |
| LCC | Life cycle cost cf an engine |
| LCCM | Life cycle cost (multiple engine) |
| LERR | Acceptable error function |
| LG | Type of landing gear |
| LOAD | Loading used to find effective flat plate area |
| LREF | Acceptable error function |
| LTR | Length of the tail rotor |
| M | Figure of merit |
| MACH | Maximum allowable Mach number at sea level |
| MACHT | Main rotor system tip Mach number |
| MAINT | Maintainability of an engine |
| MAINTM | Maintainability (multiple engine) |
| MAXRC | Specification rate of climb |
| MAXV | Maxium forward velocity in feet per second |

| | |
|--------|--|
| MCRIT | Critical Mach number |
| MCRO | Zero angle of attack critical Mach number |
| MD | Drag divergence Mach number |
| MDT | Mean down time of an engine |
| MTBF | Mean time between engine failures |
| MTBMA | Mean time between maintenance actions per engine |
| MTBR | Mean time between repairs for an engine |
| MTBRM | Mean time between repair (multiple engine) |
| MTIP | Tip Mach number of the main rotor system |
| MTTR | TIP MACH NUMBER OF THE TAIL ROTOR SYSTEM |
| MU | Advance ratio of the main rotor system |
| MUTR | Advance ratio of the tail rotor system |
| N | Do loop parameter |
| NDEG | Order of differential equation |
| NENG | Number of engines |
| NEWUSE | New useful load |
| NN | Do loop parameter |
| NRPL | Number of engine replacements (real or integer) |
| NRPLM | Number of engine replacements (multiple engine) |
| NW | Number of landing gear |
| NXRPL | Number of engine replacements (integer) |
| NXRPLM | Number of engine replacements (multiple engine) |
| OC | Operating cost of an engine |

| | |
|--------|---|
| OLD | Previous gross weight used for comparison |
| OMEGA | Main rotor rotational velocity (radians) |
| OMEGTR | Tail rotor rotational velocity (radians) |
| PA | Specification pressure altitude |
| PADJA | Adjusted power at altitude |
| PADJS | Adjusted power at sea level |
| PALT | Rate of climb pressure |
| PAVAIL | Power available |
| PC | Power to climb |
| PCMPA | Array for compressible power at altitude |
| PCMPs | Array for compressible power at sea level |
| PEOPLE | Number of people |
| PI | Induced power of the main rotor system |
| PIE | Constant for value of pi |
| PIHP | Induced power of the main rotor system in HP |
| PITLFP | Induced power (IGE) at a forward speed |
| PITLFA | Induced power at altitude at forward speed |
| PITLFS | Induced power at sea level at forward speed |
| PITLGE | Induced power in ground effect |
| PITLGH | Induced power at a hover |
| PITLH | Induced power at a hover |
| PITLTF | Induced power of the tail rotor in forward flight |
| PITLTR | Induced power for the tail rotor |

| | |
|--------|--|
| PITRFA | Induced power of the tail rotor at altitude in forward flight |
| PITRFS | Induced power of the tail rotor at sea level in forward flight |
| PIVERT | Induced power vertically |
| PIX | Array used for plotting of total induced power at sea level |
| PIY | Array used for plotting total induced power at altitude |
| PM | Preventative maintenance cost of an engine |
| PMBS | Blade stall power factor |
| PO | Profile power of the main rotor system |
| POC | Profile power to climb |
| POF | Profile power at a forward speed |
| POFA | Profile power at altitude at forward speed |
| POFS | Profile power at sea level at forward speed |
| POH | Profile power at a hover |
| POHP | Profile power of the main rotor system in HP |
| POTA | Profile power of tail rotor at altitude |
| POTR | Profile power for the tail rotor |
| POTRF | Profile power of the tail rotor in forward flight |
| POTRFA | Profile power of the tail rotor at altitude in forward flight |
| POTRFS | Profile power of the tail rotor at sea level in forward flight |
| POX | Array used for plotting of total profile power at sea level |
| POY | Array used for plotting total profile power at altitude |

| | |
|--------|---|
| PP | Parasite power |
| PPC | Parasite power to climb |
| PPF | Parasite power at a forward speed |
| PPFA | Parasite power at altitude at forward speed |
| PPFS | Parasite power at sea level at forward speed |
| PPOGE | In ground effect distance parameter |
| PPOGEN | Ground effect factor at a hover |
| PPX | Array used for plotting total parasite power at sea level |
| PPY | Array used for plotting total parasite power at altitude |
| PRESS | Specification pressure altitude |
| PS | Stall power |
| PSHP | Phantom shaft horsepower |
| PT | Total power of the main rotor system |
| PTACH | Total power for the aircraft to hover |
| PTAH | Total power of the aircraft to hover |
| PTAVAL | Total power available |
| PTF | Total power at a forward velocity |
| PTFA | Total power at altitude at forward speed |
| PTFS | Total power at sea level at forward speed |
| PTH | Total power at a hover |
| PTHOVS | Total power to hover |
| PTHP | Total power of the main rotor system in HP |
| PTTAHP | Total power of the aircraft to hover in HP |

| | |
|--------|--|
| PTTRF | Total power of the tail rotor in forward flight |
| PTTRFA | Total power of the tail rotor at altitude in forward flight |
| PTTRFS | Total power of the tail rotor at sea level in forward flight |
| PTTRH | Total power for the tail rotor at a hover |
| PTTRHP | Total power for the tail rotor at a hover in HP |
| PTVERT | Total power vertically |
| PTX | Array used for plotting total power at sea level |
| PTY | Array used for plotting total power at altitude |
| Q | Production run quantity |
| R | Rotor radius |
| RBS | Retreating blade stall velocity |
| RC | Recovery cost of an engine |
| RCLIMB | Rate of climb |
| RCM | Recovery cost (multiple engine) |
| RDC | Research and development cost of an engine |
| RDCM | Research and development costs (multiple engine) |
| RELY | Reliability of an engine |
| RELYM | Reliability (multiple engine) |
| REVWE | Revised empty weight |
| REVWG | Revised gross weight |
| RHOALT | Density at specification density altitude |
| RHOMH | Density at hover in ground effect ceiling |
| RHOS | Density at service ceiling |

| | |
|--------|---|
| RHOSC | Service ceiling density |
| RHOSL | Sea level density |
| RNGMAX | Maximum range as per specification |
| RNGNMX | New maximum range |
| RSHPC | Required shaft horsepower for cruise |
| RSHPME | Required shaft horsepower for max endurance speed |
| RSHRME | Total required shaft horsepower for max endurance |
| RSHPRC | Total required shaft horsepower for cruise |
| RRSHP | Required shaft horsepower |
| RSHPM | Required shaft horsepower (military) |
| RSPEC | Specification maximum rotor radius |
| RT | Stall analysis parameter |
| RTR | Tail rotor radius |
| S | Main rotor planform area for weight estimation |
| SB | Body surface area for weight estimation |
| SC | Specification service ceiling |
| SFCC | Cruise specific fuel consumption |
| SFCM | Military specific fuel consumption |
| SFCN | Normal specific fuel consumption |
| SHPC | Cruise shaft horsepower |
| SHPM | Military shaft horsepower |
| SHPMN | Military shaft horsepower (multiple engine) |
| SHPN | Normal shaft horsepower |

| | |
|--------|---|
| SIG | Pressure ratio |
| SIGMA | Solidity of the main rotor system |
| SIGTR | Solidity of the tail rotor system |
| SIM | Weight variance parameter |
| SPCL0D | Specification useful load |
| STEP | Variance parameter for iterations |
| STT | Total tail surface area for weight estimation |
| SV | Salvage value |
| SVM | Salvage value (multiple engine) |
| TALT | Rate of climb temperature |
| TEMP | Specification temperature |
| THETA | Temperature ratio |
| THETA0 | Collective angle in radians |
| THETA2 | Cyclic angle in radians |
| TOTALC | Total cost of an aircraft in a production run |
| TRIP1 | Trips the program so that repetitive questions are repeated |
| TRIP2 | Trips the program so that repetitive questions are repeated |
| TRIP3 | Trips the program so that repetitive questions are repeated |
| TRIP4 | Trips the program so that repetitive questions are repeated |
| TRIP5 | Trips the program so that repetitive questions are repeated |
| TSHP | Total shaft horsepower |
| TTR | Thrust of the tail rotor |

| | |
|--------|---|
| TTR80 | Tail rotor thrust at 80 knots |
| TTR160 | Tail rotor thrust at 160 knots |
| TWIST | Twist of main rotor blade |
| TYPE | Type of helicopter (light,medium,heavy) |
| TYPEM | Type of aircraft (light,medium,heavy) |
| T1 | Term used in defining THETA0 |
| T2 | Term used in defining THETA0 |
| T3 | Term used in defining THETA0 |
| T4 | Term used in defining THETA0 |
| USELOD | Useful load desired |
| VCR | Cruise velocity as per specification |
| VELMAX | Maximum forward velocity |
| VF | Forward velocity |
| VFWD | Forward velocity |
| VF80 | Forward velocity at 80 knots in ft/sec |
| VF160 | Forward velocity at 160 knots in ft/sce |
| VI | Induced velocity in a hover |
| VINEW | Induced velocity at hover |
| VIT | Vertical induced velocity at a hover |
| VITNEW | Induced vertical velocity at a hover |
| VITR | Induced velocity of the tail rotor |
| VITTR | Induced vertical velocity of the tail rotor |
| VL | stall parameter |

| | |
|--------|--|
| VMAX | Specification maximum forward velocity |
| VMAXE | Maximum endurance velocity |
| VMAXF | Maximum forward velocity in knots |
| VMAXK | Initial forward velocity for stall analysis |
| VMAXR | Maximum range velocity |
| VOPT | Optimum velocity for aircraft in ft/sec |
| VOPTK | Optimum velocity for aircraft in knots |
| VS | Forward speed in ft/sec |
| VSK | Forward speed in knots |
| VTIP | Tip velocity of the main rotor system |
| VTIPTR | Tail rotor tip velocity |
| VTNEW | Solution to fourth order differential equation |
| VVERT | Vertical velocity |
| WE | Manufacturers empty weight |
| WFC | Cruise fuel flow rate |
| WFCR | Fuel flow rate for cruise flight |
| WFM | Military fuel flow rate |
| WFME | Fuel flow rate for max endurance velocity |
| WFN | Normal fuel flow rate |
| WG | Gross weight |
| WGNEW | New gross weight |
| WXO | Transmission and oil weight |
| WXOM | Transmission and oil weight (multiple engine) |

| | |
|------|--|
| W1 | Rotor weight |
| W2A | Tail rotor weight |
| W2B | Tail rotor structure weight |
| W3 | Body weight |
| W4 | Landing gear weight |
| W5 | Nacelle weight |
| W6A | Engine weight |
| W6B | Drive weight |
| W6C | Fuel tank weight |
| W7 | Flight control weight |
| W8 | Auxillary power weight |
| W9 | Instrument weight |
| W10 | Hydraulic weight |
| W11 | Electrical weight |
| W12 | Avionics weight |
| W13 | Furnishings weight |
| W14 | Air and ice weight |
| W15 | Load and handling weight |
| X0 | Radius used for stall analysis (inboard) |
| XRLG | Fixed or retractable landing gear |
| XS | Radius outboard analysis |
| YMC | Yearly maintenance cost of an engine |
| YMCM | Yearly maintenance costs (multiple engine) |

| | |
|--------|--|
| YOC | Yearly operating cost of an engine |
| YOCM | Yearly operating costs (multiple engine) |
| ZCMPLX | Array for library function |
| ZHI | Zero horsepower intercept |

C. PROGRAM LISTING

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REAL TRIP1, TRIP2, TRIP3, TRIP4, SC, HOVIGE, RSPEC, FSLTS, MAX RC, SPCLOD, TR
1 IP5, COUNT/O./, IR
REAL WG, GWSFEC
REAL WE
REAL A, MACH, VMAX, P IE, RHOSL
REAL DL, R, AREAMR
REAL OMEGA
REAL VTIP, CT
REAL VMAXF, MAX V, MU, BL, SIGMA
REAL CHORD, AR
REAL CLA, CDC
REAL B, PI, PC, PT, PIHP, POHP, PTHP, HP
REAL FUEL, USELOD, STT, SBS, W1, W2, W3, W4, W5, W6, W7, W8, W9
1, W10, W11, W12, W13, W14, W15, REVWE, REVWG, TYPE
REAL MANS, CLD/O./
REAL STEP, FL, LG, XRLG, NW
REAL H, C, P, CGE, PITLGE, PTHOV5
REAL L, C, EFPAFF, F, KNTS
REAL VF, PF, POF, VI, VIT, PITLFF, PTF, MACHT, PPFS(55), PDFS(55), PITLFS(55
1), PTFS(55), AALT, RHOALT, PPFA(55), PIFA(55), PITLFA(55), PIFA(55), TEMP,
2 THETA, RTR, OMEGTR, CD, CTR, LTR, ART, CHORDT, SIGTR
REAL AREATR, TTR, VTIPTR, CTIR, BTR, PITLTR, POTR, PTTRH, PTTRHP, CTTA, BTA,
1 PITLTA, FQTA, PTTAH, PTTAHP
REAL MUTR, PCTRF, PTRFS(55), PITRFS(55), MTTR, POTRFA(55), P
1 ITRFA(55), PITRFA(55), VITR, VITTR, PITTRF, PITLTF
REAL TTR160, TTR80, VS, BVS, CL80, CL160, VF80, VF160, CLARVS, A80, A160, ARV
1S
REAL LAMBDA, KS, MCRIT, MTIP, LERR, MCRO, LAMBD1, CLMAX, VL, VMAX, PCMPA(55
1), PCMPS(55), C1, C2, T1, T2, T3, T4, A11, A12, A13, A14, DP, DLAMB, LREF, E1, E2,
2 E3, DI, C2, CYCLIC, COLL, TWIST, GAM, AMAX, BS, RT, XS, XO, CS, CPS, KS, PS, A90, A
3 270, A90D, A270D, MD, CPC, TSHP, VOPF, VOPFK, VSK, TETA0, THETA2, DA270, DREF
4, DEARR, PTAH, PCX(55), PIX(55), PPX(55), PTX(55), POY(55), PIY(55), PPY(55),
1 PTY(55), KNOTS(55)
REAL PACJS, FADJA, RRSHP
REAL RHCS, CTH, BH, PITLH, PPOGEH, POH, PTH, RSHPM, PTACH, PITLGH
REAL ESHPR
REAL AFHPY, AFHPF, AASLY, HL, PM(6), QC(6), YMC(6), YOC(6), MTBR(6), NRPL(6
1), NXRPL(6), EIW(6), RC(6), IF(6), IC(6), SV(6), WXD(6), SHPM(6), LAM
2 FR(6), MTBF(6), RELY(6), AVAIL(6), MTBMA(6), MDI(6), LCC(6), RDC(6), MAINT
3 (6), DWMT(6), ICM(6), SHPM(6), RDCM(6), MTBRM(6), YCM(6), NRPLM(
4 6), NXRPLM(6), EIWM(6), SVCM(6), WXD(6), RELYM(6), AVAILM(6), LCC
5 (6), MAINTM(6), SHPC(6), SHPN(6), ENGSEL

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REAL EWNEW,WGNEW,COMPAR
REAL WFM,WFC,WFN,SFCN(6),SFCM(6),SFCC(6)
REAL BETA,ALPHA
REAL PSFP,TYPEN,FSLT
REAL VMAXR,RSHME,RSHRME,WFME
REAL RSHPC,FSHPRC,WFCR,RNGMAX,VCR
REAL FALIN,GALOUT,EXCESS
REAL DMC,RNGMAX,NEWUSE,SIM
REAL VVERT,PC,VFWD,PPC,POC,PIVERT,VINEW,PAVAL,PTAVAL,PTVER
1,VTITNEW(5),VTNEW,RCLIMB
REAL ALT,PALT,TALT,RHOMH
REAL ALTSC,FHOSC
REAL TOTALT,Q,C1,C2A,C2B,C3,C4,C5,C6A,C6B,C6C,C7,C8,C9,C10,C11,C12
1,C13,C14,C15
REAL PP,KNT,RBS,FWNEW,VELMAX
1,INTEGER 1,BLADES,NENG,PEOPLE,BLADTR,IHP(600),CREW,N,NN,NDEG,IER/0/
1,K
COMPLEX ZCMFLX(4)
DATA DM/158.1288,423.709,580.750./
DATA SHFM/420.708,1561.1800,2500.3400./
DATA SHPC/370.659,1318.1530,2200.3000./
DATA SHCN/650.573,460.595,615.543./
DATA SFCC/651.573,470.606,622.562./
DATA IC/93.100,580.360,640.700./
DATA OC/008.016,020.035,040.060./
DATA PM/02.050,100.125,160.220./
DATA MTBMA/3.5,3.0,3.0,4.0,3.5/
DATA MDI/.7,6.5,1.3,2.2,6./
DATA MTBF/185.210,205.285,280.320./
DATA RTCC/0.029,0.27,0.27,0.24/
DATA IERR/.01,0.01,0.01,0.01/
DATA DERR/.01,0.01,0.01,0.01/
*****
WRITE (6,15)
READ (5,1) ANS
CALL FRICMS ('CLRS CRN 6')
IF (ANS.EQ.1) GO TO 10
CALL TEK618
GO TO 20
CONTINUE
TRIP5=5.
CONTINUE
TRIP1=0.
10
20

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```

TRIP2=0.
TRIP3=0.
TRIP4=0.
WRITE (6,26) CREM
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,27) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,28) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,29) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,30) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,31) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,32) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,33) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,34) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,35) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,36) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,37) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,38) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,39) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,40) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,41) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,42) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,43) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,44) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,45) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,46) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,47) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,48) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,49) SPC LOD
READ (5,1) S (1,CLRSCRN 6)
CALL FRICMS (6,50) SPC LOD

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```

WRITE (6,2650)
READ (5,1) TEMP
CALL FRICMS (0,CLRSCRN 60)
WRITE (6,2820)
READ (5,1) IR
CALL FRICMS (0,CLRSCRN 60)
C*****
C*****
C*****
2.1 MAKE A ROUGH ESTIMATE OF GROSS WEIGHT
C*****
C*****
WRITE (6,1550)
READ (5,1) WG
CALL FRICMS (0,CLRSCRN 60)
WG=0.8*WG
WRITE (6,1600) WG
C*****
C*****
C*****
2.2 MAKE A ROUGH ESTIMATE OF THE MANUFACTURER'S EMPTY
C*****
C*****
C*****
WRITE (6,1580)
READ (5,1) WE
CALL FRICMS (0,CLRSCRN 60)
C*****
C*****
C*****
2.3 CALCULATE THE MAXIMUM TIP VELOCITY
C*****
C*****
C*****
A=1116.85
MACH=0.65
VMAX=MACH*A
PIE=3.1415927
RHOSL=0.0023769
C*****
C*****
C*****
2.4 DETERMINE THE ROTOR RADIUS
C*****
C*****
C*****
WRITE (6,1610) WG
READ (5,1) RL
CALL FRICMS (0,CLRSCRN 60)
R=SQR((WG/(PI*RL))
AREAMR=PI*RL**2
C*****
C*****
C*****
2.5 DETERMINE A FIRST-CUT ROTATIONAL VELOCITY
C*****
C*****
C*****
OMEGA=VMAX/R
C*****
C*****
C*****
2.6 MAKE A FIRST-CUT DETERMINATION OF THRUST
C*****
C*****
C*****
COEFFICIENT
C*****
C*****
C*****
CONTINUE
CT=WG/(AREAMR*RHOSL*VTIP**2)
40

```

```

C*****
C 2.7 DETERMINE THE BLADE SOLIDITY
C*****
C IF (TRIPL.EC.1.) GO TO 50
MAXV=VMAXF
VMAXF=VMAXF*1.151*5280.0/3600.0
CONTINUE
MU=VMAXF/VTIP
WRITE (6,1620) MU
WRITE (6,1640)
READ (5,*) EL
CALL FRICMS ('CLRSCRN 6')
SIGMA=CT/BL
C*****
C 2.8 DETERMINE THE NUMBER OF MAIN ROTOR BLADES
C*****
C IF (TRIPL.EC.1.) GO TO 60
WRITE (6,1650) ELADES
READ (5,*) ELADES
CALL FRICMS ('CLRSCRN 6')
CONTINUE
C*****
C 2.9 DETERMINE THE CHORD AND THE ASPECT RATIO
C*****
C CHORD=SIGMA*PIER/FLOAT(BLADES)
AR=R/CHORD
IF (AR.GT.20.) GO TO 80
IF (AR.LT.15.) GO TO 80
GO TO 90
CONTINUE
WRITE (6,1660) WG,WE,A,VMAX,DL,R,OMEGA,VTIP,CT,MU,BL,SIGMA,BLADES,
1CHORD
1CHORD
WRITE (6,1670) AR,OMEGA
WRITE (6,1670) AR,OMEGA
READ (5,*) CMEGA
CALL FRICMS ('CLRSCRN 6')
TRIPL=1.0
GO TO 40
CONTINUE
C*****
C 2.10 DETERMINE THE AVERAGE LIFT COEFFICIENT
C*****
C CL=(6.*CT)/SIGMA
C*****
C 2.11 CHOOSE AN AIRFOIL SECTION FOR THE MAIN ROTOR BLADES
C*****

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130 READ (5,*) TYPE
    CALL FRCMS (,CLRSCRN 6,*)
    CONTINUE
    IF (TYPE,NE.1,)* GO TO 160
    IF (TRIP2,EC.2,)* GO TO 140
    WG=173.701*E*.378
    CONTINUE
    STT=.264*EXF(.0135*HP)
    SB=194.274*ALOG(WG)-1306.779
    S=CHORD*(FLCAT(BLADES))*R
    W1=408.562*ALOG(S)-1142.917
    W2A=2.219*EXP(.0005*WG)
    W2B=19.131*ALOG(STT)-32.414
    W3=.00901*SB*.917
    IF (COLAT,NE.0,)* GO TO 150
    W4=.0539*WG+200.912
    CONTINUE
    W5=34.
    W6A=-.0896*TP+221.338*FLOAT(NENG)
    W6B=17.190*EXP(.0008*WG)
    W6C=.384*(FCEL/6.5)*.0717
    W7=(1.28E-1C)*WG*.3469
    W8=0.
    W9=24.571*EXP(.0004*HP)
    W10=0.
    W11=.51.0661*ALOG(SB)+367.947
    W12=-1.062.00451-122.282*ALOG(1120.354*EXP(.003*HP))
    W13=19.600*(EXP(.372*FLCAT(PEOPLE))+EXP(-.033*SB))
    W14=-22.371*ALOG(SB)+143.396
    W15=0.
    GO TO 170
    IF (TYPE,NE.2,)* GO TO 240
    IF (TRIP2,EC.2,)* GO TO 170
    WG=16235.43*ALOG(WE)-130252.76
    CONTINUE
    STT=.0376*HF-8.106
    S=636.081*EXP(.000011*WG)
    S=CHORD*(FLCAT(BLADES))*R
    W1=11.0702*WG+12.470
    W2A=.00438*WG+12.470
    W2B=2.411*STT-15.531
    W3=.282*SB*.272
    IF (COUNT,NE.0,)* GO TO 190
    IF (WG,GT.600,)* GO TO 180
    W4=.0225*EXP(.000062*WG+8.020)
    GO TO 190
    W4=301.577*ALOG(WG)-2319.890
    CONTINUE
180
190

```



```

200 W5=.02*EXP(.000062*WG+8.02)
210 IF (NENG.NE.1.) GO TO 200
    W6A=130.0+.451*HP
    GO TO 210
    W6A=(295.0+.188*HP)*FLOAT(NENG)
    W6B=(741.460*ALCG(HP)-4542.0420)
    W6C=(363.24*ALOG(FUEL/6.5)-1656.521)
    W7=210.858*EXP(.000059*WG)
    IF (NENG.NE.1.) GO TO 220
    W8=0.0
    GO TO 230
220 W8=190.0
230 W9=56.0975*ALOG(HP)-312.237
    W10=.00362*WG+11.553
    W11=481.735*ALOG(SB)-2794.53
    W12=.135*HP+77.823
    W13=.175*SB+22.*FLOAT(PEOPLE)-10.
    W14=122.468*ALOG(SB)-730.252
    W15=84.5
    GO TO 270
240 CONTINUE
    IF (TRIP2.EC.2.) GO TO 250
    WG=4.975*WE*.887
    CONTINUE
    STT=60.127*EXP(.000145*HP)
    SB=426.0378*EXP(.000045*WG)
    S=CHORC*(FLCAT(ELADES))*R
    W1=707.174*EXP(.00539*S)
    W2A=324.550*ALOG(WG)-3021.510
    W2B=-18.42.83*STT
    W3=2.9818*SB-1321.921
    IF (COUNT.NE.0.) GO TO 260
    W4=258.358*EXP(.000041*WG)
    CONTINUE
    W5=.014*(.2041*WG)*.1.136
    W6A=(344.+.510*HP)*FLOAT(NENG)
    W6B=(.999*HF*.959)
    W6C=(.454.615*(FUEL/6.5)**(-.0566))
    W7=.00334*WG*.1.224
    W8=139.0
    W9=68.266*ALOG(HP)-387.598
    W10=(6.63E-7)*WG*.1.863
    W11=.9.780*SE*.539
    W12=(1.6744.567*ALOG(HP)-108666.)*.536*1.90
    W13=.1159*SB+18.11*FLOAT(PEOPLE)
    W14=117.771*ALOG(SB)-710.594
    W15=-72.+.111*SB+3.49*FLOAT(PEOPLE)
270 CONTINUE

```

```

1+*W15
REVME=W1+W2A+W28+W3+W4+W5+W6A+W6B+W6C+W7+W8+W9+W10+W11+W12+W13+W14
REVWG=REVWE+FUEL+USELOD
WRITE (6,1760) B,PIHP,POHP,PTHP,WE,FUEL,PEOPLE,USELOD,NENG,WG,SIGM
1A,R1HP,W1,W2A,W2B,W3,W4
WRITE (6,1770) W5,W6A,W6B,W6C,W7,W8,W9,W10,W11,W12,W13,W14,W15,REV
1WE,REVWG (8,1760) B,PIHP,POHP,PTHP,WE,FUEL,PEOPLE,USELOD,NENG,WG,SIGM
1A,R1HP,W1,W2A,W2B,W3,W4
WRITE (6,1770) W5,W6A,W6B,W6C,W7,W8,W9,W10,W11,W12,W13,W14,W15,REV
1WE,REVWG
C*****
C3.3 VALIDATE DISC LOADING
C*****
WRITE (6,1800) WG
READ (5,*) ANS
CALL FRICMS (1,CLRSCRN 60)
IF (ANS.NE.1.) GO TO 280
WRITE (6,1810)
CALL FRICMS (5,*) CL
WG=REVWG
WE=REVWE
TRIP1=1.
TRIP2=2.
GO TO 300
280 CONTINUE
C*****
C3.4 ESTABLISH FIGURE OF MERIT AT APPROXIMATELY 0.75
C*****
M=(PI/PT)*100.
WRITE (6,1780) M
CONTINUE
WRITE (6,1790)
READ (5,*) ANS
CALL FRICMS (1,CLRSCRN 60)
IF (ANS.NE.1.) GO TO 300
TRIP1=1.
TRIP2=2.
WG=REVWG
WE=REVWE
OLD=REVWG
GO TO 300
300 IF (ANS.NE.2.) GO TO 310
WRITE (6,2270) CHORD
WRITE (6,1810)
READ (5,*) CHORD

```



```

NN= AINT (MAXV/5. )+1
N= AINT (MAXV/5. )+11
DO 400 I=1,N
VF= KNTS*1.151*5280./3600.
PPF= 5*RHO*SL*(VF**3)*EFPAFF
MU= VF/VTIP
POF= (1.+4.3*MU**2)*PO
POF= POF/550.
VI= SQRT(WG/(2.*RHO*SL*AREAMR))
VI T= VI*SQRT((- (VF**2/(2.*VI**2)))
+SQRT((VF**2/(2.*VI**2))*2)+1.))
1 PITLF= (1./8)*WG*VIT
PITLF= PITLF/550.
PTF= PITLF+PCF+PPF
MACHT= (VF+VTIP)/A
PPFS(I)= PPF
POFS(I)= POF
PITLFS(I)= PITLF
PTFS(I)= PTF
WRITE (6,1850) KNTS,MACHT,PITLF,POF,PPF,PTF
KNTS= KNTS+5.
CONTINUE
TEMP= TEMP+460.
THETA= TEMP/518.688
CONST= 6.875-5E-6
PRESS= 2116.22*(1.-CONST*PA)**5.2561
SIG= PRESS/2116.22
RHOALT= .0023769*SIG*THETA
AALT= SQRT(1.4*32.174*53.3*TEMP)
WRITE (6,1860)
WRITE (8,1860)
KNTS= 0.
DO 410 I=1,N
VF= KNTS*1.151*5280./3600.
PPF= 5*RHOALT*(VF**3)*EFPAFF
MU= VF/VTIP
PO= .125*SIG*MA*COO*RHOALT*AREAMR*VTIP**3
POF= (1.+4.3*MU**2)*PO
POF= POF/550.
VI= SQRT(WG/(2.*RHOALT*AREAMR))
VI T= VI*SQRT((- (VF**2/(2.*VI**2)))
+SQRT((VF**2/(2.*VI**2))*2)+1.))
1 PITLF= (1./8)*WG*VIT
PITLF= PITLF/550.
PTF= PITLF+PCF+PPF

```

```

MACHT=(VF+VTIP)/AALT
PPFA(I)=PPF
POFA(I)=POF
PITLFA(I)=PITLF
PTFA(I)=PTF
WRITE(6,1850) KNTS,MACHI,PITLF,POF,PPF,PTF
WRITE(8,1850) KNTS,MACHT,PITLF,POF,PPF,PTF
KNTS=KNTS+5.
CONTINUE
410 *****
C ***** PRELIMINARY SIZING OF TAIL ROTOR *****
C *****
4.1 *****
RTR=1.3*SQRT(WG/1000.)
WRITE(6,1860) RTR
WRITE(8,1880) RTR
OMEGTR=4.5*CMEGA
WRITE(6,1850) CMEGTR
WRITE(8,1850) CMEGTR
CDOTR=1.38*CDO
WRITE(6,1900) CDOTR
WRITE(8,1900) CDOTR
IF (ITRIP3.EQ.3.) GO TO 420
WRITE(6,1910)
READ(5,*) PLADTR
CALL FRUE (CLRSCRN 6)
CONTINUE
420 LTR=RTR+RTR+.5*EQ.3.) GO TO 430
IF (LTR(6,1920)
READ(5,*) ARTR
CALL FRUE (CLRSCRN 6)
CONTINUE
430 CHORDT=RTR/ARTR
SIGTR=(FLOAT(BLADTR)*CHORDT)/(PIE*RTR)
*****
4.2 DETERMINE TAIL ROTOR POWER REQUIRED AT HOVER *****
*****
AREATR=PIE*ARTR**2
TTIPTR=(CMEGTR*LTR)
VTIPTR=TTIPTR*ARTR*RHOSL*VTIPTR**2)
CTTR=TTTR/(AREATR*CTTR)/FLOAT(BLADTR)
BTTR=1.-SQRT(2.*CTTR)*(TTTR**1.5/SQRT(2.*RHOSL*AREATR))
PITLTR=(1./BTTR)*CDOTR*RHOSL*AREATR*(VTIPTR**3)
PTRHP=.125*SIGTR*POTR
PTRHP=PTRHP/550.
CTTA=TTTR/(AREATR*RHOSL*VTIPTR**2)
BTA=1.-SQRT(2.*CTTA)/FLOAT(BLADTR)

```



```

CTTR=TTTR/(A*FEATR*(VTIPTR**2)*RHOALT)
BTTR=1.-SQRT(2.*CTTR)/FLOAT(BLADTR)
VITR=SQRT(TTR/(2.*RHOALT*A*REATR))
VITR=VITR*SQRT((-(VF**2/(2.*VITR**2)))
1+SQRT((VF**2/(2.*VITR**2))*2)+1.))
PITLTF=(1./ETR)*TTR*VITR
PITLTF=PITLTF/550.
PITRFP=PITLTF+POTRF
POTRFA(I)=PITRFP
PITRFA(I)=PITLTF
PITRFA(I)=PITRFP
MTTR=(VF+VTIPTR)/AALT
WRITE(6,1950) KNTS,MTTR,PITLTF,POTRF,PITRFP
WRIT= (8,1950) KNTS,MTTR,PITLTF,POTRF,PITRFP
KNTS=KNTS+5.
CONTINUE
450 *****
C *****
C *****
4. 4 VERTICAL STABILIZER *****
*****
***** IF (TRIP3.EC.3.) GO TO 460 *****
*****
WRITE(6,2960)
READ(5,*) EVS
CALL FRICMS ('CLRSCRN 6')
WRITE(6,2970) SIGTR
READ(5,*) VS
CALL FRICMS ('CLRSCRN 6')
CONTINUE
460 VF80=80.*1.151*5280./3600.
VF160=160.*1.151*5280./3600.
ARVS=BVS*2/V5
TTR80=(PTFS(17)*550.)/(LTR*OMEGA)
TTR160=(PTFS(17)*550.)/(LTR*OMEGA)
CL80=(2.*TTR80)/(RHOSL*VF80**2*VS)
CL160=(2.*TTR160)/(RHOSL*VF160**2*VS)
CLARVS=((2.*PIE)/(2.*SQRT(ARVS**2*2.*4.)))*ARVS*PIE/180.
A80=((CL80-.4)/CLARVS)
A160=((CL160-.4)/CLARVS)
WRITE(6,2980) CL80,CL160,A80,A160
WRITE(8,2980) CL80,CL160,A80,A160
*****
5. 1 DETERMINE RETREATING BLADE STALL EFFECTS *****
*****
5. 2 DETERMINE STALL POWER INCREMENT *****
*****
5. 3 DETERMINE COMPRESSIBILITY EFFECTS *****
*****
KNT=0.
TWIST=-10.*PIE/180.

```



```

470 IF (TRIF3.EC.3.) GO TO 470
WRITE (6,2930)
READ (5,*) MCRO
CALL FRICMS (.CLRSCRN 6*)
WRITE (6,2940)
READ (5,*) CLMAX
CALL FRICMS (.CLRSCRN 6*)
CONTINUE
AMAX=CLMAX/CLA R,C HORD,BLADES,WG,VTIP,EFPAFF,NENG,H,RHOALT,AALT,TW
1WRITE (8,2920) AMAX,CLA,CDO,MCRO
CT=WG/(AREA*RHQALT*(VTIP**2))
IF (H/D.GT.1.55) PPOGE=1.0
B=1.0-(SCRT(2.*CT)/FLOAT(BLADES))
WRITE (8,2910) CT,AREAMR,SIGMA,B,PPOGE
VMAX=SQR(WG/2./RHOALT/AREAMR)*(4./EFPAFF/AREAMR)**.333334
VMAXK=VMAX/1.68894
VELMAX=VMAXK
DO 630 I=1,N
WRITE (8,2880) KNT
VF=KNT*1.151*5280./3600.
MU=VF/VTIP
VL=VF**2/(2.*VI**2)
C1=(B**2+.5*MU**2)
C2=(B**2-.5*MU**2)
T1=.5*C1
T2=(B**3)/3.+(MU**2*B*.5)
T3=(B**2/4.)*((B**2+MU**2)
T4=(MU/2.)*(B**2+MU**2/4.)
A11=((B**2*MU*.5-(MU**3/8.))*4.)/(B**2*C2)
A12=(8.*MU*B)/(3.*C2)
A13=(2.*MU**2)/C2
A14=(B**2+1.5*MU**2)/C2
IF (VF.GT.0.) GO TO 480
ALPHA=0.
WRITE (8,2900) ALPHA
LAMBDA1=-SQR(CT/2.)
IF (MU.LE.0.1) GO TO 510
IF (VF.EQ.0.) DP=0.
DP=PPFA(I)*550/VF
ALPHA=-CP/WC
CONTINUE
LAMBDA=-CT/SQR(2*(LAMBDA1**2)+MU**2)+MUTAN(ALPHA)
DLAMBDA=LAMBDA-LAMBDA1
LAMBDA1=LAMBDA
LREF=ABS(DLAMB)
IF (LREF.GE.LERR) GO TO 500

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```

510 LAMBDA=LAMBDA1
E1=(2.*CT)/(SIGMA*CLA)
E2=T1*LAMBDA
E3=T3*TWIST
D1=((2.*CT)/(SIGMA*CLA))-T1*LAMBDA-TWIST*T3
D2=-((A11*LAMBDA)-(TWIST*A13)
CYCLIC=((D2*T2)-(D1*A12))/(T2*A14-T4*A12)
COLL=(D1-T4*CYCLIC)/T2
CYCD=CYCLIC*57.29578
COLLD=COLL*57.29578
THETA2=CYCLIC*57.29578
WRITE(8,2820) A11,A12,A13,A14,T1,T2,T3,T4,LAMBDA
GAM=AMAX-COLL+CYCLIC
CS=MU*GAM+LAMBDA
BS=-MU*TWIST-GAM
RT=(BS*2-4.*TWIST*CS)
WRITE(8,2860) RT
IF (RT) 560,520,520
XS=(-BS+SQR(TRT))/ (2.*TWIST)
X0=-XS-BSTWIST
IF (XS-1.) 530,560,560
IF (XS) 560,540
CPS=(SIGMA/(24.*PIE))*((1.-MU)**2)*(1.-XS)*SQR(1.-XS**2)
IF ((XS+X0)/2.-GE.1.0) KS=1.0
IF ((XS+X0)/2.-GT.1.0) GO TO 550
KS=- (BS/(2.*TWIST)+XS)/(1.-XS)
CPS=KS*CPS
GO TO 570
CPS=0.0
PS=CPS*RHOALT*AREAMR*(VTIP**3)/550.
WRITE(8,2840) KS,CPS
A90=COLL+CYCLIC+TWIST+LAMBDA/(1.+MU)
A270=COLL-CYCLIC+TWIST+LAMBDA/(1.+MU)
A90D=A90*57.29278
A270D=A270*57.29278
WRITE(8,2850) CYCD,COLL,A90D,A270D
MTIP=(VF+VTIP)/AALT
MCRIT=MCR0-CLA*A90*.113
IF (MTIP-1.) 590,580,580
WRITE(8,2850)
GO TO 610
MD=MTIP-MCRIT-0.06
IF (MD) 610,600,600
CPC=SIGMA*(C.012*MD+.1*(MD**3))
GO TO 620
CPC=0.0
610

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620 MD=0.0
    PC*RHCAIT*AREAMR*(VTIP**3)/550.
    PCMPA(I)=PMES+PS
    WRITE(8,2870) MTIP,MCRTIT,MD,CPC,PITLFA(I),POFA(I),PPFA(I),PMBS,PS
1    PCMPA(I)
    TSHP=1.13*PCMPA(I)+10.0
    VOPT=SQR(WG/RHOAL T/AREAMR*SQR T(AREAMR/3./EFPAFF))
    VOPTK=VCPT/1.68894
    KNT=KNT+5.
    CONTINUE
630 K=MAXV +40
    WRITE(6,2430)
    WRITE(8,2430)
    DO 690 I=1,K
        VF=KNT*1.151*5280./3600.
        MU=VF/VTIP
        PP=(.5*RRHOAL T*EFPAFF*(VF**3))/550.
        C1=(8**2+.5*MU**2)
        C2=(8**2-.5*MU**2)
        T1=(5*C1)
        T2=(8**2*8*.5)
        T3=(8**2/4.)*(8**2+MU**2)
        T4=(MU/2.)*(8**2+MU**2/4.)
        A11=((8**2*MU*.5-(MU**3/8.))*4.)/(8**2*C2)
        A12=(8.*MU*8)/(3.*C2)
        A13=(2.*MU*8**2)/C2
        A14=(8**2+1.5*MU**2)/C2
        IF (VF.GT.0.) GO TO 640
        ALPHA=0.
        GO TO 650
640 ALPHA=-(FP*550.)/VF/WG
650 LAMBDA1=-SQR T(CT/2.)
        IF (MU.LE.0.1) GO TO 670
        LAMBDA=-CT/SQR T(2*(LAMBDA1**2)+MU**2)+MU*ATAN(ALPHA)
660 DLAMB=LAMBDA-LAMBDA1
        LAMBDA1=LAMBDA
        LREF=ABS(DLAMB)
        IF (LREF.GE.LERR) GO TO 660
        IF (MU.LE.0.1) LAMBDA=LAMBDA1
        E1=(2.*CT)/(SIGMA*CLA)
        E2=T1*LAMBDA
        E3=T3*TWIST
670 D1=((2.*CT)/(SIGMA*CLA))-T1*LAMBDA-TWIST*T3
        D2=-((A11*LAMBDA)-(TWIST*A13))
        CYCLIC=((D2*T2)-(D1*A12))/(T2*A14-T4*A12)
        COLL=(D1-T4*CYCLIC)/T2
        THETA0=CCLL*57.29578

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        680 THETA2=CYCLIC*57.29578
        690 A270=CCLL-CYCLIC+TWIST+LAMBDA/(1.+MU)
        DA270=A270-AMAX
        DREF=ABS(DA270)
        IF (A2700.L1.12.) GO TO 680
        IF (A2700.GT.13.) GO TO 680
        VSK=VF/1.68894
        WRITE (6,2440) VSK,A270D
        WRITE (8,2440) VSK,A270D
        CONTINUE
        KNT=KNT+1.
        CONTINUE
        KNT=0.
        CT=WG/(AREAMR*RHOSL*(VTIP**2))
        IF (H/D.GT.1.55) PPOGE=1.0
        B=1.0-(SQRT(2.*CT)/FLOAT(BLADES))
        VMAX=SQRT(WG/2./RHOSL/AREAMR)*(4./(EFP AFF/AREAMR))**.333334
        VMAXK=VMAX/1.68894
        DO 850 I=1,N
        VF=KNT*1.151*5280./3600.
        MU=VF/VTIP
        VL=VF**2/(2.*VI**2)
        C1=(B**2+.5*MU**2)
        C2=(B**2-.5*MU**2)
        T1=.5*C1
        T2=(B**3)/3.+(MU**2*B*.5)
        T3=(B**2/4.)*(B**2+MU**2)
        T4=(MU/2.)*(B**2+MU**2/4.)
        A11=((B**2*MU*.5-(MU**3/8.))*4.)/(B**2*C2)
        A12=((8.*MU*B)/(3.*C2)
        A13=((2.*MU**2)/C2
        A14=(B**2+1.5*MU**2)/C2
        IF (VF.GT.0.) GO TO 700
        ALPHA=0.
        LAMBD1=-SQRT(CT/2.)
        IF (MU.LE.0.1) GO TO 730
        IF (VF.EQ.0.) DP=0.
        IF (VF.EQ.0.) GO TO 710
        DP=PPFS(I)*550/VF
        ALPHA=-CP/WG
        CONTINUE
        710 LAMBDA=-CT/SQRT(2*(LAMBD1**2)+MU**2)+MU*TAN(ALPHA)
        720 DLAMB=LAMBDA-LAMBD1
        LAMBD1=LAMBCA
        LREF=ABS(DLAMB)
        IF (LREF.GE.LERR) GO TO 720
        730 LAMBDA=LAMBC1

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E1=(2.*CT)/(SIGMA*CLA)
E2=T1*LAMBDA
E3=T3*TWIST/(SIGMA*CLA)-T1*LAMBDA-TWIST*T3
D1=((2.*CT)/(SIGMA*CLA)-T1*LAMBDA)/(TWIST*A13)
D2=((A11*LAMBDA)-(D1*A12))/(T2*A14-T4*A12)
CYCLIC=((D2*T2)-(D1*A12))/(T2*A14-T4*A12)
COLL=((C1-T4*CYCLIC)/T2
THETA0=CCLL*57.29578
THETA2=CYCLIC*57.29578
GAM=AMAX-COLL+CYCLIC
CS=MU*GAM+LAMBDA
BS=-MU*TWIST-GAM
RT=(BS**2-4.*TWIST*CS)
IF (RT) 780,740,740
XS=(-BS+SQR(RT))/(2.*TWIST)
X0=-XS-BSTWIST
IF (XS) 780,750,780,780
IF (XS) 780,780,760
CPS=(SIGMA/(24.*PIE))*((1.-MU)**2)*(1.-XS)*SQR(1.-XS**2)
IF ((XS+X0)/2..GE.1.0) KS=1.0
IF ((XS+X0)/2..GT.1.0) GO TO 770
KS=(-(BS/(2.*TWIST)+XS)/(1.-XS)
CPS=KS*CPS
GO TO 790
CPS=0.0
PS=0.0
PS=CPS*RHOSL*AREAMR*(VTIP**3)/550.
A90=COLL+CYCLIC+TWIST+LAMBDA/(1.+MU)
A270=COLL-CYCLIC+TWIST+LAMBDA/(1.+MU)
A90D=A9C*57.29278
A270D=A270*57.29278
MTIP=(VF+VTIP)/AALT
MCRIT=MCR0-CLA*A90*.113
IF (MTIP-1.) 810,800,800
CONTINUE
GO TO 830
MD=MTIP-MCRIT-0.06
IF (MD) 830,830,820
CPC=SIGMA*(C.012*MD+.1*(MD**3))
GO TO 840
CPC=0.0
MD=0.0
PMB=0.0
PMB=0.0
PC*RHCSL*AREAMR*(VTIP**3)/550.
PCMP(I)=PMB+PS
TCHP=1.13*PCMP(I)+10.0
VOPT=SQR(WG/RHCSL/AREAMR*SQR(AREAMR/3./EFPAFF))
VOPTK=VOPT/1.68894
KNT=KNT+5.

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740

750
760

770

780

790

800

810

820

830

840

```

850 CONTINUE
KNT=0. I=1.151*5280./3600.
DO 900 K=1,151*5280./3600.
VF=KNT*.1*VF/VFIP
MU=VF/VFIP
PP=(.5*RHOSL*EFPAFF*(VF**3))/550.
C1=(B**2+.5*MU**2)
C2=(B**2-.5*MU**2)
T1=.5*C1
T2=(B**2)/3.+(MU**2*B*.5)
T3=(B**2/4.)*(B**2+MU**2)
T4=(MU/2.)*(B**2+MU**2/4.)
A11=((B**2*MU*.5-(MU**3/8.))*4.)/(B**2*C2)
A12=(B**2*MU)/(3.*C2)
A13=(2.*MU**2)/C2
A14=(B**2+1.5*MU**2)/C2
IF (VF.GT.0.) GO TO 860
ALPHA=0.
GO TO 870
860 ALPHA=PP*.50./VF/WG
870 LAMBDA1=-SQRT(C1/2.)
IF (MU.LE.0.1) GO TO 890
880 LAMBDA=-CT/SQRT(2*(LAMBDA1**2)+MU**2)+MU*TAN(ALPHA)
LAMBDA1=LAMBDA-LAMBDA1
LAMBDA1=LAMBDA1
LREF=ABS(DLAMB)
IF (LREF.GE.0.1) GO TO 880
IF (MU.LE.0.1) LAMBDA=LAMBDA1
E1=(2.*LAMBDA)
E2=T1*TWIST
E3=T3*TWIST
D1=((2.*CT)/(SIGMA*CLA))-T1*LAMBDA-TWIST*T3
D2=-((A11*LAMBDA)-(TWIST*A13)
CYCLIC=((D2*T2)-(D1*A12))/(T2*A14-T4*A12)
COLL=((D1-T4*CYCLIC)/T2
THETA0=COLL*57.29578
THETA2=CYCLIC*57.29578
A270D=COLL-CYCLIC+TWIST+LAMBDA/(1.+MU)
A270=A270D-AMAX
DA270=ABS(DA270)
DREF=ABT+1.
KNT=KNT+1.
900 CONTINUE
WRITE(6,2950)
READ(5,1) FBS
CALL FRICMS(,CLRSCRN 6)
***** DETERMINE TOTAL POWER REQUIRED *****
C***** 5.4 *****

```

```

C*****
PTAH=PTAH/550.      PTAH
WRITE (8,1960) PTAH
KNOTS (1)=0.
WRITE (6,1970)
WRITE (8,1970)
DO 910 I=1,N
  POX(I)=POTRFS(I)+PITRFS(I)
  PPX(I)=PPFS(I)
  PTX(I)=PCX(I)+PIX(I)+PCMPS(I)
  WRITE (6,1980) KNOTS(I),POX(I),PPX(I),PCMPS(I),PTX(I)
  KNOTS(I+1)=KNOTS(I)+5.
CONTINUE
WRITE (6,1950)
WRITE (8,1950)
KNOTS (1)=0.
DO 920 I=1,N
  POY(I)=POTRFA(I)
  PIY(I)=PITLFA(I)
  PPY(I)=PPFA(I)
  PTY(I)=POY(I)+PIY(I)+PCMPA(I)
  WRITE (6,1990) KNOTS(I),POY(I),PIY(I),PCMPA(I),PTY(I)
  KNOTS(I+1)=KNOTS(I)+5.
CONTINUE
*****
5.5 DETERMINE THE RSHP REQUIRED AT MAXIMUM VELOCITY
*****
PADJS=PTX(NN)+PCMPS(NN)
PADJA=PTY(NN)+PCMPA(NN)
IF (PADJS.GT.PADJA) GO TO 930
RRSHP=PACJA
GO TO 940
RRSHP=PADJS
CONTINUE
WRITE (6,2000) RRSHP
*****
5.6 DETERMINE RSHP FOR HOVER CEILING, IGE
*****
RHOS=.0023769*(1.-CONST*HOVIGE)**4.2561
CTH=WG/(AREAMR*RHOS*VTIP**2)
BH=1.-SQRT(2.*CTH)/FLOAT(BLADESI)
PITLH=(1./BH)*((WG**1.5/SQRT(2.*RHOS*AREAMR))

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```

PPQGEH=-.1276*(H/D)**4+.708*(H/D)**3-1.4569*(H/D)**2+1.3432*(H/D)+
1.5147
PITLGH=PPOGEH*PITLH
POH=.125*SIGMA*CDO*RHOS*AREAMR*VTIP**3
TTR=PTH/(OMEGA*LTR)
VTIPR=CMEGTR*RTR
CTIR=TTR/(AREATR*RHOS*VTIPR**2)
BTIR=1.-SQRT(2.*CTIR)/FLOAT(BLADTR)
PITLH=(1./PTR)*(TTR**1.5/SQRT(2.*RHOS*AREATR))
POTRH=.125*SIGTR*CDOTR*RHOS*AREATR*(VTIPR**3)
PTACH=PTH+PTTRH
PTACH=PTACH/550.
*****
5.7 DETERMINE THE MAXIMUM RSHP REQUIRED
*****
IF (PTACH.GT.RRSH) GO TO 950
RSHPM=RRSH
GO TO 960
950 RSHPM=PTACH
960 CONTINUE
*****
5.8 DETERMINE THE TOTAL ESHP REQUIRED
*****
ESHPR=(.1*RSHPM*FLOAT(NENG-1))+1.03*RSHPM+10.
WRITE (6,2010) NENG,ESHPR
*****
6.1 SELECT TYPE AND NUMBER OF ENGINES
*****
6.2 INSTALLATION WEIGHT
*****
WRITE (6,2020) NENG
WRITE (6,2030)
READ (5,*)ANS
CALL FRTCMS (,CLRSCRN 6)
IF (ANS.NE.1) GO TO 970
WRITE (6,2040)
CALL FRTCMS (,CLRSCRN 6)
GO TO 960
CONTINUE
HL=(AASL)Y*AFHPY)
PM(1)=.025
WRITE (6,2050)
DO 1100 I=1,6

```

970


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YMC(I) = AFHPY*PM(I)
YDC(I) = AFHPY*OC(I)
NRPL(I) = ((HL/MTBR(I))-1.)
NXRPL(I) = AINT((HL)/MTBR(I))-1.)
IF (NRPL(I).NE.1.0) GO TO 980
GO TO 1090
IF (NRPL(I).NE.2.) GO TO 990
GO TO 1090
IF (NRPL(I).NE.3.) GO TO 1000
GO TO 1090
IF (NRPL(I).NE.4.0) GO TO 1010
GO TO 1090
IF (NRPL(I).NE.5.) GO TO 1020
GO TO 1090
IF (NRPL(I).NE.6.) GO TO 1030
GO TO 1090
IF (NRPL(I).NE.7.0) GO TO 1040
GO TO 1090
IF (NRPL(I).NE.8.) GO TO 1050
GO TO 1090
IF (NRPL(I).NE.9.) GO TO 1060
GO TO 1090
IF (NRPL(I).NE.10.0) GO TO 1070
GO TO 1090
IF (NRPL(I).NE.11.) GO TO 1080
GO TO 1090
CONTINUE
NRPL(I) = NXRFL(I)+1.
CONTINUE
EIW(I) = CW(I) + IF(I)*DW(I)
RC(I) = 1.35*IC(I)
SV(I) = .8*IC(I)
WFO(I) = .35*SHPM(I)
LAMFR(I) = 1./MTBF(I)
RELY(I) = EXP((-LAMFR(I))*AFHPF)
AVAIL(I) = MTEMA(I)/(MTBMA(I)+MDT(I))
LCC(I) = (RDC(I)+IC(I)+HL*(YOC(I)+YMC(I))
1 +NRPL(I))*RC(I)-SV(I))*0.0001
MAINT(I) = MDT(I)/AFHPF
CONTINUE
WR ITE (6,210) (DW(I),I=1,6)
WR ITE (8,210) (DW(I),I=1,6)
WR ITE (6,2110) (LCC(I),I=1,6)
WR ITE (8,2110) (LCC(I),I=1,6)
WR ITE (6,2120) (MTBR(I),I=1,6)
WR ITE (8,2120) (MTBR(I),I=1,6)
WR ITE (6,2130) (NRPL(I),I=1,6)
WR ITE (8,2130) (NRPL(I),I=1,6)
1100

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1110 IF (NRPLM(I).NE.2.) GO TO 1120
1120 IF (NRPLM(I).NE.3.) GO TO 1130
1130 IF (NRPLM(I).NE.4.0) GO TO 1140
1140 GO TO 1220
1150 IF (NRPLM(I).NE.5.) GO TO 1150
1150 IF (NRPLM(I).NE.6.) GO TO 1160
1160 IF (NRPLM(I).NE.7.0) GO TO 1170
1170 IF (NRPLM(I).NE.8.) GO TO 1180
GO TO 1220

(RDC(I),I=1,6)
(RDC(I),I=1,6)
(IC(I),I=1,6)
(IC(I),I=1,6)
(YMC(I),I=1,6)
(YMC(I),I=1,6)
(YOC(I),I=1,6)
(YOC(I),I=1,6)
(RC(I),I=1,6)
(RC(I),I=1,6)
(SV(I),I=1,6)
(SV(I),I=1,6)
(AVAIL(I),I=1,6)
(AVAIL(I),I=1,6)
(RELY(I),I=1,6)
(RELY(I),I=1,6)
(MAINT(I),I=1,6)
(MAINT(I),I=1,6)
(SHPM(I),I=1,6)
(SHPM(I),I=1,6)
NENG
NENG
DO 1230 I=1,6
DWM(I)=CH(I)*FLOAT(NENG)
ICHPM(I)=IC(I)*FLOAT(NENG)
SCHPM(I)=SHPM(I)*FLOAT(NENG)
RDCM(I)=RDC(I)*FLOAT(NENG)
MTBRM(I)=MTBR(I)
YCM(I)=YMC(I)*FLOAT(NENG)
YOCM(I)=YOC(I)*FLOAT(NENG)
NXRPLM(I)=((FL/MTBR(I))-1.)*FLOAT(NENG)
IF (NRPLM(I).NE.1.0) GO TO 1110
GO TO 1220
IF (NRPLM(I).NE.2.) GO TO 1120
GO TO 1220
IF (NRPLM(I).NE.3.) GO TO 1130
GO TO 1220
IF (NRPLM(I).NE.4.0) GO TO 1140
GO TO 1220
IF (NRPLM(I).NE.5.) GO TO 1150
GO TO 1220
IF (NRPLM(I).NE.6.) GO TO 1160
GO TO 1220
IF (NRPLM(I).NE.7.0) GO TO 1170
GO TO 1220
IF (NRPLM(I).NE.8.) GO TO 1180
GO TO 1220

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1180 IF (NRPLM(I).NE.9.) GO TO 1190
1190 GO TO 1220
1200 IF (NRPLM(I).NE.10.0) GO TO 1200
1210 GO TO 1220
1220 IF (NRPLM(I).NE.11.) GO TO 1210
1230 GO TO 1220
      CONTINUE
      NRPLM(I)=(NXRPLM(I)+1.)
      CONTINUE
      EIW(I)=FLOAT(NENG)
      EICM(I)=1.35*ICM(I)
      SVM(I)=.8*ICM(I)
      WCOM(I)=.35*SHPM(I)
      LAMFR(I)=EXP((-LAMFR(I))*AFHPI)
      RELYM(I)=(MTBMA(I))/(MTBMA(I)+MDT(I))
      AVAILM(I)=(FLCAT(NENG))*RDC(I)+IC(I)+HL*(YOC(I)
1+YMC(I))+NRPL(I)*RC(I)-SV(I))*0001
      MAINTM(I)=(MDT(I)/AFHPI)
      CONTINUE
      WR ITE (6,21,10) (DWM(I),I=1,6)
      WR ITE (8,21,10) (DWM(I),I=1,6)
      WR ITE (6,21,10) (LCCM(I),I=1,6)
      WR ITE (8,21,10) (LCCM(I),I=1,6)
      WR ITE (6,21,20) (MTBRM(I),I=1,6)
      WR ITE (8,21,20) (MTBRM(I),I=1,6)
      WR ITE (6,21,30) (NRPLM(I),I=1,6)
      WR ITE (8,21,30) (NRPLM(I),I=1,6)
      WR ITE (6,21,40) (RDCM(I),I=1,6)
      WR ITE (8,21,40) (RDCM(I),I=1,6)
      WR ITE (6,21,50) (ICM(I),I=1,6)
      WR ITE (8,21,50) (ICM(I),I=1,6)
      WR ITE (6,21,60) (YMC(I),I=1,6)
      WR ITE (8,21,60) (YMC(I),I=1,6)
      WR ITE (6,21,70) (YOCM(I),I=1,6)
      WR ITE (8,21,70) (YOCM(I),I=1,6)
      WR ITE (6,21,80) (RCM(I),I=1,6)
      WR ITE (8,21,80) (RCM(I),I=1,6)
      WR ITE (6,21,90) (SVM(I),I=1,6)
      WR ITE (8,21,90) (SVM(I),I=1,6)
      WR ITE (6,22,10) (AVAILM(I),I=1,6)
      WR ITE (8,22,10) (AVAILM(I),I=1,6)
      WR ITE (6,22,20) (RELYM(I),I=1,6)
      WR ITE (8,22,20) (RELYM(I),I=1,6)
      WR ITE (6,22,30) (MAINTM(I),I=1,6)
      WR ITE (8,22,30) (MAINTM(I),I=1,6)
      WR ITE (6,22,40) (SHPM(I),I=1,6)
      WR ITE (8,22,40) (SHPM(I),I=1,6)

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WRITE (6,2450) ESHPR
WRITE (8,2450) ESHPR
READ (5,*) ENGSEL
CALL FRICMS (,CLRS CRN 6,)
C*****
C 6.3 REVISE GROSS WEIGHT AND POWER REQUIRED *****
C*****
EW=W6A+W6B
EWNEW=EIWM(ENGSEL)+WXOM(ENGSEL)
WGNEW=EWNEW+REVWG-EW
WRITE (6,2300) REVWG, WGNEW
WRITE (8,2300) REVWG, WGNEW
COMPAR=1.-REVWG/WGNEW
IF (COMPAR.LE..1) GO TO 1250
WG=WGNEW
DO 1240 I=1,6
  DWCM(I)=0.
  LC CM(I)=0.
  MT BRM(I)=0.
  NR PLM(I)=0.
  RD CM(I)=0.
  ICM(I)=0.
  YMC M(I)=0.
  YOC M(I)=0.
  RCM(I)=0.
  SVM(I)=0.
  AVAILM(I)=0.
  RELYM(I)=0.
  MAINTM(I)=0.
  SHPRM(I)=0.
  NXRPLM(I)=0.
  EIWM(I)=0.
  WXOM(I)=0.
  LC CM(I)=0.
CONTINUE
TRIP3=3.
GO TO 120
IF (COMPAR.(E.-.1) GO TO 1270
WG=WGNEW
DO 1260 I=1,6
  DWCM(I)=0.
  LC CM(I)=0.
  MT BRM(I)=0.
  NR PLM(I)=0.
  RD CM(I)=0.
  ICM(I)=0.
  YMC M(I)=0.

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1240

1250

```

YOCM(I)=0.
RCM(I)=C.
SVALM(I)=0.
AVAILM(I)=0.
RELYM(I)=0.
MAINTM(I)=0.
SHPRM(I)=0.
NXRPLM(I)=0.
EIWM(I)=0.
WXOM(I)=0.
LCOM(I)=0.
CONTINLE
TRIP3=3.20
1260 GO TO 1270
1270 CONTINUE
C*** 7.1 DETERMINE FUEL FLOW RATES ***
C*** WR ITE (6,2250) L) * SHPM(ENGSEL) * FLOAT(NENG) ***
C*** WFM=SFCC(ENGSEL) * SHPC(ENGSEL) * FLOAT(NENG) ***
C*** WFN=SFCC(ENGSEL) * SHPN(ENGSEL) * FLOAT(NENG) ***
C*** WR ITE (6,2260) WFM, WFN, WFC ***
C*** 7.2 DETERMINE FUEL FLOW PER HORSEPOWER ***
C*** BE TA= ( WFM-WFC) / (SHPM(ENGSEL) - ***
1 AL PHA= (SHPM(ENGSEL) * FLOAT(NENG) - ***
1 SHPC(ENGSEL) * FLOAT(NENG) ) ***
C*** 7.3 COMPUTE THE INTERCEPT AT SPECIFICATION CONDITIONS ***
C*** PRESS=2116.688 * (1.-CONST*PA) ***
C*** TEMP=5116.688 * (1.-CONST*PA) ***
C*** THETA=PRESS/2116.688 * SQR(T(THETA) ***
ZHI=ALPHA * PRESS * DELTA * ZHI ***
WR ITE (6,2280) TEMP, PRESS, ALPHA, THETA, DELTA, ZHI ***
C*** 7.4 DETERMINE THE ZERO VELOCITY HORSEPOWER INCREMENT ***
C*** PSHP= (FLOAT(NENG) * ALPHA * DELTA * SQR(T(THETA))) / BETA ***
WR ITE (6,2730)
READ (5,*) TYPEM

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IF (TYPEFEM.NE.1.) GO TO 1280
FSLT=45.9
GO TO 1300
1280 IF (TYPEFEM.NE.2.) GO TO 1290
FSLT=50.1
GO TO 1300
1290 CONTINUE
FSLT=67.2
CONTINUE
IF (TRIP5.EG.5.) GO TO 1370
CALL FRTCHMS ('CLRSCRN 6')
WRITE (8,2250) PSHP
*****
** START OF DISPLAY SPECIFIC PORTION OF THE PROGRAM
*****
CALL HPROT ('AUTO')
CALL HWSCL ('SCREEN')
CALL PAGE ('11.8.5')
CALL NCBDR (9.,6.)
CALL AREA2D
CALL SWISSL
CALL THKCRV (.02)
CALL CRCS (2.5)
CALL SHDCHR (90.,1.,.002,1)
CALL THKFRM (.15)
CALL INTAXS ('NOENDS')
CALL XTICKS (2)
CALL YTICKS (5)
CALL YXANG (0.)
CALL MYLEGN (.,1)
CALL LINES ('INDUCED POWER$', IHP,1)
CALL LINES ('PRCFLE POWER$', IHP,2)
CALL LINES ('PARASITE POWER$', IHP,3)
CALL LINES ('HISPEED EFFECTS$', IHP,4)
CALL LINES ('TOTAL POWER$', IHP,5)
CALL RESET ('HEIGHT')
CALL XNAME ('FORWARD VELOCITY(KNOTS)$', 100)
CALL YNAME ('REQUIRED HORSEPOWER$', 100)
CALL HEADIN ('POWER VS. VELOCITY AT ALTITUDES$',
1 -100,1.5,1)
IF (ENGSEL.NE.1.) GO TO 1310
CALL GRAF (C.,10.,(MAXV+50.),(-500.*FLOAT(NENG)),500.,
1 (1000.*FLOAT(NENG)))
GO TO 1360

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1310 IF (ENGSEL.NE.2.) GO TO 1320
      CALL GRAF (C.,10.,(MAXV+50.),(-1000.*FLCAT(NENG)),500.,
1      (1500.*FLOAT(NENG)))
1320 GO TO 1360
      IF (ENGSEL.NE.3.) GO TO 1330
      CALL GRAF (C.,10.,(MAXV+50.),(-1500.*FLOAT(NENG)),500.,
1      (2500.*FLOAT(NENG)))
1330 GO TO 1360
      IF (ENGSEL.NE.4.) GO TO 1340
      CALL GRAF (C.,10.,(MAXV+50.),(-1500.*FLCAT(NENG)),500.,
1      (2500.*FLOAT(NENG)))
1340 GO TO 1360
      IF (ENGSEL.NE.5.) GO TO 1350
      CALL GRAF (C.,10.,(MAXV+50.),(-1500.*FLOAT(NENG)),500.,
1      (3500.*FLOAT(NENG)))
1350 GO TO 1360
      CONTINUE
      CALL GRAF (C.,10.,(MAXV+50.),(-1500.*FLCAT(NENG)),
1      500.,(4500.*FLOAT(NENG)))
1360 CONTINUE
      CALL POLY3
      CALL DCT
      CALL LEGLIN (KNOTS,PIY,N,0)
      CALL CURVE (.DOT.)
      CALL RESET
      CALL DASH
      CALL LEGLIN (KNOTS,POY,N,0)
      CALL CURVE (.DASH.)
      CALL RESET
      CALL CHACOT
      CALL LEGLIN (KNOTS,PPY,N,0)
      CALL CURVE (.CHNDOT.)
      CALL RESET
      CALL CHNDOSH
      CALL LEGLIN (KNOTS,PCMPA,N,0)
      CALL CURVE (.CHND$H.)
      CALL RESET
      CALL LEGLIN (KNOTS,PTY,N,0)
      CALL CURVE (IHP,5,3,7,4,25)
      CALL LEGEND (.X--PSHP$,100,0.,-PSHP)
      CALL RLMESS (.X-MAX SHP$,100,0.,SHPMM(ENGSEL))
      CALL RLMESS (.X-CRUISE$,100,VCR,0.)
      CALL RLMESS (3,5,4,15,2,1.55,1.)
      CALL BLESET (.THKCRV.)
      CALL DCT
      CALL RESET
      CALL GRID (2,1)
      CALL RESET (.DOT.)

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CALL ENDFL (0)
** END OF DISSPLA SPECIFIC PORTION OF THE PROGRAM
**
WRITE (6,2310) PSHP
WRITE (8,1410) PSHP
GO TO 1380
CONTINUE
1370 WRITE (6,2770)
CONTINUE
1380
7.5 DETERMINE THE MAXIMUM RANGE VELOCITY
**
WRITE (6,2320)
READ (5,*) VMAXR
CALL FRICMS (,CLRSCRN 6)
WRITE (6,2760)
READ (5,*) VELMAX
CALL FRICMS (,CLRSCRN 6)
7.6 DETERMINE THE MAXIMUM ENDURANCE VELOCITY
**
WRITE (6,2330)
READ (5,*) VMAXE
CALL FRICMS (,CLRSCRN 6)
WRITE (6,2340)
READ (5,*) RSHPM
RSHRME=FSHP+RSHPM
WFME=RSHRME*BETA
CALL FRICMS (,CLRSCRN 6)
7.7 DETERMINE THE POWER REQUIRED AND FUEL FLOW RATE AT
SPECIFICATION CRUISE VELOCITY
**
WRITE (6,2350)
READ (5,*) FSHPC
RSHPRC=PSHP+RSHPC
WFCCR=RSHPRC*BETA
CALL FRICMS (,CLRSCRN 6)
IF (TRINCE
CONTINUE
1390
7.8 DETERMINE THE TOTAL FUEL REQUIREMENTS
**
FW=(.05*WFN)*2.+(WFCCR*RNNGMAX/VCR)*.25*WFME
GALOUT=FW/6.5
WRITE (6,2360) FW

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1450

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CONTINUE
PAVAIL=(SHPPM(ENGSEL)-10.)/(0.1*FLOAT(NENG-1)+1.03)
WRITE (6,2460)
READ (5,*) VVERT
RCLIMB=VVERT
CALL FRTCMS (0,CLRSCRN 60)
VVERT=VVERT/60
VFW=VMAXE*1.151*5280./3600.
VNEW=SQRT(CWG/(2.*RHOSL*AREAMR))
EFPVAF=2.*EFPAFF
VITNEW(1)=1.
VITNEW(2)=2.*VVERT
VITNEW(3)=VFW**2+VVERT**2
VITNEW(4)=0.
VITNEW(5)=-VNEW**4
NDEG=4
CALL ZPCLR (VITNEW,NDEG,ZCMPLX,IER)
VTNEW=ZCMPLX(3)
PC=DWG*VVERT
PC=PC/550.
MU=VFW/VIF
MUTR=VFW/VITPTR
PPC=(0.5*RHOSL*EFPV*VVERT**3)+(0.5*RHOSL*EFPAFF*VFW**3)
POC=PC/550.
POC=0.125*RHOSL*CDO*SIGMA*AREAMR*VTIP**3*(1.+4.3*HU**2)
POC=PC/550.
PIVERT=(1./8)*DWG*VTNEW
PIVERT=PIVERT/550.
PIVERT=PIVERT+PC+PPC
POTR=.125*SIGTR*CDCTR*RHOSL*AREATR*(VTIPTR**3)
POTRF=(1.+4.3*MUTR**2)*POTR
POTRF=PCTRF/550.
PPF=5*RHOSL*(VFW**3)*EFPAFF
PPF=PPF/550.
PO=.125*SIGMA*CDO*RHOSL*AREAMR*(VTIP**3)
POF=(1.+4.3*MU**2)*PO
POF=POF/550.
VI=SQRT(DWG/(2.*RHOSL*AREAMR))
VIT=V*SQRT((VFW**2/(2.*VI**2))**2)+1.)
1 PIITLF=(1./8)*DWG*VIT
PIITLF=PIITLF/550.
PIITLF=PIITLF+PPF
TTR=(TTR/(AREAMR*(VTIPTR**2)*RHOSL)
BTTR=1.-SQRT(2.*CTTR)/FLOAT(BLATR)
VITR=SQRT(TTR/(2.*RHOSL*AREATR))
VITR=VITR*SQRT((-VFW**2/(2.*VITR**2)))

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1  +SQR T((V FWD**2/(2.*V ITR**2)**2)+1.))
P I T L T F=(1./E)*T I T R*V I T R
P I T L T F=P I T L T F/550.
P T T R F=P I T L T F+P O T R F
P T A V A L=P T T R F+P T V E R T
W R I T E(6,2470) P A V A I L,P T A V A L,P I V E R T
R E A D(5,*) A N S
C A L L F R I C M S(1,C L R S C R N 6')
I F (A N S.EQ.1.) G O T O 1450
V V E R T=V V E R T+60.
W R I T E(6,2480) R C L I M B
W R I T E(8,2480) R C L I M B
C**8.3 C O M P U T E M A X I M U M H O V E R A L T I T U D E, I G E
C**C O N T I N U E
C**1460
R E A D(5,2501) A L T
C A L L F R I C M S(1,C L R S C R N 6')
D E L T A=P A L T/2116.22
T A L T=518.688*(1.-C O N S T*A L T)
T H E T A=T A L T/518.688
C A L L F R I C M S(1,C L R S C R N 6')
R H O M H=0.023769*(1.-C O N S T*A L T)**4.2561
C T H=D W G/(A R E A M R*K H O M H*V T I P**2)
B H=1.-S Q R T(2.*C T H)/F L O A T(B L A D E S)
P I T L H=(1./B F)*(D W G**1.5/S Q R T(2.*R H O M H*A R E A M R))
P P O G E H=-1.276*(H/D)**4+.708*(H/D)**3-1.4569*(H/D)**2+1.3432*(H/D)+
1.5147
P O H=1.25*S I G M A*C D O*R H O M H*A R E A M R*V T I P**3
P T H=P I T L H+P C H
T I T R=P T H/(O M E G A*L T R)
V T I P T R=C M E G T R*L T R
C T I T R=T I T R/(A R E A T R*R H O M H*V T I P T R**2)
B T I T R=1.-S Q R T(2.*C T I T R)/F L O A T(B L A D T R)
P I T L T R=(1./E T R)*(T I T R**1.5/S Q R T(2.*R H O M H*A R E A T R))
P O T T R=1.25*S I G T R*C D O T R*R H O M H*A R E A T R*(V T I P T R**3)
P T T R H=F I T L T F+P O T R
P T A C H=P T A C H+P T I T R H
P T A C H=P T A C H/550.
P A V A I L=((S H F M M(E N G S E L)-10.)/(1.*F L O A T(N E N G-1)+1.03))*D E L T A/S Q R T(T H
1 E T A)
W R I T E(6,2450) P A V A I L,P T A C H
R E A D(5,*) A N S
C A L L F R I C M S(1,C L R S C R N 6')
I F (A N S.EQ.1.) G O T O 1460
W R I T E(6,2530) A L T

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PI TLF=FITLF/550.
PTTF=PI TLF+PCF+PPF
TTR=((PTTF*550.)/(OMEGA*LTR))
CTTR=TTR/(AREA*TR*((VTI*PTR**2)*RHOSC)
BTTR=1.-SQRT(2.*CTTR)/FLOAT(BLADTR)
VI TTR=SQRT(TTR/((2.*RHOSC**AREATR)))
VI TTR=VI TTR*SQRT((- (VFWDD**2/(2.*VITR**2))**2)+1.))

1 PI TLF=(1./PI)*TTR*VITR
PI TLF=PI TLF/550.
PTTRF=PI TLF+POTRF
PTAVAL=PTTRF+PTVERT
WRITE (6,2540) PAVAIL,PTAVAL
READ (5,*) ANS
CALL FRTCMS (,CLRSCRN 6)
IF (ANS.EQ.1.) GO TO 1470
WRITE (6,2520) ALTSC
WRITE (8,2520) ALTSC
C*****9.1 MAKE FINAL CHECK FOR SPECIFICATION COMPLIANCE*****
C*****
C*****
1 MAXR, MAXV, VELMAX, VMAXE, VMAXR, RBS, RCLIMB, NENG, V
1 WRITE MAXV, VELMAX, VMAXE, VMAXR, RBS, RCLIMB, NENG, V
1 MAXR, MAXV, VELMAX, VMAXE, VMAXR, RBS, RCLIMB, NENG, V
IF (ENGSEL.NE.1.) GO TO 1480
WRITE (6,2560)
WRITE (8,2560)
GO TO 1530
1480 IF (ENGSEL.NE.2.) GO TO 1490
WRITE (6,2570)
WRITE (8,2570)
GO TO 1530
1490 IF (ENGSEL.NE.3.) GO TO 1500
WRITE (6,2580)
WRITE (8,2580)
GO TO 1530
1500 IF (ENGSEL.NE.4.) GO TO 1510
WRITE (6,2590)
WRITE (8,2590)
GO TO 1530
1510 IF (ENGSEL.NE.5.) GO TO 1520
WRITE (6,2600)
WRITE (8,2600)
GO TO 1530
1520 CONTINUE
WRITE (6,2610)
WRITE (8,2610)

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1590 FORMAT (55H ENTER THE GROSS WEIGHT THAT YOU WANT FOR THE FIRST 80%
1600 19H ESTIMATE), WEIGHT ESTIMATE =,F8.2)
1610 FORMAT (30H ENTER THE VALUE OF THE DISC LOADING FOR THE ESTIMATED,
1620 17H GROSS WEIGHT OF, F9.2, 4H LBS)
1630 11) FORMAT (28H THE ADVANCE RATIO (MU) IS =,F6.4, /)
1640 12) FORMAT (52H ENTER THE BLADE LOADING FOR THE GIVEN ADVANCE RATIO)
1650 13) FORMAT (52H ENTER THE NUMBER OF MAIN ROTOR BLADES THAT YOU WANT)
1660 14) FORMAT (30H1GROSS WEIGHT (LBS) =,F10.2, /, 30H EMPTY WEIGHT
1670 15) (LBS) =,F10.2, /, 30H SONIC SPEED (FPS) =,F10.2, /, 30H DISK LOADING
1680 16) MAXIMUM TIP VELOCITY (FPS) =,F10.2, /, 30H TIP VELOCITY (FPS) =,F10.2, /, 30H
1690 17) ROTATIONAL VELOCITY (RPS) =,F10.2, /, 30H TIP VELOCITY (FPS) =,F10.2, /, 30H
1700 18) ADVANCE RATIO (MU) =,F12.4, /, 30H BLADE LOADING =,F15.7, /, 30H NUMBER OF MA
1710 19) IN ROTOR BLADES =, 5X, 12, /, 30H CHORD MAIN ROTOR BLADE (FT) =,F14.6)
1720 20) THE ROTATIONAL SPEED IS =,F11.3)
1730 21) WHAT IS THE COEFFICIENT OF LIFT WITH RESPECT TO ALPHA?
1740 22) WHAT IS THE ZERO LIFT COEFFICIENT OF DRAG?
1750 23) GROSS WEIGHT (LBS) =,F10.2, /, 30H EMPTY WEIGHT =,F10.2, /, 30H
1760 24) MAXIMUM TIP VELOCITY (FPS) =,F10.2, /, 30H DISK LOADING (LBS) =,F10.2, /, 30H
1770 25) ROTATIONAL VELOCITY (RPS) =,F10.2, /, 30H TIP VELOCITY (FPS) =,F10.2, /, 30H
1780 26) ADVANCE RATIO (MU) =,F12.4, /, 30H BLADE LOADING =,F15.7, /, 30H NUMBER OF MA
1790 27) IN ROTOR BLADES =, 5X, 12, /, 30H CHORD MAIN ROTOR BLADE (FT) =,F14.6)
1800 28) THE ASPECT RATIO IS =,F11.3)
1810 29) WHAT IS THE COEFFICIENT OF LIFT W/R ALPHA =,F12.4, /, 30H
1820 30) COEFF OF DRAG =,F12.4)
1830 31) ENTER THE AMOUNT OF FUEL IN POUNDS)
1840 32) ENTER THE USEFUL LOAD IN POUNDS THAT YOU WANT)
1850 33) ENTER THE NUMBER OF PEOPLE YOU ARE PLANNING ON)
1860 34) ENTER THE NUMBER OF ENGINES YOU WANT)
1870 35) TIP LOSS FACTOR =,F16.7, /, 30H POWER (HP) =,F10.1, /, 30H POWER (INDUC
1880 36) PCWR (TOTAL) (HP) =,F10.1, /, 30H FUEL WEIGHT (LBS) =,F11.2, /, 30H
1890 37) FUEL WEIGHT (LBS) =,F11.2, /, 30H USEFUL LOAD (LBS) =,F11.2, /, 30H
1900 38) NUMBER OF PEOPLE =, 6X, 12, /, 30H USEFUL LOAD (LBS) =,F11.2, /, 30H ESTIMA
1910 39) GROSS WEIGHT (LBS) =,F11.2, /, 30H SOLIDITY =,

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1770 7F16.7,/,30H ROTOR RADIUS (FT) =,F12.3,/,30H HOVER POWER
      8(HP) =,F10.1,/,30H ROTOR WEIGHT (LBS) =,F11.2,/,30H STRUCTURE (L
      9/,30H TAIL: ROTCR (LBS) =,F11.2,/,30H
      $B$) =,F11.2,/,30H BODY (LBS) =,F11.2,/,30H
      $LANDING GEAR (LBS) =,F11.2,/,30H
      $FORMAT (30H) NACELLE (LBS) =,F11.2,/,30H PROPULSION:
      1ENGINE (LBS) =,F11.2,/,30H DRIVE (LBS) =,F11.2,/,30H
      2/,30H FUEL TANKS (LBS) =,F11.2,/,30H FLIGHT CONTROLS (L
      3$S) =,F11.2,/,30H AUXILIARY POWER (LBS) =,F11.2,/,30H
      4INSTRUMENTS (LBS) =,F11.2,/,30H HYDRAULICS (LBS)
      5 =,F11.2,/,30H ELECTRICAL (LBS) =,F11.2,/,30H AVIONIC
      6CS (LBS) =,F11.2,/,30H FURNISHINGS (LBS) =,F11.2,/,30H LOAD AND HAN
      7F11.2,/,30H AIR AND ICE (LBS) =,F11.2,/,30H REVISED EMPTY WEIGHT (LBS) =,F11.
      8DOLLING (LBS) =,F11.2,/,30H REVISED EMPTY WEIGHT (LBS) =,F11.2,/,30H
      92/,30H REVISED GROSS WEIGHT (LBS) =,F11.2,/,30H CHANGE ,23H THE ROTATIONAL VELOC
      $FORMAT (//46H) LOOK AT YOUR FIGURE OF MERIT (2) =,F7.3,/,30H
      1780 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,5
      1790 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1800 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1810 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1820 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1830 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1840 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1850 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1860 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1870 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1880 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1890 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1900 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1910 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1920 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20
      1930 $FORMAT (//46H) RECALCULATE THE ROTOR RADIUS WITH THE NEW DL,/,10X,20

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2210 (23H RELIABILITY(ENG): ,6F8.4)
2220 (23H MAINTAINABILITY(ENG): ,6F8.3)
2230 (23H PERFORMANCE(SHP-MIL): ,6F8.1)
2240 (49H SELECT: (1.A)---(2.8)---(4.D)---(5.E)---(6.F))
2250 (//51H)-----FUEL FLOW RATES-----,/
2260 (//51H) POWER NORMAL POWER =,F8.2)
2270 (3X,F10.2,7X,F10.2,///,///)
2280 (30H) F10.2,7X,F10.2,///,///)
2290 (30H) F10.2,7X,F10.2,///,///)
2300 (30H) F10.2,7X,F10.2,///,///)
2310 (30H) F10.2,7X,F10.2,///,///)
2320 (30H) F10.2,7X,F10.2,///,///)
2330 (30H) F10.2,7X,F10.2,///,///)
2340 (30H) F10.2,7X,F10.2,///,///)
2350 (30H) F10.2,7X,F10.2,///,///)
2360 (30H) F10.2,7X,F10.2,///,///)
2370 (30H) F10.2,7X,F10.2,///,///)
2380 (30H) F10.2,7X,F10.2,///,///)
2390 (30H) F10.2,7X,F10.2,///,///)
2400 (30H) F10.2,7X,F10.2,///,///)
2410 (30H) F10.2,7X,F10.2,///,///)
2420 (30H) F10.2,7X,F10.2,///,///)
2430 (30H) F10.2,7X,F10.2,///,///)
2440 (30H) F10.2,7X,F10.2,///,///)
2450 (30H) F10.2,7X,F10.2,///,///)
2460 (30H) F10.2,7X,F10.2,///,///)
2470 (30H) F10.2,7X,F10.2,///,///)
2480 (30H) F10.2,7X,F10.2,///,///)
2490 (30H) F10.2,7X,F10.2,///,///)

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3.....20X,F10.2,/,41H FUSELAGE LENGTH (FT),.....FORMA
4.....F10.2,10X,F10.2,/,41H EQUIVALENT FLAT PLAGE AREA (FT),FORMA
5RD 20X,F10.2,/,41H
610.2)
2640 FORMAT (50H ENTER THE SPECIFICATION PRESSURE ALTITUDE IN FEET)
2650 FORMAT (43H ENTER THE SPECIFICATION TEMPERATURE IN (F))
2660 FORMAT (53H FROM THE SPECIFICATIONS SHEET, WHAT IS THE NUMBER OF,6
1H CREW?)
2670 FORMAT (51H FROM THE SPECIFICATIONS SHEET, WHAT IS THE SERVICE,9H
1CEILING?)
2680 FORMAT (55H FROM THE SPECIFICATIONS SHEET, WHAT IS THE HOVER (IGE)
19HCEILING?)
2690 FORMAT (51H FROM THE SPECIFICATIONS SHEET, WHAT IS THE MAXIMUM,14H
1FOROTOR RADIALS?)
2700 FORMAT (51H FROM THE SPECIFICATIONS SHEET, WHAT IS THE MAXIMUM,17H
1FUSELAGE LENGTH?)
2710 FORMAT (47H ENTER TYPE OF HELICOPTER FOR WEIGHT ESTIMATION,/,15X,8
1H1. LIGHT,/,15X,9H2. MEDIUM,/,15X,8H3. HEAVY)
2720 FORMAT (52H ENTER THE MAXIMUM RATE OF CLIMB FROM SPECIFICATIONS)
2730 FORMAT (40H WHICH TYPE HELICOPTER ARE YOU DESIGNING,/,10X,7H1. LIGH
1T,/,10X,8H2. MEDIUM,/,10X,7H3. HEAVY)
2740 FORMAT (49H YOU HAVE NOT CONVERGED TO WITH 10% OF THE WEIGHT,/,29H
1THEREFORE YOU MUST REITERATE)
2750 FORMAT (36H ENTER THE SPECIFICATION USEFUL LOAD)
2760 FORMAT (44H ENTER THE MAXIMUM POSSIBLE FORWARD VELOCITY)
2770 FORMAT (36H HERE IS THE TOTAL POWER VS. FORWARD,16H VELOCITY TABLE
1,/,16H NOW GRAPH A FEW,39H POINTS AND EXTRAPOLATE THE NEEDED DATA
2)
2780 FORMAT (35H ENTER TYPE OF LANDING GEAR DESIRED,/,10X,10H1. WHEEL
1S,/,10X,9H2. SKIDS)
2790 FORMAT (32H WHAT TYPE OF GEAR DO YOU DESIRE,/,10X,9H1. FIXED,/,1
10X,15H2. RETRACTABLE)
2800 FORMAT (33H ENTER THE NUMBER OF LANDING GEAR)
2810 FORMAT (55H ICOST ANALYSIS PER VEHICLE (IN DOLLARS FOR 100 A/C RUN)
1,/,5X,3CH RCTOR =,F11.2,/,5X,30H
2
31.2,/,5X,30H BODY =,F11.2,/,5X,30H LANDING =
4GEAR
5,F11.2,/,5X,30H PROPULSION: ENGINE =,F11.2,/,5X,30H
6DRIVE =,F11.2,/,5X,30H FUEL TANKS
7 =,F11.2,/,5X,30H FLIGHT CONTROLS =,F11.2,/,5X,30H AU
8XILIARY POWER =,F11.2,/,5X,30H INSTRUMENTS =,F11.2,/,5X,30H
9 =,F11.2,/,5X,30H HYDRAULICS =,F11.2,/,5X,30H
$ ELECTRICAL =,F11.2,/,5X,30H AVIONICS =,F11.2,/,5X,
$ =,F11.2,/,5X,30H FURNISHINGS =,F11.2,/,5X,
$30H AIR AND ICE =,F11.2,/,5X,30H LOAD AND HANDLING
$ =,F11.2)
2820 FORMAT (33H ENTER THE INFLATION RATE DOLLARS)

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2940 11H ZERC ANGLE OF ATTACK)
      FORMAT (51H ENTER THE VALUE OF THE MAXIMUM COEFFICIENT OF LIFT,/,2
16H FOR YOUR SELECTED AIRFOIL)
2950 16H FOR YOUR SELECTED AIRFOIL)
      FORMAT (53H ENTER THE VALUE OF THE VELOCITY WHERE THE RETREATING, /
1,42H BLADE STALL ANGLE IS NEAREST 12.5 DEGREES)
2960 1,42H BLADE STALL ANGLE IS NEAREST 12.5 DEGREES)
      FORMAT (///42H ENTER THE SPAN OF THE VERTICAL STABILIZER)
2970 1,42H BLADE STALL ANGLE IS NEAREST 12.5 DEGREES)
      FORMAT (29H THE TAIL ROTOR SOLIDITY IS ,F9.7,/,35H ENTER THE VER
1TICAL STABILIZER AREA)
2980 1TICAL STABILIZER AREA)
      FORMAT (///36H VERTICAL STABILIZER DATA ,/,40X,23H 8
10 KNOTS ,160 KNOTS ,/,37H SECTION COEFFICIENT OF LIFT ,5X,
2F8.5,5X,F8.5,/,37H ANGLE OF ATTACK TO UNLOAD TAIL ROTOR,6X,F6.3,7X
3,F6.3)
      END

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D. SAMPLE OUTPUT

| | | |
|-----------------------------|-----------|--------|
| GROSS WEIGHT (LBS) | 14400.00 | |
| EMPTY WEIGHT (LBS) | 4320.00 | |
| SONIC SPEED (FPS) | 1116.89 | |
| MAXIMUM TIP VELOCITY (FPS) | 725.98 | |
| DISK LOADING (FT) | 7.10 | |
| ROTOR RADIUS (FT) | 25.41 | |
| ROTATIONAL VELOCITY (RPS) | 28.57 | |
| TIP VELOCITY (FPS) | 725.98 | |
| COEFFICIENT OF THRUST | 0.005668 | |
| ADVANCE RATIO | 0.3721 | |
| BLADE LOAD | 0.0960 | |
| SOLIDITY | 0.0590377 | |
| NUMBER OF MAIN ROTOR BLADES | 4 | |
| CHORD MAIN ROTOR BLADE (FT) | 1.178138 | 21.567 |
| THE ASPECT RATIO IS | = | 28.572 |
| THE ROTATIONAL SPEED IS | = | |

| | | |
|-----------------------------|-----------|--|
| GROSS WEIGHT (LBS) | 14400.00 | |
| EMPTY WEIGHT (LBS) | 4320.00 | |
| SONIC SPEED (FPS) | 1116.89 | |
| MAXIMUM TIP VELOCITY (FPS) | 725.98 | |
| DISK LOADING (FT) | 7.10 | |
| ROTOR RADIUS (FT) | 25.41 | |
| ROTATIONAL VELOCITY (RPS) | 27.00 | |
| TIP VELOCITY (FPS) | 686.03 | |
| COEFFICIENT OF THRUST | 0.006347 | |
| ADVANCE RATIO | 0.3937 | |
| BLADE LOAD | 0.0920 | |
| SOLIDITY | 0.0689887 | |
| NUMBER OF MAIN ROTOR BLADES | 4 | |
| CHORD MAIN ROTOR BLADE (FT) | 1.377 | |
| ASPECT RATIO OF MAIN ROTOR | 18.46 | |
| COEFF OF LIFT (AVG) | 0.5520 | |
| COEFF OF LIFT W/ R ALPHA | 6.3025 | |
| COEFF OF DRAG @ 0 LIFT | 0.0100 | |

| MAIN ROTOR PROFILE | | POWER PROFILE | | PARASITE | | TOTAL | |
|----------------------|-------------|------------------|-------------------------|-------------------|-------------------|----------------|----------------|
| AIR SPEED (KNOTS) | TIP MACH | INDUCED (SHP) | POWER @ SSL (SHP) | PARASITE (SHP) | PARASITE (SHP) | TOTAL (SHP) | TOTAL (SHP) |
| 0.00 | 0.65 | 1335.01 | 353.65 | 0.04 | 0.04 | 1688.66 | 66 |
| 5.00 | 0.66 | 1320.66 | 353.87 | 0.30 | 0.30 | 1674.35 | 55 |
| 10.00 | 0.67 | 1278.58 | 355.50 | 1.03 | 1.03 | 1633.49 | 35 |
| 15.00 | 0.67 | 1211.97 | 355.54 | 2.44 | 2.44 | 1568.42 | 92 |
| 20.00 | 0.68 | 1126.64 | 356.34 | 4.76 | 4.76 | 1486.36 | 02 |
| 25.00 | 0.69 | 1033.82 | 358.78 | 8.23 | 8.23 | 1394.36 | 87 |
| 30.00 | 0.70 | 933.55 | 361.05 | 13.06 | 13.06 | 1302.37 | 63 |
| 35.00 | 0.70 | 841.53 | 363.80 | 19.50 | 19.50 | 1218.30 | 80 |
| 40.00 | 0.71 | 759.37 | 366.30 | 27.08 | 27.08 | 1145.80 | 53 |
| 45.00 | 0.72 | 687.24 | 370.20 | 38.69 | 38.69 | 1085.53 | 80 |
| 50.00 | 0.73 | 622.63 | 378.52 | 50.81 | 50.81 | 1038.80 | 44 |
| 55.00 | 0.74 | 565.38 | 383.39 | 63.67 | 63.67 | 997.41 | 88 |
| 60.00 | 0.75 | 515.36 | 393.90 | 84.50 | 84.50 | 953.20 | 89 |
| 65.00 | 0.76 | 472.57 | 406.27 | 104.53 | 104.53 | 911.60 | 60 |
| 70.00 | 0.76 | 435.47 | 423.05 | 128.99 | 128.99 | 876.11 | 70 |
| 75.00 | 0.77 | 402.99 | 437.87 | 155.11 | 155.11 | 843.20 | 89 |
| 80.00 | 0.78 | 375.64 | 454.30 | 187.10 | 187.10 | 812.60 | 117 |
| 85.00 | 0.79 | 353.20 | 472.28 | 222.27 | 222.27 | 798.11 | 70 |
| 90.00 | 0.81 | 332.05 | 492.58 | 261.69 | 261.69 | 786.20 | 28 |
| 95.00 | 0.82 | 312.48 | 514.39 | 302.52 | 302.52 | 770.13 | 13 |
| 100.00 | 0.82 | 294.86 | 539.05 | 345.37 | 345.37 | 750.61 | 80 |
| 105.00 | 0.83 | 279.67 | 566.12 | 390.06 | 390.06 | 733.80 | 74 |
| 110.00 | 0.83 | 266.67 | 595.50 | 436.36 | 436.36 | 719.98 | 66 |
| 115.00 | 0.84 | 255.46 | 627.61 | 484.60 | 484.60 | 708.76 | 98 |
| 120.00 | 0.85 | 245.67 | 661.50 | 534.02 | 534.02 | 699.65 | 77 |
| 125.00 | 0.85 | 237.91 | 697.19 | 584.55 | 584.55 | 692.73 | 61 |
| 130.00 | 0.86 | 231.04 | 734.58 | 636.26 | 636.26 | 687.61 | 19 |
| 135.00 | 0.87 | 225.00 | 772.81 | 689.93 | 689.93 | 683.71 | 55 |
| 140.00 | 0.88 | 219.77 | 811.94 | 744.62 | 744.62 | 680.84 | 11 |
| 145.00 | 0.89 | 215.33 | 851.95 | 799.84 | 799.84 | 678.75 | 19 |
| 150.00 | 0.90 | 211.68 | 893.88 | 855.66 | 855.66 | 677.37 | 11 |
| 155.00 | 0.91 | 208.73 | 937.74 | 912.09 | 912.09 | 676.91 | 11 |
| 160.00 | 0.92 | 206.48 | 983.55 | 968.84 | 968.84 | 676.75 | 11 |
| 165.00 | 0.93 | 204.83 | 1031.28 | 1025.93 | 1025.93 | 676.75 | 11 |
| 170.00 | 0.94 | 203.73 | 1080.94 | 1083.48 | 1083.48 | 676.75 | 11 |
| 175.00 | 0.95 | 203.13 | 1132.46 | 1141.36 | 1141.36 | 676.75 | 11 |
| 180.00 | 0.96 | 203.00 | 1185.80 | 1199.69 | 1199.69 | 676.75 | 11 |
| 185.00 | 0.97 | 203.34 | 1240.94 | 1258.06 | 1258.06 | 676.75 | 11 |
| 190.00 | 0.98 | 204.11 | 1297.88 | 1316.48 | 1316.48 | 676.75 | 11 |
| 195.00 | 0.99 | 205.29 | 1356.61 | 1374.93 | 1374.93 | 676.75 | 11 |
| 200.00 | 1.00 | 206.87 | 1417.14 | 1433.41 | 1433.41 | 676.75 | 11 |
| 205.00 | 1.01 | 208.83 | 1479.45 | 1491.93 | 1491.93 | 676.75 | 11 |
| 210.00 | 1.02 | 211.16 | 1543.56 | 1550.46 | 1550.46 | 676.75 | 11 |
| 215.00 | 1.03 | 213.85 | 1609.48 | 1608.99 | 1608.99 | 676.75 | 11 |
| 220.00 | 1.04 | 216.88 | 1677.21 | 1667.52 | 1667.52 | 676.75 | 11 |
| 225.00 | 1.05 | 220.24 | 1746.75 | 1726.05 | 1726.05 | 676.75 | 11 |
| 230.00 | 1.06 | 223.93 | 1818.08 | 1784.58 | 1784.58 | 676.75 | 11 |
| 235.00 | 1.07 | 227.94 | 1891.19 | 1843.11 | 1843.11 | 676.75 | 11 |
| 240.00 | 1.08 | 232.26 | 1966.08 | 1901.64 | 1901.64 | 676.75 | 11 |
| 245.00 | 1.09 | 236.88 | 2042.74 | 1960.17 | 1960.17 | 676.75 | 11 |
| 250.00 | 1.10 | 241.79 | 2121.16 | 2018.70 | 2018.70 | 676.75 | 11 |
| 255.00 | 1.11 | 246.98 | 2201.34 | 2077.23 | 2077.23 | 676.75 | 11 |
| 260.00 | 1.12 | 252.44 | 2283.27 | 2135.76 | 2135.76 | 676.75 | 11 |
| 265.00 | 1.13 | 258.15 | 2366.94 | 2194.29 | 2194.29 | 676.75 | 11 |
| 270.00 | 1.14 | 264.10 | 2452.34 | 2252.82 | 2252.82 | 676.75 | 11 |
| 275.00 | 1.15 | 270.28 | 2539.46 | 2311.35 | 2311.35 | 676.75 | 11 |
| 280.00 | 1.16 | 276.68 | 2628.29 | 2369.88 | 2369.88 | 676.75 | 11 |
| 285.00 | 1.17 | 283.29 | 2718.82 | 2428.41 | 2428.41 | 676.75 | 11 |
| 290.00 | 1.18 | 289.99 | 2810.94 | 2486.94 | 2486.94 | 676.75 | 11 |
| 295.00 | 1.19 | 296.78 | 2904.64 | 2545.47 | 2545.47 | 676.75 | 11 |
| 300.00 | 1.20 | 303.64 | 2999.91 | 2603.99 | 2603.99 | 676.75 | 11 |
| 305.00 | 1.21 | 310.57 | 3096.74 | 2662.52 | 2662.52 | 676.75 | 11 |
| 310.00 | 1.22 | 317.65 | 3195.13 | 2721.05 | 2721.05 | 676.75 | 11 |
| 315.00 | 1.23 | 324.87 | 3295.06 | 2779.58 | 2779.58 | 676.75 | 11 |
| 320.00 | 1.24 | 332.22 | 3396.52 | 2838.11 | 2838.11 | 676.75 | 11 |
| 325.00 | 1.25 | 339.69 | 3499.51 | 2896.64 | 2896.64 | 676.75 | 11 |
| 330.00 | 1.26 | 347.27 | 3603.99 | 2955.17 | 2955.17 | 676.75 | 11 |
| 335.00 | 1.27 | 354.95 | 3709.94 | 3013.70 | 3013.70 | 676.75 | 11 |
| 340.00 | 1.28 | 362.72 | 3817.34 | 3072.23 | 3072.23 | 676.75 | 11 |
| 345.00 | 1.29 | 370.57 | 3926.17 | 3130.76 | 3130.76 | 676.75 | 11 |
| 350.00 | 1.30 | 378.49 | 4036.41 | 3189.29 | 3189.29 | 676.75 | 11 |
| 355.00 | 1.31 | 386.47 | 4148.04 | 3247.82 | 3247.82 | 676.75 | 11 |
| 360.00 | 1.32 | 394.50 | 4261.04 | 3306.35 | 3306.35 | 676.75 | 11 |
| 365.00 | 1.33 | 402.57 | 4375.41 | 3364.88 | 3364.88 | 676.75 | 11 |
| 370.00 | 1.34 | 410.67 | 4491.14 | 3423.41 | 3423.41 | 676.75 | 11 |
| 375.00 | 1.35 | 418.79 | 4608.22 | 3481.94 | 3481.94 | 676.75 | 11 |
| 380.00 | 1.36 | 426.92 | 4726.64 | 3540.47 | 3540.47 | 676.75 | 11 |
| 385.00 | 1.37 | 435.06 | 4846.39 | 3598.99 | 3598.99 | 676.75 | 11 |
| 390.00 | 1.38 | 443.20 | 4967.46 | 3657.52 | 3657.52 | 676.75 | 11 |
| 395.00 | 1.39 | 451.33 | 5089.84 | 3716.05 | 3716.05 | 676.75 | 11 |
| 400.00 | 1.40 | 459.44 | 5213.51 | 3774.58 | 3774.58 | 676.75 | 11 |
| 405.00 | 1.41 | 467.53 | 5338.46 | 3833.11 | 3833.11 | 676.75 | 11 |
| 410.00 | 1.42 | 475.59 | 5464.67 | 3891.64 | 3891.64 | 676.75 | 11 |
| 415.00 | 1.43 | 483.62 | 5592.12 | 3950.17 | 3950.17 | 676.75 | 11 |
| 420.00 | 1.44 | 491.62 | 5720.79 | 4008.70 | 4008.70 | 676.75 | 11 |
| 425.00 | 1.45 | 500.00 | 5850.66 | 4067.23 | 4067.23 | 676.75 | 11 |
| 430.00 | 1.46 | 508.37 | 5981.79 | 4125.76 | 4125.76 | 676.75 | 11 |
| 435.00 | 1.47 | 516.72 | 6114.14 | 4184.29 | 4184.29 | 676.75 | 11 |
| 440.00 | 1.48 | 525.04 | 6247.69 | 4242.82 | 4242.82 | 676.75 | 11 |
| 445.00 | 1.49 | 533.33 | 6382.39 | 4301.35 | 4301.35 | 676.75 | 11 |
| 450.00 | 1.50 | 541.58 | 6518.22 | 4359.88 | 4359.88 | 676.75 | 11 |
| 455.00 | 1.51 | 549.79 | 6655.16 | 4418.41 | 4418.41 | 676.75 | 11 |
| 460.00 | 1.52 | 557.95 | 6793.26 | 4476.94 | 4476.94 | 676.75 | 11 |
| 465.00 | 1.53 | 566.06 | 6932.51 | 4535.47 | 4535.47 | 676.75 | 11 |
| 470.00 | 1.54 | 574.11 | 7072.84 | 4593.99 | 4593.99 | 676.75 | 11 |
| 475.00 | 1.55 | 582.11 | 7214.24 | 4652.52 | 4652.52 | 676.75 | 11 |
| 480.00 | 1.56 | 590.05 | 7356.69 | 4711.05 | 4711.05 | 676.75 | 11 |
| 485.00 | 1.57 | 597.93 | 7500.17 | 4769.58 | 4769.58 | 676.75 | 11 |
| 490.00 | 1.58 | 605.75 | 7644.64 | 4828.11 | 4828.11 | 676.75 | 11 |
| 495.00 | 1.59 | 613.50 | 7790.09 | 4886.64 | 4886.64 | 676.75 | 11 |
| 500.00 | 1.60 | 621.19 | 7936.51 | 4945.17 | 4945.17 | 676.75 | 11 |
| 505.00 | 1.61 | 628.81 | 8083.88 | 5003.70 | 5003.70 | 676.75 | 11 |
| 510.00 | 1.62 | 636.37 | 8232.19 | 5062.23 | 5062.23 | 676.75 | 11 |
| 515.00 | 1.63 | 643.87 | 8381.41 | 5120.76 | 5120.76 | 676.75 | 11 |
| 520.00 | 1.64 | 651.30 | 8531.54 | 5179.29 | 5179.29 | 676.75 | 11 |
| 525.00 | 1.65 | 658.66 | 8682.56 | 5237.82 | 5237.82 | 676.75 | 11 |
| 530.00 | 1.66 | 665.95 | 8834.44 | 5296.35 | 5296.35 | 676.75 | 11 |
| 535.00 | 1.67 | 673.17 | 8987.16 | 5354.88 | 5354.88 | 676.75 | 11 |
| 540.00 | 1.68 | 680.31 | 9140.69 | 5413.41 | 5413.41 | 676.75 | 11 |
| 545.00 | 1.69 | 687.37 | 9295.04 | 5471.94 | 5471.94 | 676.75 | 11 |
| 550.00 | 1.70 | 694.35 | 9450.19 | 5530.47 | 5530.47 | 676.75 | 11 |
| 555.00 | 1.71 | 701.25 | 9606.09 | 5588.99 | 5588.99 | 676.75 | 11 |
| 560.00 | 1.72 | 708.06 | 9762.69 | 5647.52 | 5647.52 | 676.75 | 11 |
| 565.00 | 1.73 | 714.78 | 9919.94 | 5706.05 | 5706.05 | 676.75 | 11 |
| 570.00 | 1.74 | 721.41 | 10077.81 | 5764.58 | 5764.58 | 676.75 | 11 |
| 575.00 | 1.75 | 727.95 | 10236.26 | 5823.11 | 5823.11 | 676.75 | 11 |
| 580.00 | 1.76 | 734.40 | 10395.26 | 5881.64 | 5881.64 | 676.75 | 11 |
| 585.00 | 1.77 | 740.76 | 10554.77 | 5940.17 | 5940.17 | 676.75 | 11 |
| 590.00 | 1.78 | 747.03 | 10714.74 | 5998.70 | 5998.70 | 676.75 | 11 |
| 595.00 | 1.79 | 753.21 | 10875.14 | 6057.23 | 6057.23 | 676.75 | 11 |
| 600.00 | 1.80 | 759.30 | 11035.94 | 6115.76 | 6115.76 | 676.75 | 11 |
| 605.00 | 1.81 | 765.30 | 11197.10 | 6174.29 | 6174.29 | 676.75 | 11 |
| 610.00 | 1.82 | 771.21 | 11358.59 | 6232.82 | 6232.82 | 676.75 | 11 |
| 615.00 | 1.83 | 777.03 | 11520.36 | 6291.35 | 6291.35 | 676.75 | 11 |
| 620.00 | 1.84 | 782.76 | 11682.37 | 6349.88 | 6349.88 | 676.75 | 11 |
| 625.00 | 1.85 | 788.40 | 11844.59 | 6408.41 | 6408.41 | 676.75 | 11 |
| 630.00 | 1.86 | 793.95 | 12006.99 | 6466.94 | 6466.94 | 676.75 | 11 |
| 635.00 | 1.87 | 799.40 | 12169.54 | 6525.47 | 6525.47 | 676.75 | 11 |
| 640.00 | 1.88 | 804.76 | 12332.19 | 6583.99 | 6583.99 | 676.75 | 11 |
| 645.00 | 1.89 | 809.99 | 12494.91 | 6642.52 | 6642.52 | 676.75 | 11 |
| 650.00 | 1.90 | 815.11 | 12657.64 | 6701.05 | 6701.05 | 676.75 | 11 |
| 655.00 | 1.91 | 820.13 | 12820.34 | 6759.58 | 6759.58 | 676.75 | 11 |
| 660.00 | 1.92 | 825.05 | 12983.04 | 6818.11 | 6818.11 | 676.75 | 11 |
| 665.00 | 1.93 | 829.87 | 13145.69 | 6876.64 | 6876.64 | 676.75 | 11 |
| 670.00 | 1.94 | 834.59 | 13308.24 | 6935.17 | 6935.17 | 676.75 | 11 |
| 675.00 | 1.95 | 839.21 | 13470.64 | 6993.70 | 6993.70 | 676.75 | 11 |
| 680.00 | 1.96 | 843.72 | 13632.84 | 7052. | | | |

| AT SPECIFICATION | | MAIN ROTOR ALTITUDE | | POWER PROFILE | | PARASITE | | TOTAL | |
|----------------------|-------------|---------------------|----------------|----------------|-------------------|-------------------|----------------|----------------|----------------|
| AIR SPEED (KNOTS) | TIP MACH | INDUCED (SHP) | POWER (SHP) | POWER (SHP) | PARASITE (SHP) | PARASITE (SHP) | TOTAL (SHP) | TOTAL (SHP) | TOTAL (SHP) |
| 0.0 | 0.63 | 1388.74 | 326.81 | 0.0 | 0.0 | 1715.55 | 1715.55 | 1715.55 | |
| 5.0 | 0.64 | 1374.93 | 327.00 | 0.04 | 0.04 | 1701.24 | 1701.24 | 1701.24 | |
| 10.0 | 0.65 | 1334.39 | 327.57 | 0.28 | 0.28 | 1662.40 | 1662.40 | 1662.40 | |
| 15.0 | 0.66 | 1269.92 | 328.85 | 0.25 | 0.25 | 1599.77 | 1599.77 | 1599.77 | |
| 20.0 | 0.67 | 1186.69 | 331.56 | 0.40 | 0.40 | 1518.75 | 1518.75 | 1518.75 | |
| 25.0 | 0.68 | 1091.99 | 333.65 | 0.60 | 0.60 | 1427.95 | 1427.95 | 1427.95 | |
| 30.0 | 0.69 | 900.42 | 336.12 | 0.77 | 0.77 | 1335.45 | 1335.45 | 1335.45 | |
| 35.0 | 0.70 | 815.19 | 338.20 | 0.92 | 0.92 | 1248.65 | 1248.65 | 1248.65 | |
| 40.0 | 0.71 | 745.03 | 342.81 | 1.07 | 1.07 | 1172.18 | 1172.18 | 1172.18 | |
| 45.0 | 0.72 | 675.95 | 345.80 | 1.19 | 1.19 | 1107.93 | 1107.93 | 1107.93 | |
| 50.0 | 0.73 | 618.02 | 349.54 | 1.25 | 1.25 | 1056.60 | 1056.60 | 1056.60 | |
| 55.0 | 0.74 | 570.67 | 354.17 | 1.32 | 1.32 | 1015.58 | 1015.58 | 1015.58 | |
| 60.0 | 0.75 | 528.23 | 358.05 | 1.37 | 1.37 | 985.97 | 985.97 | 985.97 | |
| 65.0 | 0.76 | 492.77 | 364.54 | 1.41 | 1.41 | 964.89 | 964.89 | 964.89 | |
| 70.0 | 0.77 | 460.02 | 371.36 | 1.44 | 1.44 | 952.66 | 952.66 | 952.66 | |
| 75.0 | 0.78 | 430.71 | 381.85 | 1.47 | 1.47 | 948.74 | 948.74 | 948.74 | |
| 80.0 | 0.79 | 404.18 | 395.39 | 1.50 | 1.50 | 951.75 | 951.75 | 951.75 | |
| 85.0 | 0.80 | 384.76 | 402.85 | 1.53 | 1.53 | 961.42 | 961.42 | 961.42 | |
| 90.0 | 0.81 | 364.66 | 410.76 | 1.56 | 1.56 | 978.54 | 978.54 | 978.54 | |
| 95.0 | 0.82 | 346.23 | 418.30 | 1.59 | 1.59 | 1001.02 | 1001.02 | 1001.02 | |
| 100.0 | 0.83 | 331.57 | 423.65 | 1.62 | 1.62 | 1031.85 | 1031.85 | 1031.85 | |
| 105.0 | 0.84 | 315.37 | 428.91 | 1.65 | 1.65 | 1066.85 | 1066.85 | 1066.85 | |
| 110.0 | 0.85 | 301.11 | 435.57 | 1.68 | 1.68 | 1108.22 | 1108.22 | 1108.22 | |
| 115.0 | 0.86 | 287.77 | 442.78 | 1.71 | 1.71 | 1157.94 | 1157.94 | 1157.94 | |
| 120.0 | 0.87 | 277.01 | 450.57 | 1.74 | 1.74 | 1211.81 | 1211.81 | 1211.81 | |
| 125.0 | 0.88 | 267.77 | 458.99 | 1.77 | 1.77 | 1273.40 | 1273.40 | 1273.40 | |
| 130.0 | 0.89 | 259.49 | 467.57 | 1.80 | 1.80 | 1340.15 | 1340.15 | 1340.15 | |
| 135.0 | 0.90 | 253.14 | 476.37 | 1.83 | 1.83 | 1415.31 | 1415.31 | 1415.31 | |
| 140.0 | 0.91 | 247.94 | 485.37 | 1.86 | 1.86 | 1496.35 | 1496.35 | 1496.35 | |
| 145.0 | 0.92 | 243.40 | 494.57 | 1.89 | 1.89 | 1584.35 | 1584.35 | 1584.35 | |
| 150.0 | 0.93 | 239.40 | 503.97 | 1.92 | 1.92 | 1679.32 | 1679.32 | 1679.32 | |
| 155.0 | 0.94 | 235.94 | 513.68 | 1.95 | 1.95 | 1781.64 | 1781.64 | 1781.64 | |
| 160.0 | 0.95 | 232.77 | 523.61 | 1.98 | 1.98 | 1891.90 | 1891.90 | 1891.90 | |
| 165.0 | 0.96 | 229.98 | 533.73 | 2.01 | 2.01 | 2008.96 | 2008.96 | 2008.96 | |
| 170.0 | 0.97 | 227.42 | 544.02 | 2.04 | 2.04 | 2133.90 | 2133.90 | 2133.90 | |
| 175.0 | 0.98 | 225.07 | 554.57 | 2.07 | 2.07 | 2266.96 | 2266.96 | 2266.96 | |
| 180.0 | 0.99 | 222.91 | 565.37 | 2.10 | 2.10 | 2407.95 | 2407.95 | 2407.95 | |
| 185.0 | 1.00 | 220.92 | 576.41 | 2.13 | 2.13 | 2557.20 | 2557.20 | 2557.20 | |
| 190.0 | 1.01 | 219.12 | 587.69 | 2.16 | 2.16 | 2715.05 | 2715.05 | 2715.05 | |

TAIL ROTOR RADIUS (FT)= 5.451
 TAIL ROTOR SPEED (RPS)= 122.201
 TAIL ROTOR CDO = 0.0138000

| TAIL ROTOR POWER PROFILE | | | | |
|--------------------------|-------------|------------------|------------------|----------------|
| AIRSPEED (KNOTS) | TIP MACH | POWER @ SSL | | TOTAL (SHP) |
| | | INDUCED (SHP) | PROFILE (SHP) | |
| 0.0 | 0.60 | 95.87 | 43.67 | 139.54 |
| 5.0 | 0.60 | 93.94 | 43.70 | 137.63 |
| 10.0 | 0.61 | 88.34 | 43.79 | 132.13 |
| 15.0 | 0.62 | 79.67 | 43.94 | 123.61 |
| 20.0 | 0.63 | 68.94 | 44.15 | 113.09 |
| 25.0 | 0.63 | 57.45 | 44.42 | 101.87 |
| 30.0 | 0.64 | 46.56 | 44.75 | 91.31 |
| 35.0 | 0.65 | 37.29 | 45.14 | 82.40 |
| 40.0 | 0.66 | 29.17 | 45.60 | 75.50 |
| 45.0 | 0.67 | 22.33 | 46.11 | 70.97 |
| 50.0 | 0.68 | 17.03 | 47.31 | 64.62 |
| 55.0 | 0.69 | 13.15 | 48.01 | 63.14 |
| 60.0 | 0.70 | 11.34 | 48.76 | 62.30 |
| 65.0 | 0.71 | 10.59 | 49.57 | 61.97 |
| 70.0 | 0.72 | 10.05 | 50.45 | 62.04 |
| 75.0 | 0.73 | 9.53 | 51.38 | 62.43 |
| 80.0 | 0.74 | 9.07 | 52.33 | 63.11 |
| 85.0 | 0.75 | 8.62 | 53.45 | 64.02 |
| 90.0 | 0.76 | 8.15 | 54.55 | 65.16 |
| 95.0 | 0.77 | 7.66 | 55.72 | 66.51 |
| 100.0 | 0.78 | 7.15 | 56.96 | 68.06 |
| 105.0 | 0.79 | 6.60 | 58.26 | 69.73 |
| 110.0 | 0.80 | 6.03 | 59.61 | 71.86 |
| 115.0 | 0.81 | 5.45 | 61.03 | 73.20 |
| 120.0 | 0.82 | 4.87 | 62.50 | 74.74 |
| 125.0 | 0.83 | 4.27 | 64.04 | 76.51 |
| 130.0 | 0.84 | 3.65 | 65.63 | 78.51 |
| 135.0 | 0.85 | 3.00 | 67.30 | 81.51 |
| 140.0 | 0.86 | 2.33 | 69.02 | 84.75 |
| 145.0 | 0.87 | 1.65 | 70.80 | 87.25 |
| 150.0 | 0.88 | 0.95 | 72.63 | 91.02 |
| 155.0 | 0.89 | 0.25 | 74.53 | 95.08 |
| 160.0 | 0.90 | 0.00 | 76.49 | 99.46 |
| 165.0 | 0.91 | 0.00 | 78.51 | 103.16 |
| 170.0 | 0.92 | 0.00 | 80.59 | 107.22 |
| 175.0 | 0.93 | 0.00 | 82.73 | 111.65 |
| 180.0 | 0.94 | 0.00 | 84.93 | 116.48 |
| 185.0 | 0.95 | 0.00 | 87.19 | 121.75 |
| 190.0 | 0.96 | 0.00 | 89.51 | 127.51 |

VERTICAL STABILIZER DATA

| | | |
|--------------------------------------|----------|-----------|
| SECTION COEFFICIENT OF LIFT | 80 KNOTS | 160 KNOTS |
| ANGLE OF ATTACK TO UNLOAD TAIL ROTOR | 0.83326 | 0.46359 |
| | 22.263 | 3.268 |

| | |
|---------------------------------|------------|
| RADIUS | 26.733826 |
| MAIN ROTOR CHORD | 1.600000 |
| NUMBER OF MAIN ROTOR BLADES | 0.000000 |
| AIRCRAFT GROSS WEIGHT | 17585.0703 |
| ROTOR TIP VELOCITY | 725.978027 |
| HORIZONTAL FLAT PLATE AREA | 29.308441 |
| NUMBER OF ENGINES IN HELICOPTER | 0.000000 |

| | |
|--------------------------------|------------|
| MAIN ROTOR HEIGHT ABOVE GROUND | 23.000000 |
| AIR DENSITY (ρ) | 0.002197 |
| SONIC VELOCITY | 1154.32056 |
| BLADE GEOMETRIC TWIST | -0.174533 |

| | |
|----------------------------------|------------|
| MAXIMUM 2-D LIFT COEFFICIENT | 1.250000 |
| 2-D STATIC STALL ANGLE (AMAX) | 0.1983330 |
| LIFT CURVE SLOPE (/RAD) | 6.302530 |
| ZERO-LIFT DRAG COEFFICIENT | 0.010000 |
| CRITICAL MACH NO (FOR $CL = 0$) | 0.720000 |
| COEFFICIENT OF THRUST | 0.006765 |
| DISC AREA | 2245.28784 |
| SOLIDITY | 0.076202 |
| TIP-LOSS FACTOR | 0.970920 |
| GROUND EFFECT RATIO | 0.874897 |

 FORWARD VELOCITY IN KNOTS = 0.0

 DISK PLANE ANGLE OF ATTACK = 0.0

DYNAMIC PARAMETERS

Al1..... 0.0
 Al2..... 0.0
 Al3..... 0.0
 Al4..... 1.000000
 T1..... 0.471343
 T2..... 0.305091
 T3..... 0.222164
 T4..... 0.0
 INFLOW RATIO (LAMBDA)..... -0.058160

STALL PCWER CALCULATIONS

RT..... -0.028292
 INBOARD STALL CORRECTION FACTOR..... 0.0
 STALL PCWER COEFFICIENT..... 0.0

ANGLE OF ATTACK CALCULATIONS

LONGITUDINAL CYCLIC ANGLE(DEG)..... 0.0
 LONGITUDINAL COLLECTIVE ANGLE(DEG)..... 17.720932
 ALPHA(90) (DEG)..... 4.388375
 ALPHA(270) (DEG)..... 4.388375

HIGH SPEED MACH EFFECTS

ADVANCING BLADE TIP MACH NUMBER... 0.628922
 CRITICAL MACH NUMBER..... 0.665450
 DRAG DIVERGENCE MACH NUMBER..... 0.0
 COMPRESSIBILITY POWER COEFF..... 0.0

MAIN ROTOF POWER REQUIRED

INDUCED POWER = 1388.74
 PROFILE POWER = 326.81
 PARASITE POWER = 0.0
 COMPRESSIBILITY POWER = 0.0
 STALL POWER = 0.0
 HIGH SPEED EFFECTS = 0.0

 *** FORWARD VELOCITY IN KNOTS = 140.00 ***

DYNAMIC PARAMETERS

| | |
|-----------------------|-----------|
| A11 | 0.711244 |
| A12 | 0.947375 |
| A13 | 0.689869 |
| A14 | 1.238236 |
| T1 | 0.497838 |
| T2 | 0.356539 |
| T3 | 0.247140 |
| T4 | 0.157756 |
| INFLOW RATIO (LAMBDA) | -0.053642 |

STALL PCWER CALCULATIONS

| | |
|---------------------------------|-----------|
| RT | 0.002215 |
| INBOARD STALL CORRECTION FACTOR | 0.5647528 |
| STALL PCWER COEFFICIENT | 0.0000402 |

ANGLE OF ATTACK CALCULATIONS

| | |
|------------------------------------|-----------|
| LONGITUDINAL CYCLIC ANGLE(DEG) | -7.126393 |
| LONGITUDINAL COLLECTIVE ANGLE(DEG) | 18.903610 |
| ALPHA(90) (DEG) | -0.541373 |
| ALPHA(270) (DEG) | 13.710670 |

HIGH SPEED MACH EFFECTS

| | |
|---------------------------------|-----------|
| ADVANCING BLADE TIP MACH NUMBER | 0.8333665 |
| CRITICAL MACH NUMBER | 0.726730 |
| DRAG DIVERGENCE MACH NUMBER | 0.046935 |
| COMPRESSIBILITY POWER COEFF | 0.000044 |

MAIN ROTOR POWER REQUIRED

| | |
|-------------------------|--------|
| INDUCED POWER = | 247.98 |
| PROFILE POWER = | 475.75 |
| PARASITE POWER = | 772.58 |
| COMPRESSIBILITY POWER = | 149.96 |
| STALL PCWER = | 137.91 |

HIGH SPEED EFFECTS = 287.86

NOTE THE VELOCITY THAT HAS THE STALL ANGLE LESS
THAN OR EQUAL TO 12.5 DEGREES

| VELOCITY (KNOTS) | ANGLE (DEG) |
|---------------------|----------------|
| 126.94 | 12.1 |
| 127.94 | 12.2 |
| 128.94 | 12.3 |
| 129.94 | 12.4 |
| 130.94 | 12.6 |
| 131.94 | 12.7 |
| 132.94 | 12.8 |
| 133.94 | 12.9 |

TOTAL POWER FOR THE AIRCRAFT TO HOVER IS= 1829.48

| TOTAL ROTOR POWER PROFILE @ SSL POWER | | | | | |
|--|------------------|------------------|-------------------|---------------|----------------|
| AIR SPEED (KNOTS) | INDUCED (SHP) | PROFILE (SHP) | PARASITE (SHP) | COMP (SHP) | TOTAL (SHP) |
| 0.0 | 1430.58 | 397.31 | 0.0 | 0.0 | 1828.19 |
| 5.0 | 1414.59 | 397.35 | 0.0 | 0.0 | 1812.18 |
| 10.0 | 1366.52 | 398.26 | 0.0 | 0.0 | 1765.48 |
| 15.0 | 1291.54 | 399.43 | 0.0 | 0.0 | 1599.10 |
| 20.0 | 1155.26 | 401.08 | 0.0 | 0.0 | 1496.23 |
| 25.0 | 1088.57 | 403.20 | 0.0 | 0.0 | 1393.77 |
| 30.0 | 978.84 | 405.86 | 0.0 | 0.0 | 1300.13 |
| 35.0 | 879.23 | 408.40 | 0.0 | 0.0 | 1221.27 |
| 40.0 | 789.11 | 412.40 | 0.0 | 0.0 | 1156.50 |
| 45.0 | 712.50 | 416.88 | 0.0 | 0.0 | 1105.42 |
| 50.0 | 650.51 | 425.83 | 0.0 | 0.0 | 1067.71 |
| 55.0 | 594.51 | 431.25 | 0.0 | 0.0 | 1040.57 |
| 60.0 | 546.27 | 437.15 | 0.0 | 0.0 | 1023.85 |
| 65.0 | 503.77 | 443.55 | 0.0 | 0.0 | 1016.24 |
| 70.0 | 467.15 | 450.65 | 0.0 | 0.0 | 1015.85 |
| 75.0 | 437.68 | 457.65 | 0.0 | 0.0 | 1024.32 |
| 80.0 | 410.15 | 465.40 | 0.0 | 0.0 | 1039.71 |
| 85.0 | 387.15 | 473.68 | 0.0 | 0.0 | 1062.13 |
| 90.0 | 367.25 | 482.40 | 0.0 | 0.0 | 1091.51 |
| 95.0 | 347.25 | 491.59 | 0.0 | 0.0 | 1127.76 |
| 100.0 | 331.25 | 491.23 | 0.0 | 0.0 | 1181.98 |
| 105.0 | 316.25 | 501.23 | 0.0 | 0.0 | 1257.98 |
| 110.0 | 300.25 | 512.08 | 0.0 | 0.0 | 1327.85 |
| 115.0 | 287.25 | 523.65 | 0.0 | 0.0 | 1411.04 |
| 120.0 | 270.25 | 534.65 | 0.0 | 0.0 | 1503.73 |
| 125.0 | 253.25 | 546.14 | 0.0 | 0.0 | 1601.07 |
| 130.0 | 237.25 | 556.99 | 0.0 | 0.0 | 1708.23 |
| 135.0 | 222.25 | 569.11 | 0.0 | 0.0 | 1822.40 |
| 140.0 | 207.25 | 582.55 | 0.0 | 0.0 | 1947.91 |
| 145.0 | 192.25 | 599.83 | 0.0 | 0.0 | 2083.83 |
| 150.0 | 177.25 | 623.67 | 0.0 | 0.0 | 2239.91 |
| 155.0 | 162.25 | 638.99 | 0.0 | 0.0 | 2417.28 |
| 160.0 | 147.25 | 653.79 | 0.0 | 0.0 | 2562.63 |
| 165.0 | 132.25 | 669.05 | 0.0 | 0.0 | 2723.80 |
| 170.0 | 117.25 | 686.79 | 0.0 | 0.0 | 2887.15 |
| 175.0 | 102.25 | 702.99 | 0.0 | 0.0 | 3057.62 |
| 180.0 | 87.25 | 719.67 | 0.0 | 0.0 | 3233.44 |
| 185.0 | 72.25 | 737.13 | 0.0 | 0.0 | 3418.59 |

| AIR SPEED (KNOTS) | AT SPECIFICATION | TOTAL ROTOR ALTITUDE (SHF) | POWER (SHF) | PROFILE (SHF) | PARASITE (SHF) | TEMPERATURE (SHF) | TOTAL (SHF) |
|----------------------|------------------|-------------------------------|----------------|------------------|-------------------|----------------------|----------------|
| 0.00 | 1451.31 | 367.17 | 0.00 | 0.00 | 0.00 | 1858.21 | |
| 5.00 | 1475.18 | 367.38 | 0.00 | 0.00 | 0.00 | 1842.73 | |
| 10.00 | 1429.00 | 368.04 | 0.00 | 0.00 | 0.00 | 1797.50 | |
| 15.00 | 1356.00 | 369.13 | 0.00 | 0.00 | 0.00 | 1726.08 | |
| 20.00 | 1155.00 | 370.61 | 0.00 | 0.00 | 0.00 | 1634.75 | |
| 25.00 | 1146.00 | 375.01 | 0.00 | 0.00 | 0.00 | 1532.32 | |
| 30.00 | 1146.00 | 377.84 | 0.00 | 0.00 | 0.00 | 1428.12 | |
| 35.00 | 1146.00 | 381.11 | 0.00 | 0.00 | 0.00 | 1332.91 | |
| 40.00 | 1146.00 | 384.81 | 0.00 | 0.00 | 0.00 | 1247.91 | |
| 45.00 | 1146.00 | 388.95 | 0.00 | 0.00 | 0.00 | 1177.81 | |
| 50.00 | 1146.00 | 393.52 | 0.00 | 0.00 | 0.00 | 1121.51 | |
| 55.00 | 1146.00 | 398.58 | 0.00 | 0.00 | 0.00 | 1078.59 | |
| 60.00 | 1146.00 | 403.86 | 0.00 | 0.00 | 0.00 | 1046.80 | |
| 65.00 | 1146.00 | 409.18 | 0.00 | 0.00 | 0.00 | 1024.10 | |
| 70.00 | 1146.00 | 416.93 | 0.00 | 0.00 | 0.00 | 1012.68 | |
| 75.00 | 1146.00 | 422.12 | 0.00 | 0.00 | 0.00 | 1007.94 | |
| 80.00 | 1146.00 | 430.74 | 0.00 | 0.00 | 0.00 | 1021.42 | |
| 85.00 | 1146.00 | 437.80 | 0.00 | 0.00 | 0.00 | 1038.81 | |
| 90.00 | 1146.00 | 445.22 | 0.00 | 0.00 | 0.00 | 1062.90 | |
| 95.00 | 1146.00 | 454.29 | 0.00 | 0.00 | 0.00 | 1094.04 | |
| 100.00 | 1146.00 | 463.59 | 0.00 | 0.00 | 0.00 | 1148.36 | |
| 110.00 | 1146.00 | 472.33 | 0.00 | 0.00 | 0.00 | 1210.67 | |
| 115.00 | 1146.00 | 482.30 | 0.00 | 0.00 | 0.00 | 1278.82 | |
| 120.00 | 1146.00 | 492.30 | 0.00 | 0.00 | 0.00 | 1353.08 | |
| 125.00 | 1146.00 | 503.41 | 0.00 | 0.00 | 0.00 | 1435.08 | |
| 130.00 | 1146.00 | 514.96 | 0.00 | 0.00 | 0.00 | 1521.47 | |
| 135.00 | 1146.00 | 525.94 | 0.00 | 0.00 | 0.00 | 1621.07 | |
| 140.00 | 1146.00 | 537.35 | 0.00 | 0.00 | 0.00 | 1863.80 | |
| 145.00 | 1146.00 | 550.20 | 0.00 | 0.00 | 0.00 | 2046.22 | |
| 150.00 | 1146.00 | 563.41 | 0.00 | 0.00 | 0.00 | 2235.55 | |
| 155.00 | 1146.00 | 576.97 | 0.00 | 0.00 | 0.00 | 2461.30 | |
| 160.00 | 1146.00 | 590.49 | 0.00 | 0.00 | 0.00 | 2614.83 | |
| 165.00 | 1146.00 | 604.97 | 0.00 | 0.00 | 0.00 | 2753.66 | |
| 170.00 | 1146.00 | 618.00 | 0.00 | 0.00 | 0.00 | 2900.96 | |
| 175.00 | 1146.00 | 634.46 | 0.00 | 0.00 | 0.00 | 3055.21 | |
| 180.00 | 1146.00 | 649.36 | 0.00 | 0.00 | 0.00 | 3220.03 | |
| 185.00 | 1146.00 | 665.17 | 0.00 | 0.00 | 0.00 | 3394.00 | |
| 190.00 | 1146.00 | 681.68 | 0.00 | 0.00 | 0.00 | 3577.13 | |

THE REQUIRED SHAFT HORSEPOWER IS = 3013.56

FOR 2 ENGINE(S), THE REQUIRED SHAFT HORSEPOWER IS= 3415.32

| | ENGINE SELECTION CRITERIA | | | | | |
|-------------------------|---------------------------|--------|--------|----------|--------|--------|
| | 1 ENGINE | | | 2 ENGINE | | |
| | A | B | C | D | E | F |
| POWERPLANT WEIGHT(LB): | 158.0 | 288.0 | 423.0 | 709.0 | 580.0 | 750.0 |
| LIFE-CYCLE COST(\$10M): | 3.00 | 5.97 | 10.95 | 14.50 | 18.13 | 25.39 |
| ENGINE LIFE(HRS): | 600.0 | 750.0 | 800.0 | 800.0 | 1000.0 | 750.0 |
| NUMBER OF REPLACEMENTS: | 4.0 | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 |
| R AND D COST(\$K): | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| INITIAL COST(\$K): | 93.0 | 100.0 | 580.0 | 360.0 | 640.0 | 700.0 |
| YEAR MAINT COST(\$K): | 7.50 | 15.00 | 30.00 | 37.50 | 48.00 | 66.00 |
| YEAR OPERATE COST(\$K): | 2.40 | 4.80 | 6.00 | 10.50 | 12.00 | 18.00 |
| REPLACEMENT CCST(\$K): | 125.55 | 135.00 | 783.00 | 486.00 | 864.00 | 945.00 |
| SALVAGE VALUE(\$K): | 74.40 | 80.00 | 464.00 | 288.00 | 512.00 | 560.00 |
| AVAILABILITY(ENG): | 0.8333 | 0.8333 | 0.8000 | 0.6977 | 0.6667 | 0.5738 |
| RELIABILITY(ENG): | 0.9892 | 0.9905 | 0.9903 | 0.9930 | 0.9929 | 0.9938 |
| MAINTAINABILITY(ENG): | 0.350 | 0.300 | 0.250 | 0.650 | 1.000 | 1.300 |
| PERFORMANCE(SHP-MIL): | 420.0 | 708.0 | 1561.0 | 1800.0 | 2500.0 | 3400.0 |

| | ENGINE SELECTION CRITERIA | | | | | |
|-------------------------|---------------------------|--------|---------|----------|---------|---------|
| | 1 ENGINE | | | 2 ENGINE | | |
| | A | B | C | D | E | F |
| POWERPLANT WEIGHT(LB): | 316.0 | 576.0 | 846.0 | 1418.0 | 1160.0 | 1500.0 |
| LIFE-CYCLE COST(\$10M): | 6.00 | 11.93 | 21.91 | 28.99 | 36.27 | 50.77 |
| ENGINE LIFE(HRS): | 600.0 | 750.0 | 800.0 | 800.0 | 1000.0 | 750.0 |
| NUMBER OF REPLACEMENTS: | 8.0 | 6.0 | 5.0 | 5.0 | 4.0 | 6.0 |
| R AND D COST(\$K): | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| INITIAL COST(\$K): | 186.0 | 200.0 | 1160.0 | 720.0 | 1280.0 | 1400.0 |
| YEAR MAINT COST(\$K): | 15.00 | 30.00 | 60.00 | 75.00 | 96.00 | 132.00 |
| YEAR OPERATE COST(\$K): | 4.80 | 9.60 | 12.00 | 21.00 | 24.00 | 36.00 |
| REPLACEMENT CCST(\$K): | 251.10 | 270.00 | 1566.00 | 576.00 | 1728.00 | 1890.00 |
| SALVAGE VALUE(\$K): | 148.80 | 160.00 | 928.00 | 576.00 | 1024.00 | 1120.00 |
| AVAILABILITY(ENG): | 0.8333 | 0.8333 | 0.8000 | 0.6977 | 0.6667 | 0.5738 |
| RELIABILITY(ENG): | 0.9892 | 0.9905 | 0.9903 | 0.9930 | 0.9929 | 0.9938 |
| MAINTAINABILITY(ENG): | 0.350 | 0.300 | 0.250 | 0.650 | 1.000 | 1.300 |
| PERFORMANCE(SHP-MIL): | 840.0 | 1416.0 | 3122.0 | 3600.0 | 5000.0 | 6800.0 |

THE REQUIRED SHAFT HORSEPOWER IS = 3415.32

OLD GROSS WEIGHT = 17585.07
NEW GROSS WEIGHT = 18409.23

-----FUEL FLOW RATES-----
 MILITARY POWER 2142.00 NOR MAL POWER 1854.36 CRUISE POWER 1517.66

TEMPERATURE (R) = 504.423
 PRESSURE (PSF) = 1827.697
 ALPHA AT SSL = 624.344
 THETA AT SPEC ALTITUDE = 0.972
 DELTA AT SPEC ALTITUDE = 0.864
 ZEROC HORSEPOWER INTERCEPT = 531.755
 AT SPEC ALTITUDE

THE ZERO HORSEPOWER INCREMENT AT ALTITUDE= 2221.240

THE FUEL WEIGHT IS = 3959.12LBS
 THE DESIGN GROSS WEIGHT IS = 18368.34
 THE ESTIMATED GRCS WEIGHT IS = 17585.07

THE BEST RATE OF CLIMB IS 3800.00 FEET PER MINUTE

THE HOVER CEILING ALTITUDE IS = 12000.00

THE SERVICE CEILING ALTITUDE IS = 21000.00

PERFORMANCE

GEOMETRY

| | | | |
|---|---------------------|--|---------|
| WEIGHT (LBS) - | MAX GROSS | | 18000.0 |
| FUEL CAPACITY (GAL) | - EMPTY | | 9095.5 |
| | - INTERNAL | | 609.1 |
| | - EXTERNAL | | 0.0 |
| MAIN ROTOR - | CHORD (FT) | | 1.60 |
| | RADIUS (FT) | | 26.73 |
| | NUMBER OF BLADES | | 4 |
| | DRAW COEFFICIENT | | 0.0100 |
| | ROTATIONAL VELOCITY | | 27.16 |
| | SOLIDITY | | 0.0762 |
| TAIL ROTOR - | CHORD (FT) | | 0.91 |
| | RADIUS (FT) | | 5.45 |
| | NUMBER OF BLADES | | 4 |
| | DRAW COEFFICIENT | | 0.0138 |
| | ROTATIONAL VELOCITY | | 122.20 |
| | SOLIDITY | | 0.2122 |
| VERTICAL TAIL AREA (FT ²) | | | 35.43 |
| FUSELAGE LENGTH (FT) | | | 50.10 |
| EQUIVALENT FLAT PLATE AREA (FT ²) | | | 29.31 |
| | FORWARD VERTICAL | | 58.62 |

COST ANALYSIS PER VEHICLE (IN DOLLARS FOR 100 A/C RUN)

| | | | |
|------------------------|---|---|------------|
| ROTOR | | = | 207647.31 |
| TAIL: RCTOR | | = | 11561.87 |
| STRUCTURE | | = | 20104.41 |
| BODY | | = | 182568.06 |
| LANDING GEAR | | = | 119506.94 |
| NACELLE | | = | 34988.90 |
| PROPULSION: ENGINE | | = | 1281599.00 |
| DRIVE | | = | 121739.87 |
| FUEL TANKS | | = | 160159.44 |
| FLIGHT CCNTFOLS | | = | 109443.50 |
| AUXILLARY PCWER | | = | 54357.60 |
| INSTRUMENTS | | = | 15419.93 |
| HYDRAULICAL | | = | 8067.89 |
| ELECTRICAL | | = | 68819.69 |
| AVIONICS | | = | 52901.66 |
| FURNISHINGS | | = | 35208.07 |
| AIR AND ICE | | = | 21086.03 |
| LOAD AND HANDLING | | = | 20675.80 |
| TOTAL CCST PER VEHICLE | = | | 2525889.00 |

APPENDIX C

TABLE III

AH-64 Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 24.0 | feet |
| Tail rotor radius | 4.6 | feet |
| Number of main rotor blades | 4 | |
| Number of tail rotor blades | 4 | |
| Height of the main rotor system | 12.6 | feet |
| Speed of the main rotor | 30.3 | rads/sec |
| Speed of the tail rotor | 147.0 | rads/sec |
| Chord of the main rotor | 1.75 | feet |
| Chord of the tail rotor | 0.83 | feet |
| Span of the main rotor | 18.8 | feet |
| Span of the tail rotor | 3.1 | feet |
| Twist of the main rotor blade | -9.0 | degrees |
| Twist of the tail rotor blade | -8.8 | degrees |
| Profile drag of the main rotor blade | 0.009 | |
| Profile drag of the tail rotor blade | 0.009 | |
| Disc loading of the main rotor system | 8.1 | |
| Width of the fuselage | 3.96 | feet |
| Length of the fuselage | 49.1 | feet |
| Frontal equivalent flat plate area | 34.7 | sq ft |
| Vertical equivalent flat plate area | 45.8 | sq ft |
| Maximum forward velocity | 154 | knots |
| Maximum range | 246 | nmi |
| Rate of climb | 2490 | ft/min |
| Hover ceiling (IGE) | 14,200 | feet |
| Hover ceiling (OGE) | 11,000 | feet |
| Length of the tail | 29.7 | feet |
| Operating weight | 11,010 | pounds |
| Load weight | 2,020 | pounds |
| Fuel weight | 1,620 | pounds |
| Maximum gross weight | 14,650 | pounds |

TABLE IV

OH-6A Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 16.3 | feet |
| Tail rotor radius | 4.3 | feet |
| Number of main rotor blades | 4 | |
| Number of tail rotor blades | 2 | |
| Height of the main rotor system | 7.0 | feet |
| Speed of the main rotor | 49.2 | rads/sec |
| Speed of the tail rotor | 315.0 | rads/sec |
| Chord of the main rotor | 0.57 | feet |
| Chord of the tail rotor | 0.40 | feet |
| Span of the main rotor | 11.5 | feet |
| Span of the tail rotor | 1.4 | feet |
| Twist of the main rotor blade | -9.0 | degrees |
| Twist of the tail rotor blade | -8.0 | degrees |
| Profile drag of the main rotor blade | 0.009 | |
| Profile drag of the tail rotor blade | 0.009 | |
| Disc loading of the main rotor system | 8.1 | |
| Width of the fuselage | 4.57 | feet |
| Length of the fuselage | 23.0 | feet |
| Frontal equivalent flat plate area | 5.0 | sq ft |
| Vertical equivalent flat plate area | 10.8 | sq ft |
| Maximum forward velocity | 116 | knots |
| Maximum range | 330 | nmi |
| Rate of climb | 500 | ft/min |
| Hover ceiling (IGE) | 7,100 | feet |
| Hover ceiling (OGE) | 4,200 | feet |
| Length of the tail | 15.2 | feet |
| Operating weight | 1,160 | pounds |
| Load weight | 960 | pounds |
| Fuel weight | 400 | pounds |
| Maximum gross weight | 2,520 | pounds |

TABLE V
SH-3H Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 31.0 | feet |
| Tail rotor radius | 5.3 | feet |
| Number of main rotor blades | 5 | |
| Number of tail rotor blades | 5 | |
| Height of the main rotor system | 14.3 | feet |
| Speed of the main rotor | 21.3 | rads/sec |
| Speed of the tail rotor | 130.0 | rads/sec |
| Chord of the main rotor | 1.52 | feet |
| Chord of the tail rotor | 0.61 | feet |
| Span of the main rotor | 29.3 | feet |
| Span of the tail rotor | 4.0 | feet |
| Twist of the main rotor blade | -8.0 | degrees |
| Twist of the tail rotor blade | 0.0 | degrees |
| Profile drag of the main rotor blade | 0.0095 | |
| Profile drag of the tail rotor blade | 0.0105 | |
| Disc loading of the main rotor system | 6.96 | |
| Width of the fuselage | 7.08 | feet |
| Length of the fuselage | 31.3 | feet |
| Frontal equivalent flat plate area | 31.3 | sq ft |
| Vertical equivalent flat plate area | 36.0 | sq ft |
| Maximum forward velocity | 120 | knots |
| Maximum range | 505 | nmi |
| Rate of climb | 500 | ft/min |
| Hover ceiling (IGE) | 3,700 | feet |
| Hover ceiling (OGE) | 4,000 | feet |
| Length of the tail | 36.6 | feet |
| Operating weight | 13,600 | pounds |
| Load weight | 1,760 | pounds |
| Fuel weight | 5,640 | pounds |
| Maximum gross weight | 21,000 | pounds |

TABLE VI

S-76 Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 22.0 | feet |
| Tail rotor radius | 4.0 | feet |
| Number of main rotor blades | 4 | |
| Number of tail rotor blades | 4 | |
| Height of the main rotor system | 10.0 | feet |
| Speed of the main rotor | 30.7 | rads/sec |
| Speed of the tail rotor | 168.0 | rads/sec |
| Chord of the main rotor | 1.29 | feet |
| Chord of the tail rotor | 0.54 | feet |
| Span of the main rotor | 17.0 | feet |
| Span of the tail rotor | 3.3 | feet |
| Twist of the main rotor blade | -10.0 | degrees |
| Twist of the tail rotor blade | -8.0 | degrees |
| Profile drag of the main rotor blade | 0.009 | |
| Profile drag of the tail rotor blade | 0.015 | |
| Disc loading of the main rotor system | 8.1 | |
| Width of the fuselage | 7.00 | feet |
| Length of the fuselage | 43.4 | feet |
| Frontal equivalent flat plate area | 11.6 | sq ft |
| Vertical equivalent flat plate area | 30.0 | sq ft |
| Maximum forward velocity | 155 | knots |
| Maximum range | 404 | nmi |
| Rate of climb | 425 | ft/min |
| Hover ceiling (IGE) | 6,200 | feet |
| Hover ceiling (OGE) | 2,800 | feet |
| Length of the tail | 26.5 | feet |
| Operating weight | 5,600 | pounds |
| Load weight | 2,520 | pounds |
| Fuel weight | 1,880 | pounds |
| Maximum gross weight | 10,000 | pounds |

TABLE VII
UH-60A Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 26.8 | feet |
| Tail rotor radius | 4.0 | feet |
| Number of main rotor blades | 4 | |
| Number of tail rotor blades | 4 | |
| Height of the main rotor system | 11.2 | feet |
| Speed of the main rotor | 27.2 | rads/sec |
| Speed of the tail rotor | 125.0 | rads/sec |
| Chord of the main rotor | 1.75 | feet |
| Chord of the tail rotor | 0.81 | feet |
| Span of the main rotor | 29.3 | feet |
| Span of the tail rotor | 4.25 | feet |
| Twist of the main rotor blade | -18.0 | degrees |
| Twist of the tail rotor blade | -18.0 | degrees |
| Profile drag of the main rotor blade | 0.008 | |
| Profile drag of the tail rotor blade | 0.008 | |
| Disc loading of the main rotor system | 8.95 | |
| Width of the fuselage | 7.75 | feet |
| Length of the fuselage | 50.1 | feet |
| Frontal equivalent flat plate area | 25.7 | sq ft |
| Vertical equivalent flat plate area | 30.8 | sq ft |
| Maximum forward velocity | 156 | knots |
| Maximum range | 275 | nmi |
| Rate of climb | 200 | ft/min |
| Hover ceiling (IGE) | 7,800 | feet |
| Hover ceiling (OGE) | 3,900 | feet |
| Length of the tail | 31.5 | feet |
| Operating weight | 10,680 | pounds |
| Load weight | 7,270 | pounds |
| Fuel weight | 2,350 | pounds |
| Maximum gross weight | 20,250 | pounds |

TABLE VIII

CH-54B Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 36.0 | feet |
| Tail rotor radius | 8.0 | feet |
| Number of main rotor blades | 6 | |
| Number of tail rotor blades | 4 | |
| Height of the main rotor system | 17.6 | feet |
| Speed of the main rotor | 19.4 | rads/sec |
| Speed of the tail rotor | 66.0 | rads/sec |
| Chord of the main rotor | 1.97 | feet |
| Chord of the tail rotor | 1.28 | feet |
| Span of the main rotor | 29.8 | feet |
| Span of the tail rotor | 6.45 | feet |
| Twist of the main rotor blade | -8.0 | degrees |
| Twist of the tail rotor blade | -8.0 | degrees |
| Profile drag of the main rotor blade | 0.0095 | |
| Profile drag of the tail rotor blade | 0.0105 | |
| Disc loading of the main rotor system | 10.3 | |
| Width of the fuselage | 7.08 | feet |
| Length of the fuselage | 70.2 | feet |
| Frontal equivalent flat plate area | 65.0 | sq ft |
| Vertical equivalent flat plate area | 99.4 | sq ft |
| Maximum forward velocity | 110 | knots |
| Maximum range | 200 | nmi |
| Rate of climb | 189 | ft/min |
| Hover ceiling (IGE) | 6,400 | feet |
| Hover ceiling (OGE) | 2,400 | feet |
| Length of the tail | 44.5 | feet |
| Operating weight | 19,230 | pounds |
| Load weight | 14,190 | pounds |
| Fuel weight | 8,580 | pounds |
| Maximum gross weight | 42,000 | pounds |

TABLE IX

CH-53D Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 36.1 | feet |
| Tail rotor radius | 8.0 | feet |
| Number of main rotor blades | 6 | |
| Number of tail rotor blades | 4 | |
| Height of the main rotor system | 15.8 | feet |
| Speed of the main rotor | 19.4 | rads/sec |
| Speed of the tail rotor | 83.0 | rads/sec |
| Chord of the main rotor | 2.17 | feet |
| Chord of the tail rotor | 1.28 | feet |
| Span of the main rotor | 28.9 | feet |
| Span of the tail rotor | 6.45 | feet |
| Twist of the main rotor blade | -6.0 | degrees |
| Twist of the tail rotor blade | -8.0 | degrees |
| Profile drag of the main rotor blade | 0.0095 | |
| Profile drag of the tail rotor blade | 0.0095 | |
| Disc loading of the main rotor system | 10.3 | |
| Width of the fuselage | 8.83 | feet |
| Length of the fuselage | 67.2 | feet |
| Frontal equivalent flat plate area | 47.3 | sq ft |
| Vertical equivalent flat plate area | 90.0 | sq ft |
| Maximum forward velocity | 164 | knots |
| Maximum range | 242 | nmi |
| Rate of climb | 625 | ft/min |
| Hover ceiling (IGE) | 14,000 | feet |
| Hover ceiling (OGE) | 8,000 | feet |
| Length of the tail | 44.5 | feet |
| Operating weight | 23,630 | pounds |
| Load weight | 14,030 | pounds |
| Fuel weight | 4,340 | pounds |
| Maximum gross weight | 42,000 | pounds |

TABLE X
CH-53E Data

| <u>Parameter</u> | <u>Value</u> | |
|---------------------------------------|--------------|----------|
| Main rotor radius | 38.5 | feet |
| Tail rotor radius | 10.0 | feet |
| Number of main rotor blades | 7 | |
| Number of tail rotor blades | 4 | |
| Height of the main rotor system | 16.0 | feet |
| Speed of the main rotor | 18.7 | rads/sec |
| Speed of the tail rotor | 73.0 | rads/sec |
| Chord of the main rotor | 2.44 | feet |
| Chord of the tail rotor | 1.28 | feet |
| Span of the main rotor | 28.6 | feet |
| Span of the tail rotor | 8.53 | feet |
| Twist of the main rotor blade | -13.6 | degrees |
| Twist of the tail rotor blade | -8.0 | degrees |
| Profile drag of the main rotor blade | 0.009 | |
| Profile drag of the tail rotor blade | 0.0095 | |
| Disc loading of the main rotor system | 15.0 | |
| Width of the fuselage | 8.83 | feet |
| Length of the fuselage | 99.0 | feet |
| Frontal equivalent flat plate area | 120.0 | sq ft |
| Vertical equivalent flat plate area | 63.6 | sq ft |
| Maximum forward velocity | 146 | knots |
| Maximum range | 400 | nmi |
| Rate of climb | 325 | ft/min |
| Hover ceiling (IGE) | 6,000 | feet |
| Hover ceiling (OGE) | 1,400 | feet |
| Length of the tail | 48.0 | feet |
| Operating weight | 24,790 | pounds |
| Load weight | 15,480 | pounds |
| Fuel weight | 25,480 | pounds |
| Maximum gross weight | 73,500 | pounds |

HELICOPTER DESIGN

AE 4308/4900

1. AH-64 8. UH-60A
2. CH-53A 9. CH-53B
3. OH-6H 7. CH-53D
4. S-70 6. CH-54E

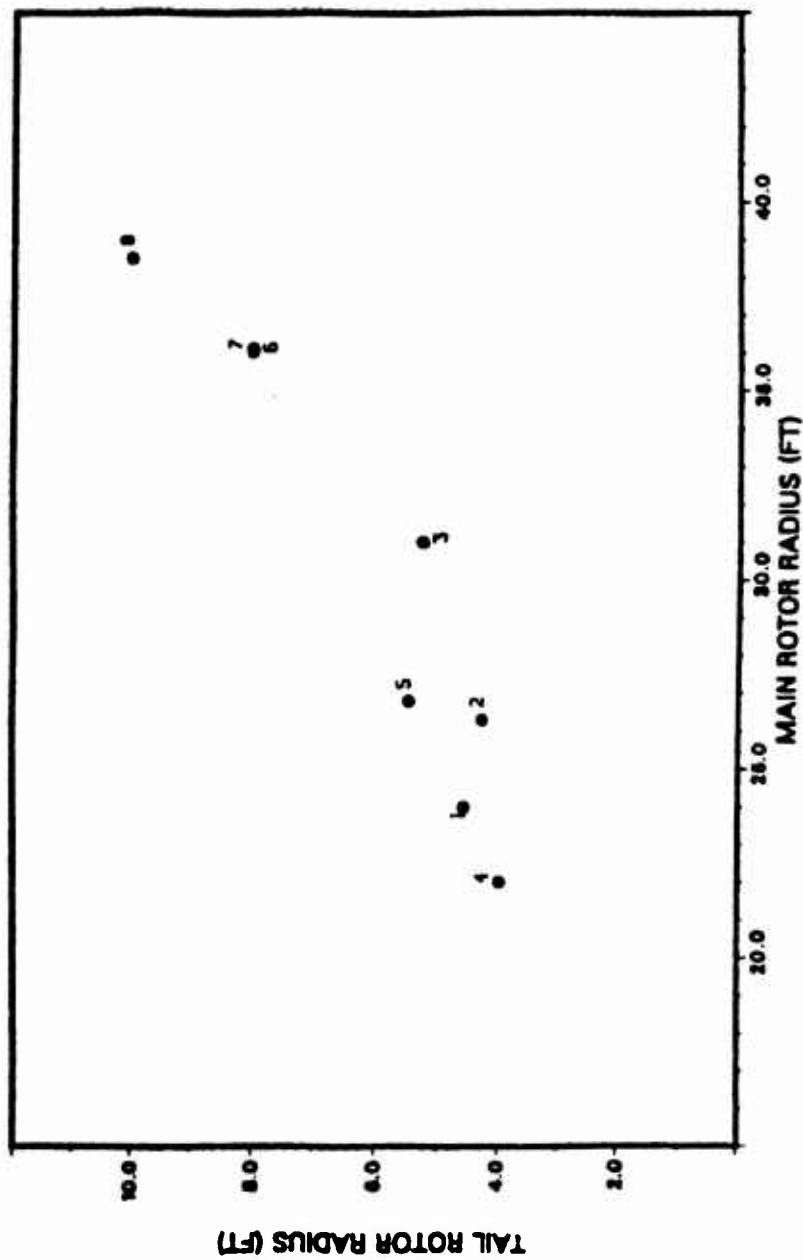


Figure 3.1. X-Y Plot (horizontal page format)

HELICOPTER DESIGN

AE 4308/4800

| | |
|----------|------------|
| 1. AH-64 | 8. UH-60A |
| 2. OH-6A | 9. CH-54E |
| 3. SH-60 | 10. CH-53D |
| 4. S-70 | 11. CH-54E |

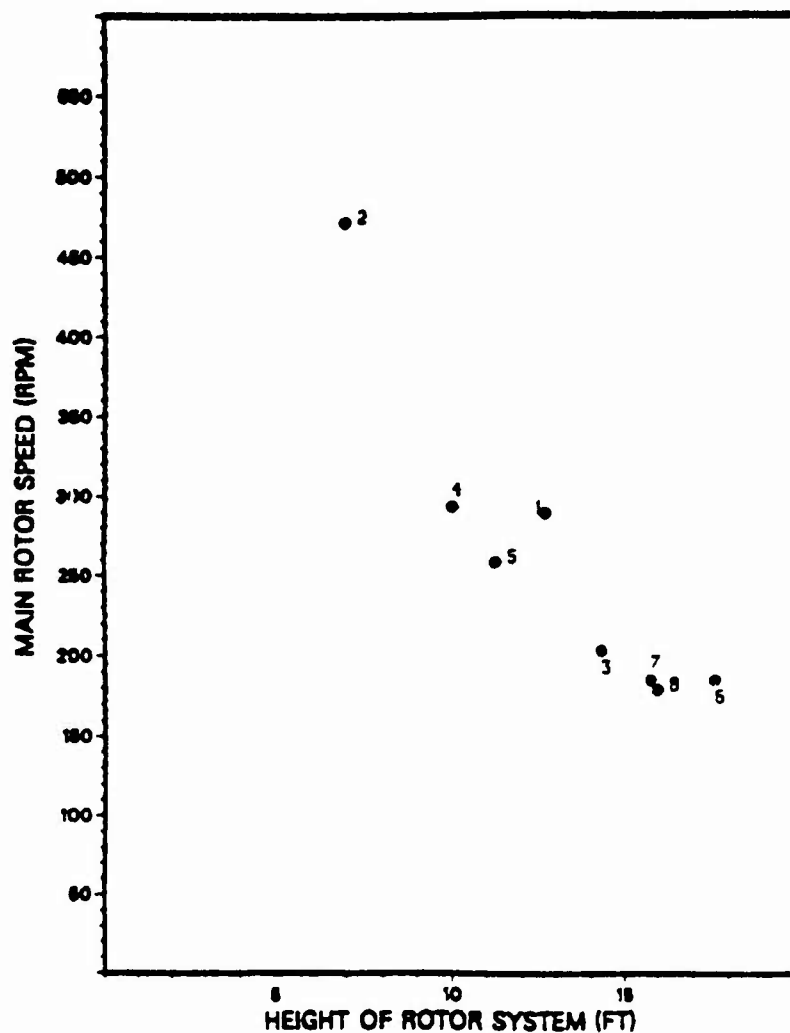


Figure 3.2. X-Y Plot (vertical page format)

HELICOPTER DESIGN

AE 4308/4900

- | | |
|-----------|-----------|
| 1. AH-64 | 8. UH-60A |
| 2. CH-53A | 9. CH-54E |
| 3. SH-3H | 7. CH-53D |
| 4. S-70 | 6. CH-54E |

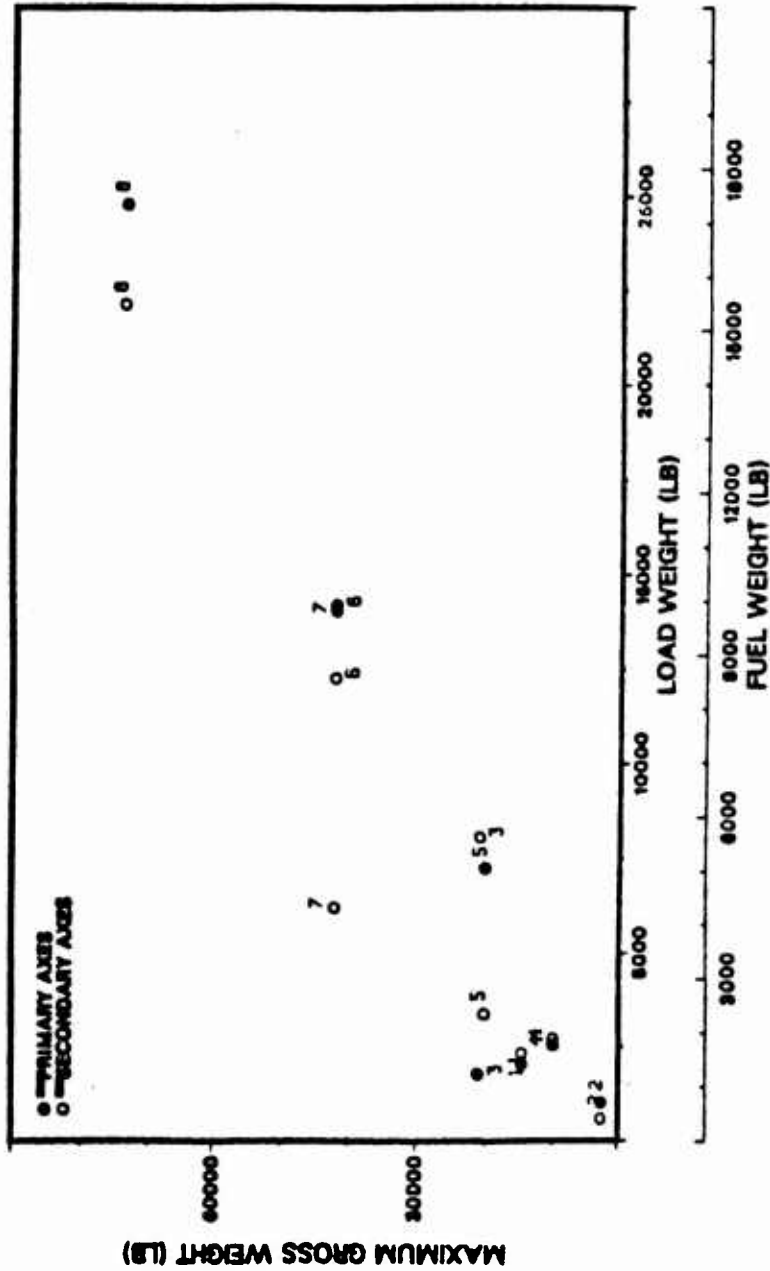


Figure 3.3. Multiple X Axes Plot (horizontal page format)

HELICOPTER DESIGN

AE 4308/4800

| | |
|----------|-----------|
| 1. AH-64 | 5. UH-60A |
| 2. OH-6A | 6. CH-54B |
| 3. SH-60 | 7. CH-53D |
| 4. S-70 | 8. CH-54E |

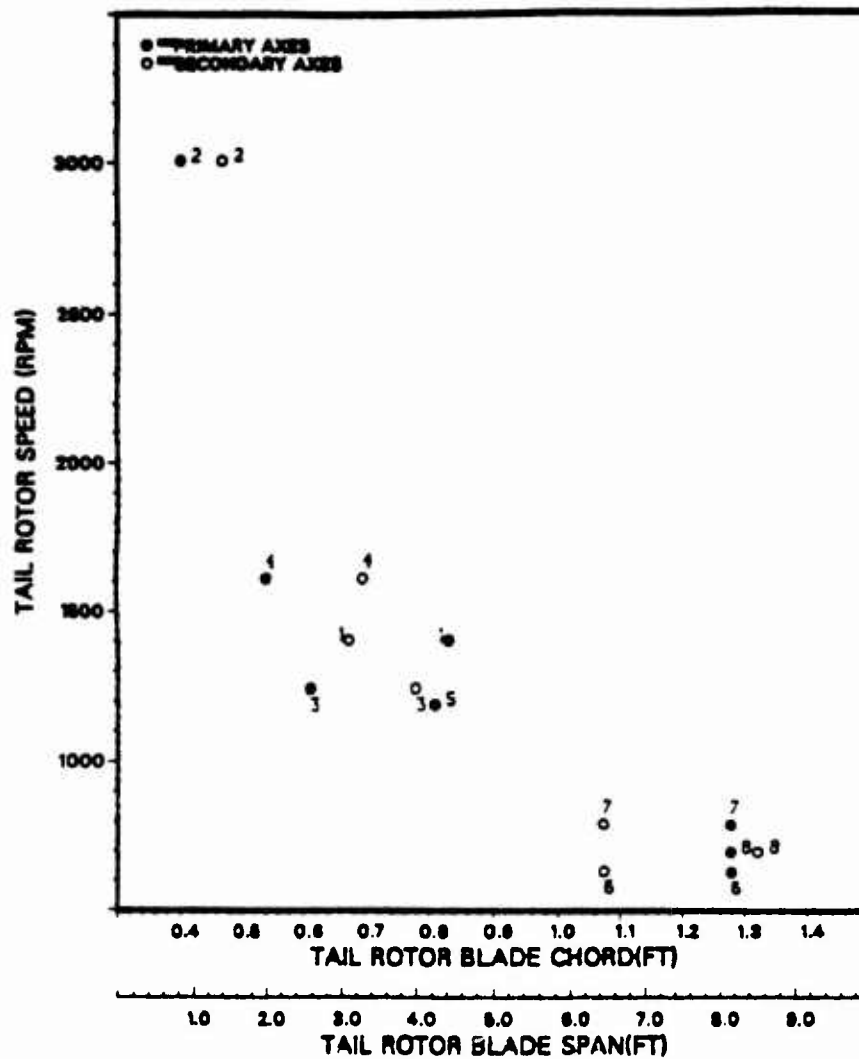


Figure 3.4. Multiple X Axes Plot (vertical page format)

HELICOPTER DESIGN

AE 4306/4900

1. AH-64 2. UH-60A
3. CH-53A 4. CH-53E
5. SH-60 6. CH-53D
7. CH-53E
8. CH-53E

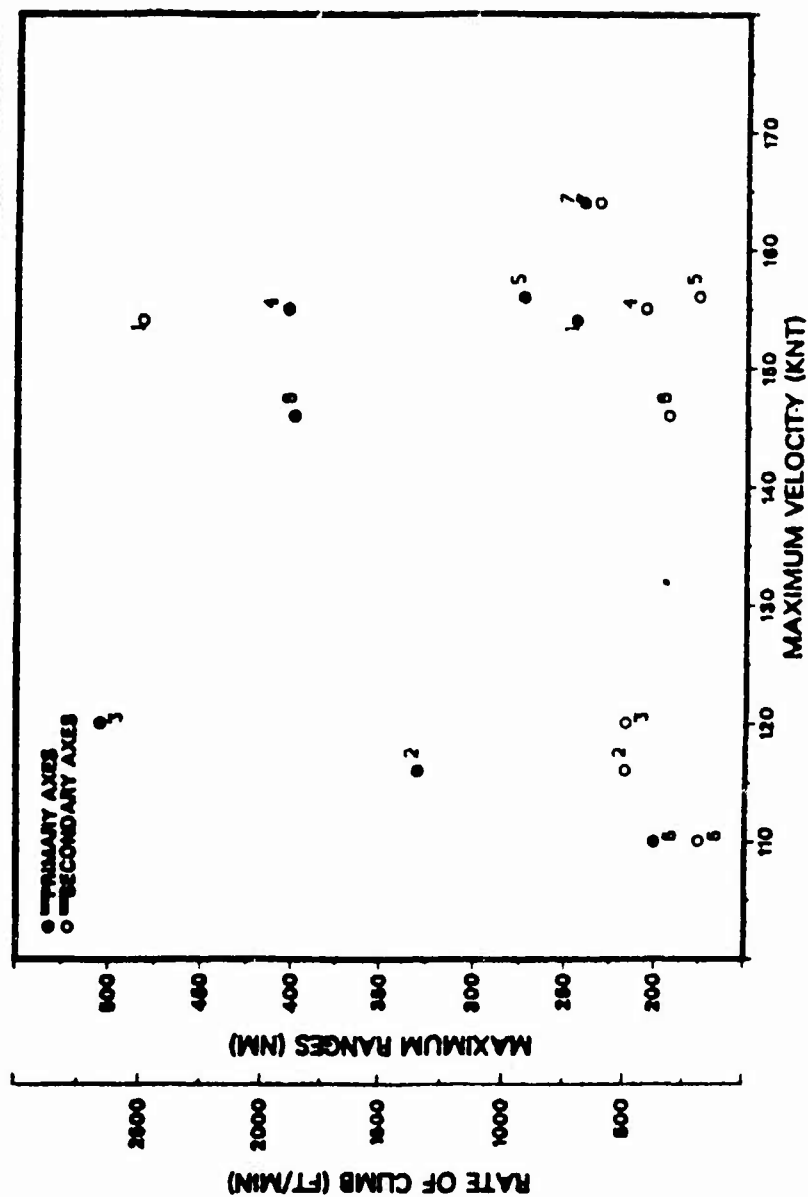


Figure 3.5. Multiple Y Axes Plot (horizontal page format)

HELICOPTER DESIGN

AE 4308/4800

| | |
|-----------|-----------|
| 1. AH-64 | 5. UH-60A |
| 2. CH-53A | 6. CH-53E |
| 3. SH-60B | 7. CH-53D |
| 4. S-70 | 8. CH-53F |

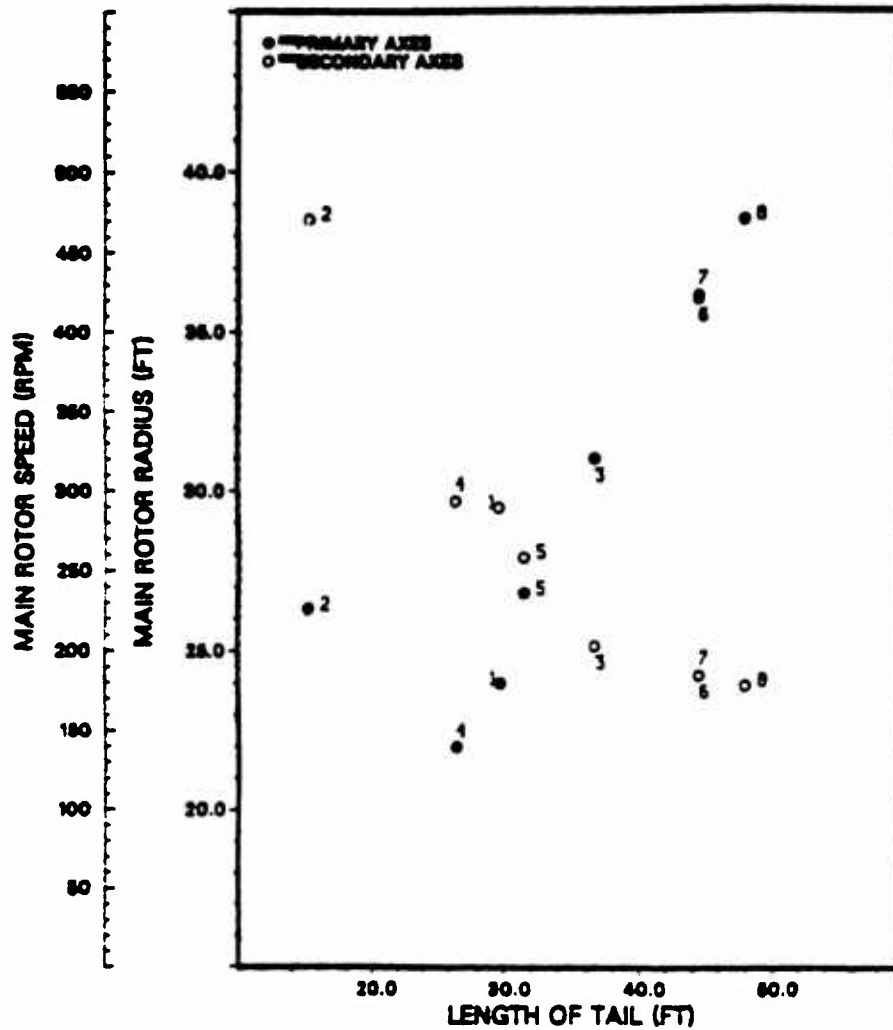


Figure 3.6. Multiple Y Axes Plot (vertical page format)

HELICOPTER DESIGN AE 4308/4900

- 1. AH-64
- 2. CH-53A
- 3. CH-53E
- 4. S-70
- 5. UH-60A
- 6. CH-540
- 7. CH-53D
- 8. CH-54E

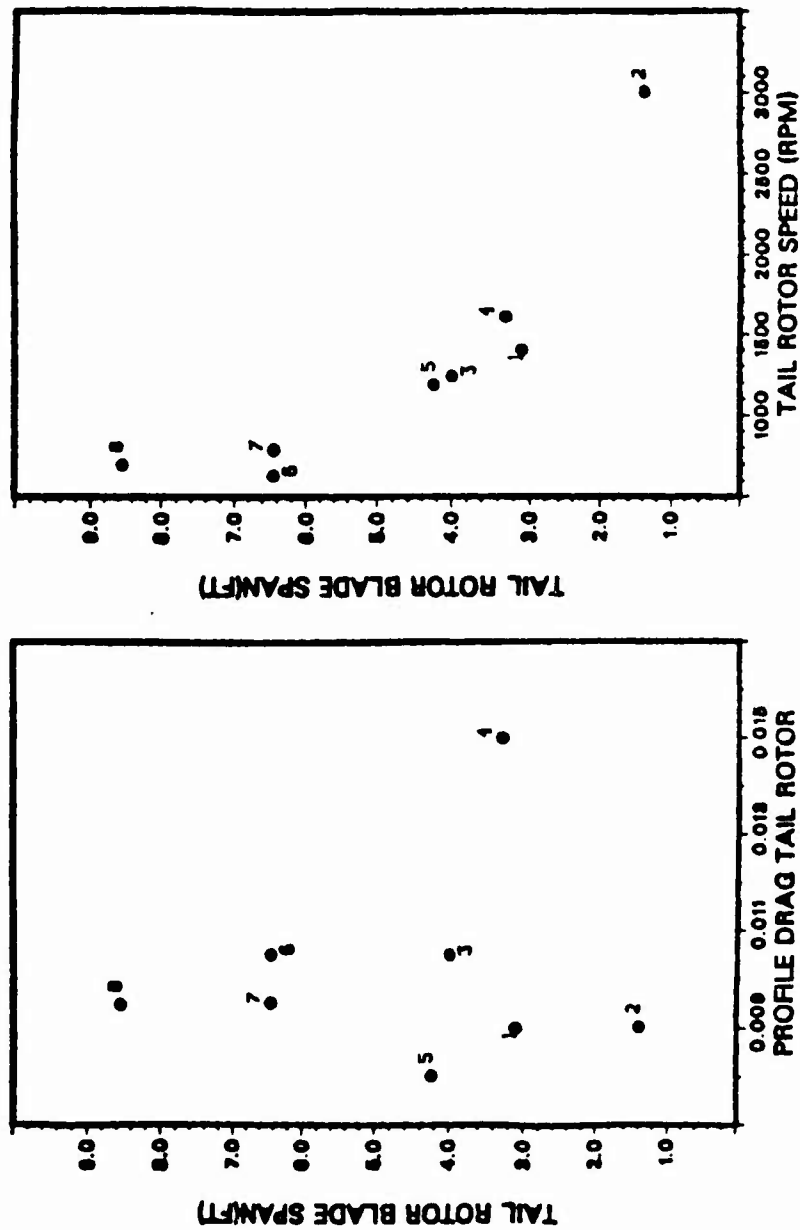


Figure 3.7. Two Plot Option

HELICOPTER DESIGN

AE 4308/4800

| | |
|----------|-----------|
| 1. AH-64 | 8. UH-60A |
| 2. OH-6A | 9. CH-53A |
| 3. SH-3H | 7. CH-53D |
| 4. S-70 | 6. CH-54E |

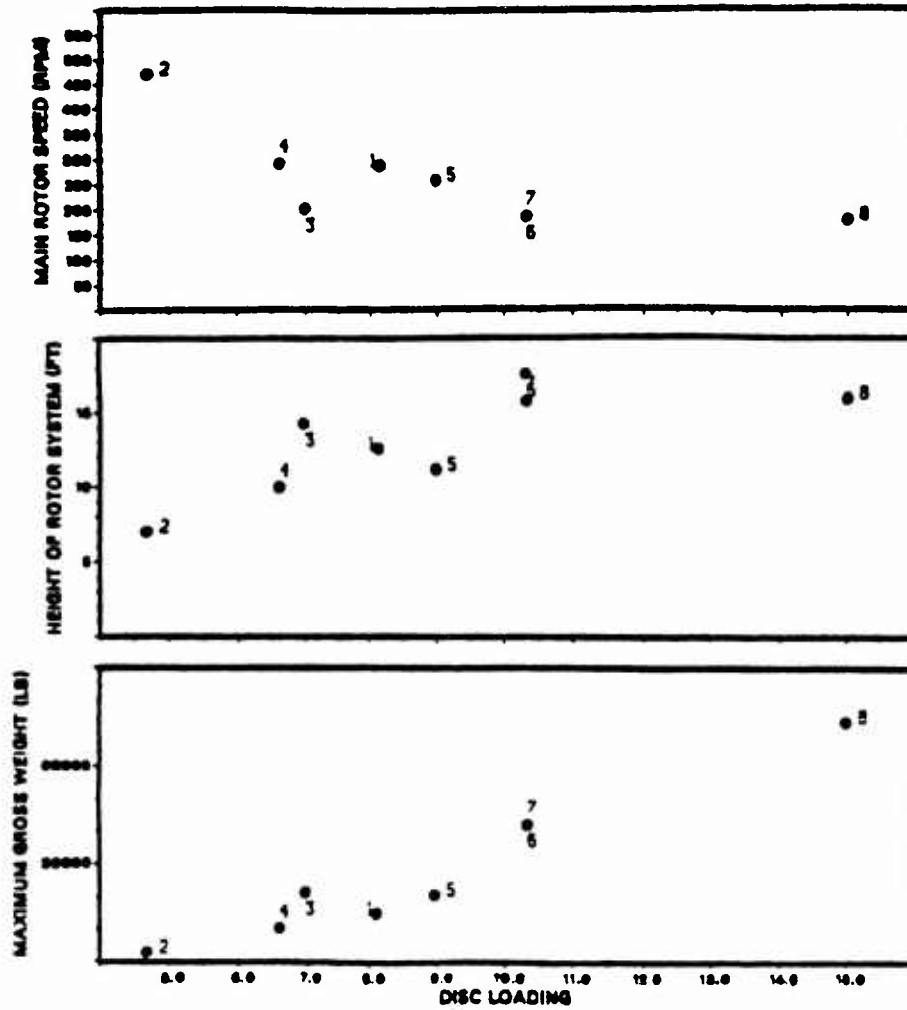


Figure 3.8. Three Plot Option

HELICOPTER DESIGN AE 4308/4900

1. AH-64 2. UH-60A
3. OH-6A 4. CH-54E
5. SH-3H 6. CH-53D
7. B-76 8. CH-54E

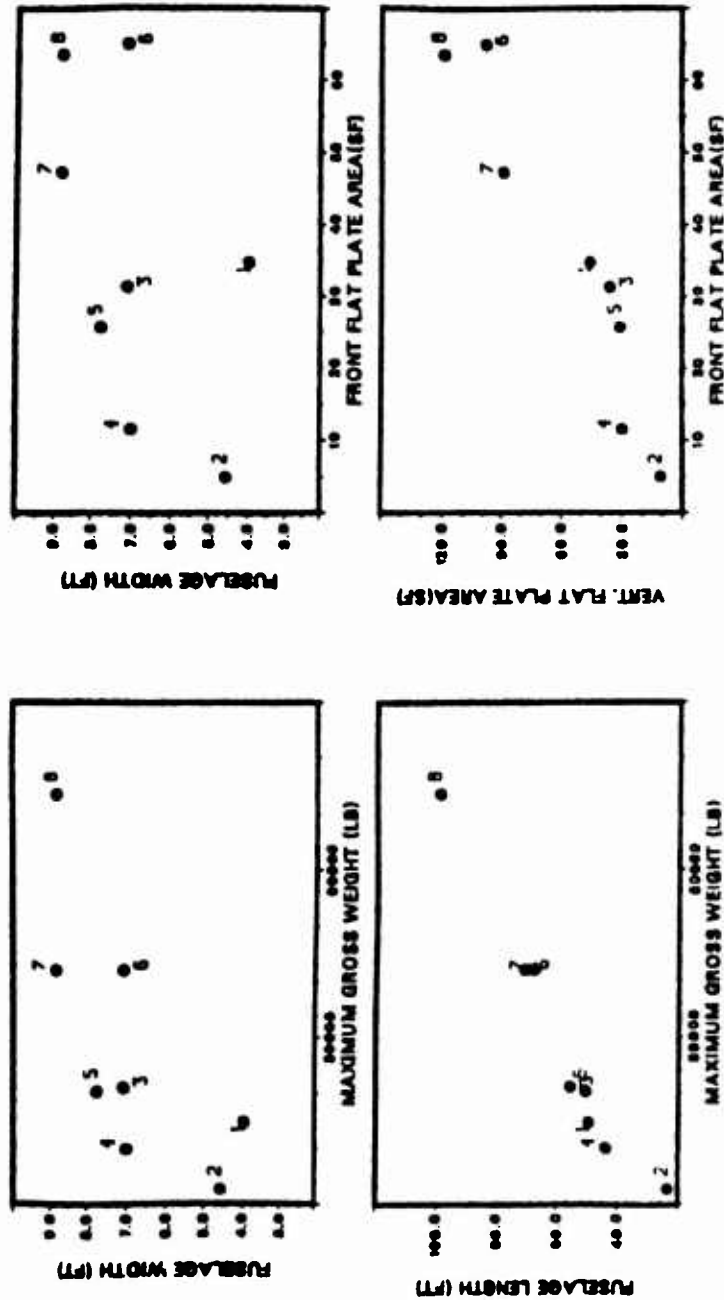


Figure 3.9. Four Plot Option

POWER VS. VELOCITY AT ALTITUDE

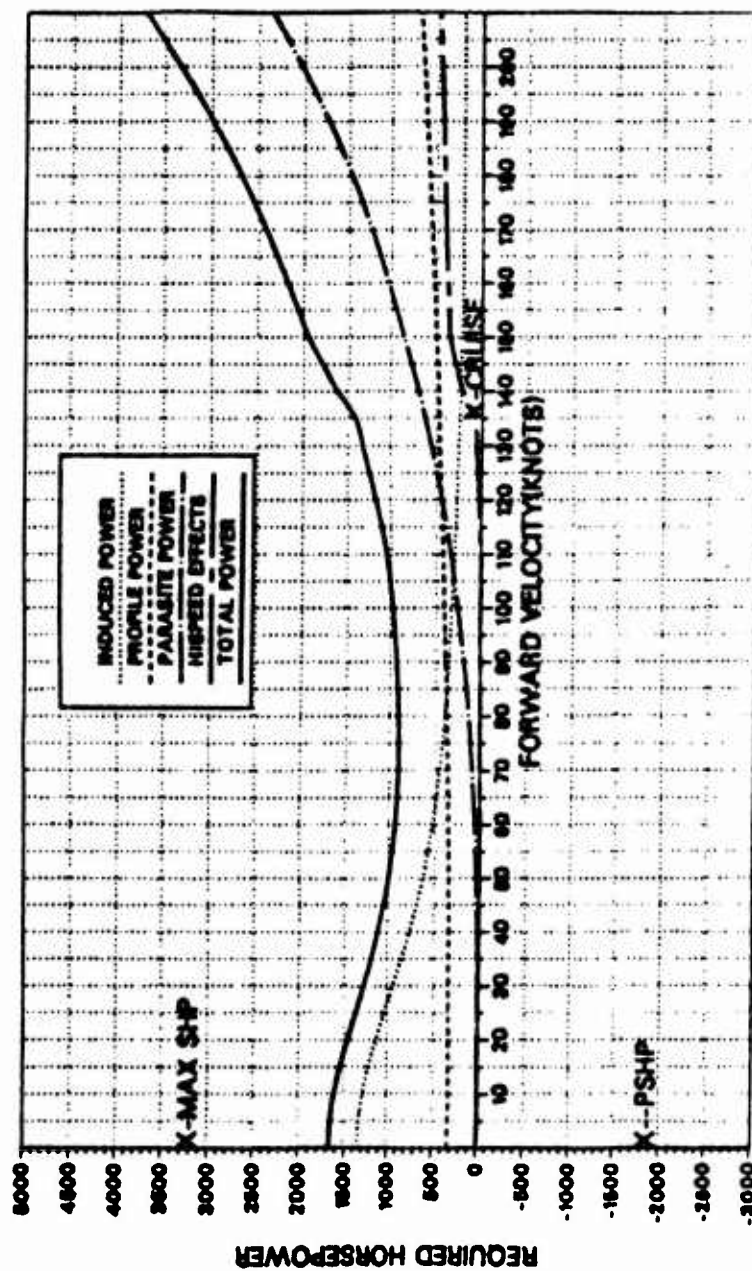


Figure 3.10. Sample Total Power Curve

BIBLIOGRAPHY

Casey, Timothy J., Powerplant Selection for Conceptual Helicopter Design, M.S. Thesis, Naval Postgraduate School, Monterey, CA, 1980.

Kee, Stephen G., Guide for Conceptual Helicopter Design, M.S. Thesis, Naval Postgraduate School, Monterey, CA, 1983.

Rogers, Michael W., Computer Programs for Preliminary Helicopter Design, M.S. Thesis, Naval Postgraduate School, Monterey, CA, 1983.

Schwab, Rudolph T., Computer Program Analysis of Helicopter Weight Estimate Relationships Utilizing Parametric Equations, M.S. Thesis, Naval Postgraduate School, Monterey, CA, 1982.

Young, James E., Helicopter Vertical Stabilizer Design Considerations, M.S. Thesis, Naval Postgraduate School, Monterey, CA, 1980.

LIST OF REFERENCES

1. ISSCO Graphics, DISSPLA Pocket Guide, Integrated Software Systems Corporation, 1981.
2. Layton, D.M., Helicopter Design Manual, Naval Postgraduate School, 1983.
3. Layton, D.M., Helicopter Performance, Naval Postgraduate School, 1983.

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